

## FEATURES

### Low noise

- 1 nV/ $\sqrt{\text{Hz}}$  input noise
- 45 nV/ $\sqrt{\text{Hz}}$  output noise

### High accuracy dc performance (AD8429BRZ)

- 90 dB CMRR minimum ( $G = 1$ )
- 50  $\mu\text{V}$  maximum input offset voltage
- 0.02% maximum gain accuracy ( $G = 1$ )

### Excellent ac specifications

- 80 dB CMRR to 5 kHz ( $G = 1$ )
- 15 MHz bandwidth ( $G = 1$ )
- 1.2 MHz bandwidth ( $G = 100$ )
- 22 V/ $\mu\text{s}$  slew rate
- THD:  $-130$  dBc (1 kHz,  $G = 1$ )

### Versatile

- $\pm 4$  V to  $\pm 18$  V dual supply
- Gain set with a single resistor ( $G = 1$  to 10,000)

### Temperature range for specified performance

- $-40^\circ\text{C}$  to  $+125^\circ\text{C}$

## APPLICATIONS

- Medical instrumentation
- Precision data acquisition
- Microphone preamplification
- Vibration analysis

## GENERAL DESCRIPTION

The AD8429 is an ultralow noise, instrumentation amplifier designed for measuring extremely small signals over a wide temperature range ( $-40^\circ\text{C}$  to  $+125^\circ\text{C}$ ).

The AD8429 excels at measuring tiny signals. It delivers ultralow input noise performance of 1 nV/ $\sqrt{\text{Hz}}$ . The high CMRR of the AD8429 prevents unwanted signals from corrupting the acquisition. The CMRR increases as the gain increases, offering high rejection when it is most needed. The high performance pin configuration of the AD8429 allows it to reliably maintain high CMRR at frequencies well beyond those of typical instrumentation amplifiers.

The AD8429 reliably amplifies fast changing signals. Its current feedback architecture provides high bandwidth at high gain, for example, 1.2 MHz at  $G = 100$ . The design includes circuitry to improve settling time after large input voltage transients. The AD8429 was designed for excellent distortion performance, allowing use in demanding applications such as vibration analysis.

Gain is set from 1 to 10,000 with a single resistor. A reference pin allows the user to offset the output voltage. This feature can

### Rev. A

### Document Feedback

Information furnished by Analog Devices is believed to be accurate and reliable. However, no responsibility is assumed by Analog Devices for its use, nor for any infringements of patents or other rights of third parties that may result from its use. Specifications subject to change without notice. No license is granted by implication or otherwise under any patent or patent rights of Analog Devices. Trademarks and registered trademarks are the property of their respective owners.

## PIN CONNECTION DIAGRAM

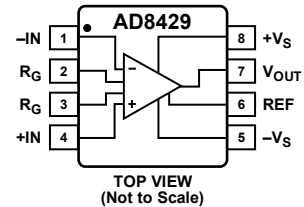


Figure 1.

09730-001

be useful to shift the output level when interfacing to a single supply signal chain.

The AD8429 performance is specified over the extended industrial temperature range of  $-40^\circ\text{C}$  to  $+125^\circ\text{C}$ . It is available in an 8-lead plastic SOIC package.

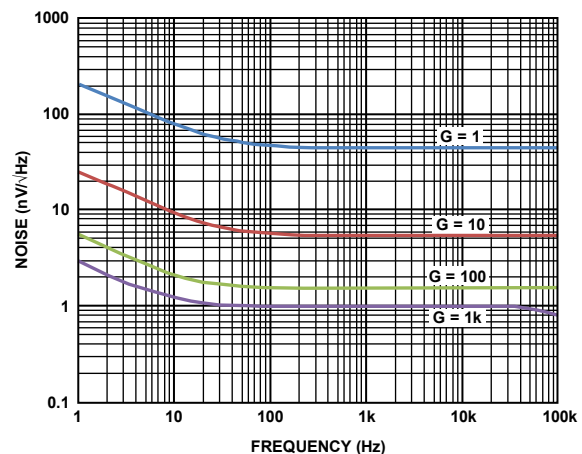


Figure 2. RTI Voltage Noise Spectral Density vs. Frequency

09730-012

## TABLE OF CONTENTS

Features .....	1	Architecture .....	15
Applications.....	1	Gain Selection.....	15
Pin Connection Diagram .....	1	Reference Terminal .....	15
General Description .....	1	Input Voltage Range.....	16
Revision History .....	2	Layout .....	16
Specifications.....	3	Input Bias Current Return Path .....	17
Absolute Maximum Ratings.....	6	Input Protection .....	17
Thermal Resistance .....	6	Radio Frequency Interference (RFI).....	17
ESD Caution.....	6	Calculating the Noise of the Input Stage.....	18
Pin Configuration and Function Descriptions.....	7	Outline Dimensions .....	19
Typical Performance Characteristics .....	8	Ordering Guide .....	19
Theory of Operation .....	15		

## REVISION HISTORY

### 2/2017—Rev. 0 to Rev. A

Changes to Figure 2.....	1
Change to Input Current Parameter, Table 1 .....	3
Changes to Figure 20 and Figure 21 .....	10
Changes to Figure 24 through Figure 27 .....	11
Changes to Figure 28 and Figure 30.....	12
Change to Large Differential Input Voltage at High Gain Section.....	17
Changes to Figure 53.....	18

### 4/2011—Revision 0: Initial Version

## SPECIFICATIONS

$V_S = \pm 15\text{ V}$ ,  $V_{REF} = 0\text{ V}$ ,  $T_A = 25^\circ\text{C}$ ,  $G = 1$ ,  $R_L = 10\text{ k}\Omega$ , unless otherwise noted.

Table 1.

Parameter	Test Conditions/Comments	A Grade			B Grade			Unit	
		Min	Typ	Max	Min	Typ	Max		
COMMON-MODE REJECTION RATIO (CMRR)	$V_{CM} = \pm 10\text{ V}$								
CMRR DC to 60 Hz with 1 k $\Omega$ Source Imbalance									
G = 1		80			90			dB	
G = 10		100			110			dB	
G = 100		120			130			dB	
G = 1000		134			140			dB	
CMRR at 5 kHz		$V_{CM} = \pm 10\text{ V}$							
G = 1			76			80			dB
G = 10	90				90			dB	
G = 100	90				90			dB	
G = 1000	90			90			dB		
VOLTAGE NOISE, RTI	$V_{IN+}, V_{IN-} = 0\text{ V}$								
Spectral Density <sup>1</sup> : 1 kHz									
Input Voltage Noise, $e_{ni}$					1.0			nV/ $\sqrt{\text{Hz}}$	
Output Voltage Noise, $e_{no}$					45			nV/ $\sqrt{\text{Hz}}$	
Peak to Peak: 0.1 Hz to 10 Hz									
G = 1				2			2	$\mu\text{V p-p}$	
G = 1000			100			100	nV p-p		
CURRENT NOISE									
Spectral Density: 1 kHz				1.5			1.5	pA/ $\sqrt{\text{Hz}}$	
Peak to Peak: 0.1 Hz to 10 Hz				100			100	pA p-p	
VOLTAGE OFFSET <sup>2</sup>	$V_S = \pm 5\text{ V to } \pm 15\text{ V}$								
Input Offset, $V_{OSI}$					150			$\mu\text{V}$	
Average TC				0.1	1		0.1	$\mu\text{V}/^\circ\text{C}$	
Output Offset, $V_{OSO}$					1000			$\mu\text{V}$	
Average TC				3	10		3	$\mu\text{V}/^\circ\text{C}$	
Offset RTI vs. Supply (PSR)									
G = 1		90					100	dB	
G = 10		110					120	dB	
G = 100		130					130	dB	
G = 1000		130					130	dB	
INPUT CURRENT	$V_{IN+}, V_{IN-} = 0\text{ V}$								
Input Bias Current					300			nA	
Average TC				250			250	pA/ $^\circ\text{C}$	
Input Offset Current					100			nA	
Average TC				15			15	pA/ $^\circ\text{C}$	
DYNAMIC RESPONSE									
Small Signal Bandwidth: -3 dB									
G = 1				15			15	MHz	
G = 10				4			4	MHz	
G = 100				1.2			1.2	MHz	
G = 1000			0.15			0.15	MHz		

Parameter	Test Conditions/Comments	A Grade			B Grade			Unit
		Min	Typ	Max	Min	Typ	Max	
Settling Time 0.01%	10 V step							
G = 1			0.75			0.75		μs
G = 10			0.65			0.65		μs
G = 100			0.85			0.85		μs
Settling Time 0.001%	10 V step							
G = 1			0.9			0.9		μs
G = 10			0.9			0.9		μs
G = 100			1.2			1.2		μs
Slew Rate								
G = 1 to 100			22			22		V/μs
THD	First five harmonics, f = 1 kHz, R <sub>L</sub> = 2 kΩ, V <sub>OUT</sub> = 10 V p-p							
G = 1			-130			-130		dBc
G = 10			-116			-116		dBc
G = 100			-113			-113		dBc
G = 1000			-111			-111		dBc
THD + N	f = 1 kHz, R <sub>L</sub> = 2 kΩ, V <sub>OUT</sub> = 10 V p-p							
G = 100			0.0005			0.0005		%
GAIN <sup>3</sup>	G = 1 + (6 kΩ/R <sub>G</sub> )							
Gain Range		1		10000	1		10000	V/V
Gain Error	V <sub>OUT</sub> = ±10 V							
G = 1				0.05			0.02	%
G > 1				0.3			0.15	%
Gain Nonlinearity	V <sub>OUT</sub> = -10 V to +10 V R <sub>L</sub> = 10 kΩ							
G = 1 to 1000			2			2		ppm
Gain vs. Temperature								
G = 1			2	5		2	5	ppm/°C
G > 1				-100			-100	ppm/°C
INPUT								
Impedance (Pin to Ground) <sup>4</sup>			1.5  3			1.5  3		GΩ  pF
Input Operating Voltage Range <sup>5</sup>	V <sub>S</sub> = ±4 V to ±18 V	-V <sub>S</sub> + 2.8		+V <sub>S</sub> - 2.5	-V <sub>S</sub> + 2.8		+V <sub>S</sub> - 2.5	V
OUTPUT								
Output Swing	R <sub>L</sub> = 2 kΩ	-V <sub>S</sub> + 1.8		+V <sub>S</sub> - 1.2	-V <sub>S</sub> + 1.8		+V <sub>S</sub> - 1.2	V
Over Temperature			-V <sub>S</sub> + 1.9		+V <sub>S</sub> - 1.3	-V <sub>S</sub> + 1.9		+V <sub>S</sub> - 1.3
Output Swing	R <sub>L</sub> = 10 kΩ	-V <sub>S</sub> + 1.7		+V <sub>S</sub> - 1.1	-V <sub>S</sub> + 1.7		+V <sub>S</sub> - 1.1	V
Over Temperature			-V <sub>S</sub> + 1.8		+V <sub>S</sub> - 1.2	-V <sub>S</sub> + 1.8		+V <sub>S</sub> - 1.2
Short-Circuit Current			35			35		mA
REFERENCE INPUT								
R <sub>IN</sub>	V <sub>IN+</sub> , V <sub>IN-</sub> = 0 V		10			10		kΩ
I <sub>IN</sub>			70			70		μA
Voltage Range			-V <sub>S</sub>		+V <sub>S</sub>			V
Reference Gain to Output				1			1	V/V
Reference Gain Error			0.01	0.05		0.01	0.05	%

Parameter	Test Conditions/Comments	A Grade			B Grade			Unit
		Min	Typ	Max	Min	Typ	Max	
POWER SUPPLY								
Operating Range		±4		±18	±4		±18	V
Quiescent Current	T = 125°C		6.7	7 9		6.7	7 9	mA mA
TEMPERATURE RANGE								
For Specified Performance		-40		+125	-40		+125	°C

<sup>1</sup> Total voltage noise =  $\sqrt{(e_n)^2 + (e_{no}/G)^2 + e_{RG}^2}$ . See the Theory of Operation section for more information.

<sup>2</sup> Total RTI  $V_{OS} = (V_{OSI}) + (V_{OSO}/G)$ .

<sup>3</sup> These specifications do not include the tolerance of the external gain setting resistor,  $R_G$ . For  $G > 1$ , add  $R_G$  errors to the specifications given in this table.

<sup>4</sup> Differential and common-mode input impedance can be calculated from the pin impedance:  $Z_{DIFF} = 2(Z_{PIN})$ ;  $Z_{CM} = Z_{PIN}/2$ .

<sup>5</sup> Input voltage range of the AD8429 input stage only. The input range can depend on the common-mode voltage, differential voltage, gain, and reference voltage. See the Input Voltage Range section for more details.

## ABSOLUTE MAXIMUM RATINGS

Table 2.

Parameter	Rating
Supply Voltage	±18 V
Output Short-Circuit Current Duration	Indefinite
Maximum Voltage at -IN, +IN <sup>1</sup>	±V <sub>S</sub>
Differential Input Voltage <sup>1</sup>	
Gain ≤ 4	±V <sub>S</sub>
4 > Gain > 50	±50 V/gain
Gain ≥ 50	±1 V
Maximum Voltage at REF	±V <sub>S</sub>
Storage Temperature Range	-65°C to +150°C
Specified Temperature Range	-40°C to +125°C
Maximum Junction Temperature	140°C
ESD	
Human Body Model	3.0 kV
Charge Device Model	1.5 kV
Machine Model	0.2 kV

<sup>1</sup>For voltages beyond these limits, use input protection resistors. See the Theory of Operation section for more information.

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

## THERMAL RESISTANCE

$\theta_{JA}$  is specified for a device in free air using a 4-layer JEDEC printed circuit board (PCB).

Table 3.

Package	$\theta_{JA}$	Unit
8-Lead SOIC	121	°C/W

## ESD CAUTION



### ESD (electrostatic discharge) sensitive device.

Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS

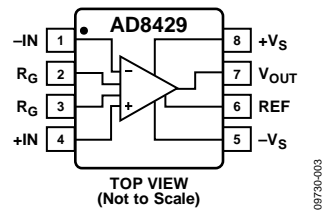


Figure 3. Pin Configuration

Table 4. Pin Function Descriptions

Pin No.	Mnemonic	Description
1	-IN	Negative Input Terminal.
2, 3	R <sub>G</sub>	Gain Setting Terminals. Place resistor across the R <sub>G</sub> pins to set the gain. $G = 1 + (6 \text{ k}\Omega/R_G)$ .
4	+IN	Positive Input Terminal.
5	-V <sub>S</sub>	Negative Power Supply Terminal.
6	REF	Reference Voltage Terminal. Drive this terminal with a low impedance voltage source to level shift the output.
7	V <sub>OUT</sub>	Output Terminal.
8	+V <sub>S</sub>	Positive Power Supply Terminal.

# TYPICAL PERFORMANCE CHARACTERISTICS

T = 25°C, V<sub>S</sub> = ±15V, V<sub>REF</sub> = 0, R<sub>L</sub> = 10 kΩ, unless otherwise noted.

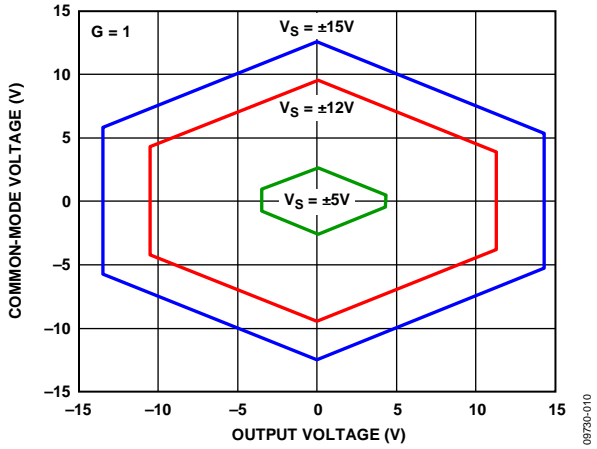


Figure 4. Input Common-Mode Voltage vs. Output Voltage, Dual Supply, V<sub>S</sub> = ±5V, ±12V, ±15V (G = 1)

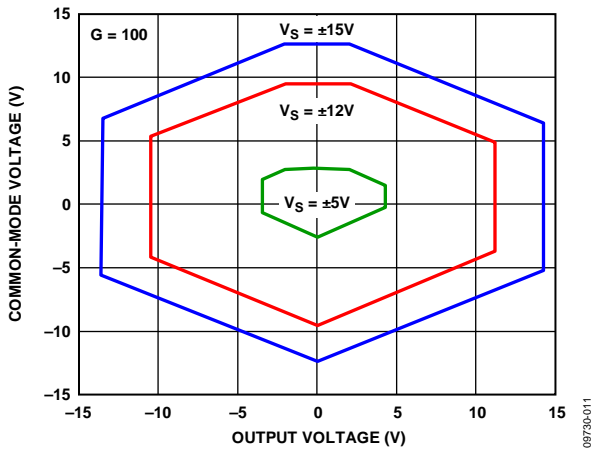


Figure 5. Input Common-Mode Voltage vs. Output Voltage, Dual Supply, V<sub>S</sub> = ±5V, ±12V, ±15V (G = 100)

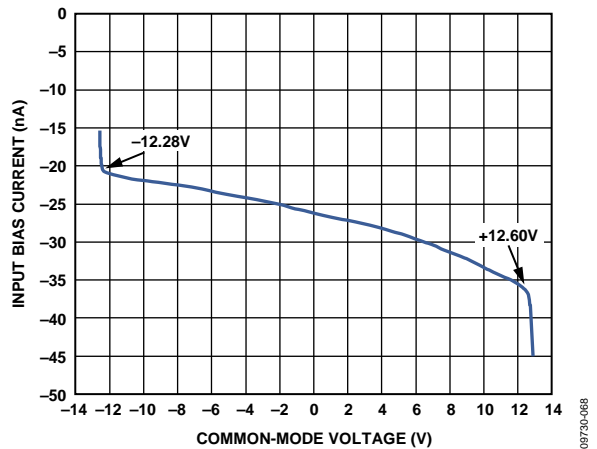


Figure 6. Input Bias Current vs. Common-Mode Voltage

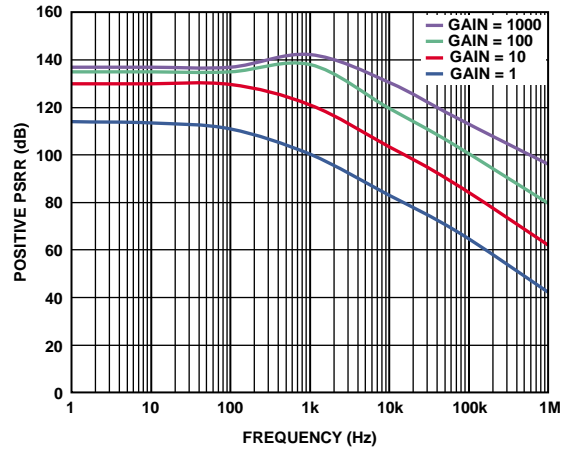


Figure 7. Positive PSRR vs. Frequency

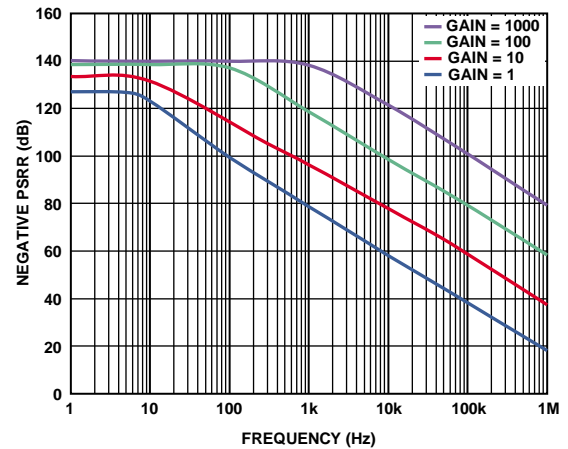


Figure 8. Negative PSRR vs. Frequency

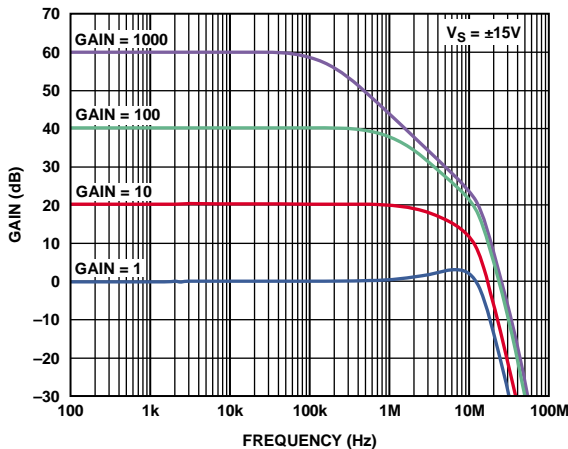


Figure 9. Gain vs. Frequency



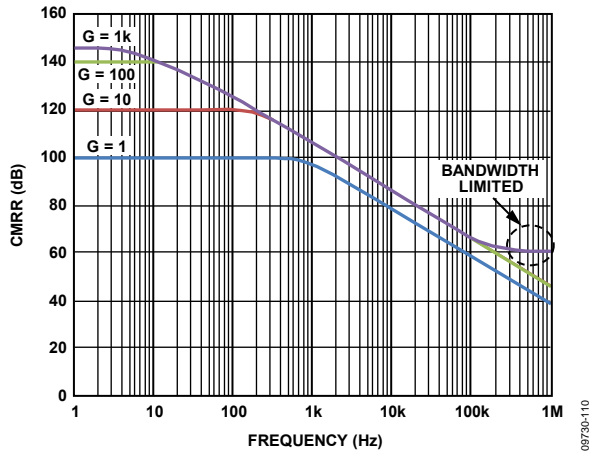


Figure 10. CMRR vs. Frequency

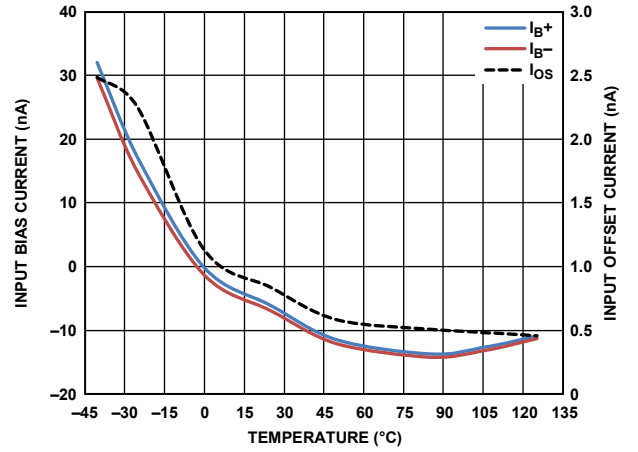


Figure 13. Input Bias Current and Input Offset Current vs. Temperature

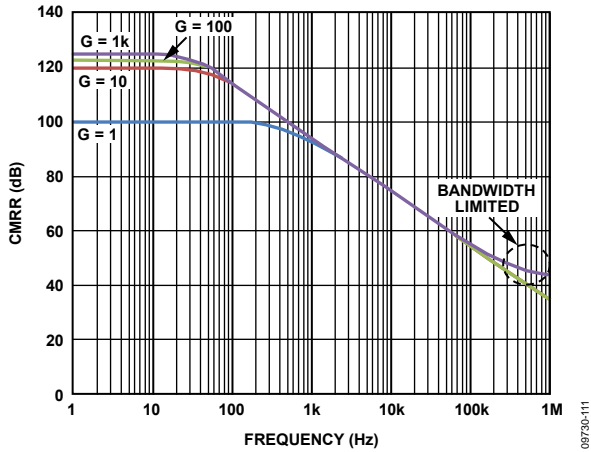


Figure 11. CMRR vs. Frequency, 1 kΩ Source Imbalance

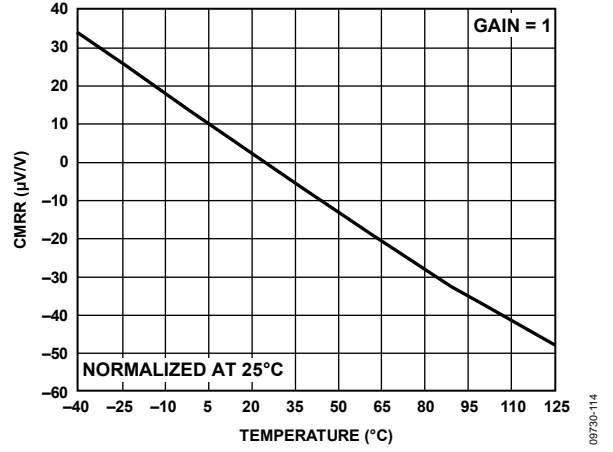


Figure 14. CMRR vs. Temperature (G = 1), Normalized at 25°C

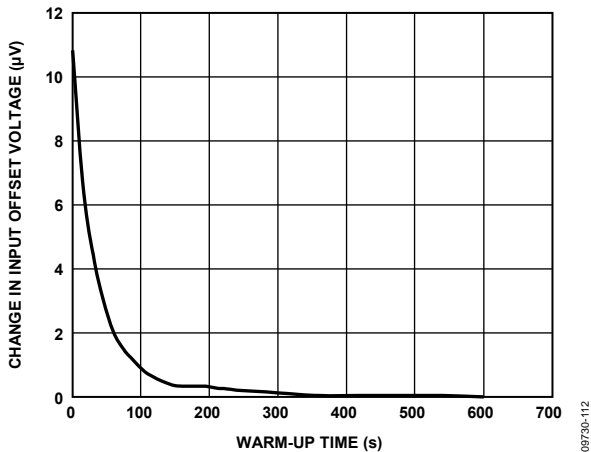


Figure 12. Change in Input Offset Voltage ( $V_{OSI}$ ) vs. Warm-Up Time

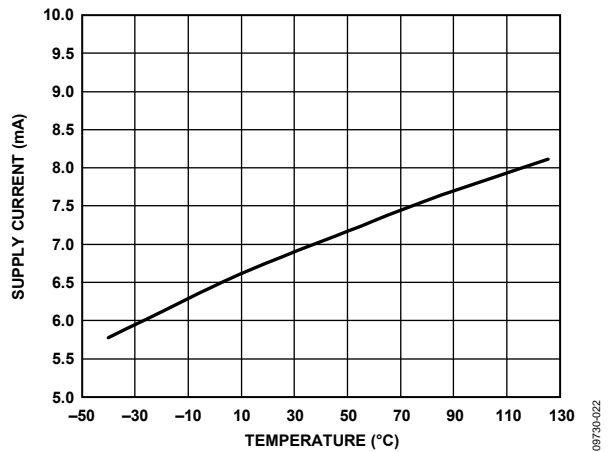


Figure 15. Supply Current vs. Temperature (G = 1)

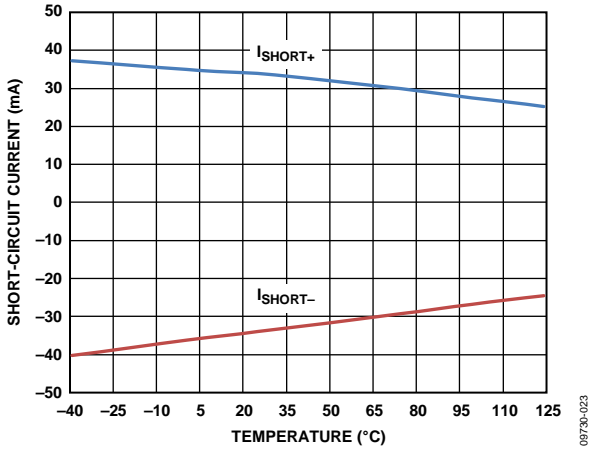


Figure 16. Short-Circuit Current vs. Temperature ( $G = 1$ )

09730-023

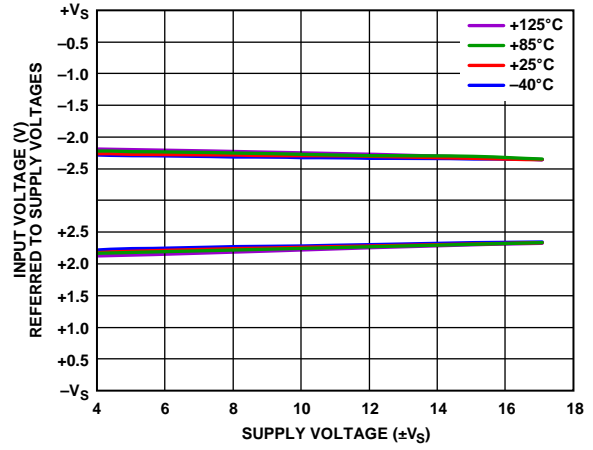


Figure 19. Input Voltage Limit vs. Supply Voltage

09730-026

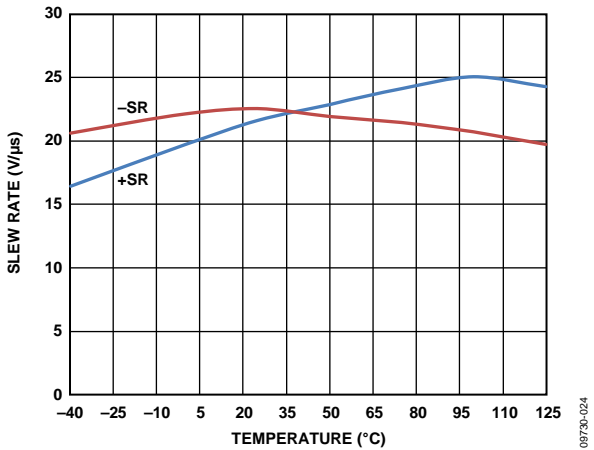


Figure 17. Slew Rate vs. Temperature,  $V_s = \pm 15\text{ V}$  ( $G = 1$ )

09730-024

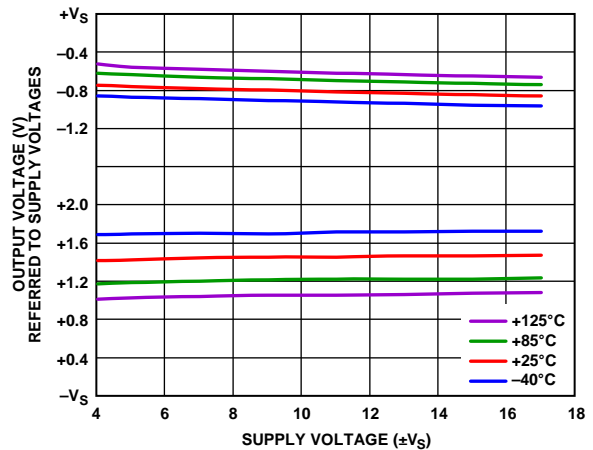


Figure 20. Output Voltage Swing vs. Supply Voltage,  $R_L = 10\text{ k}\Omega$

09730-027

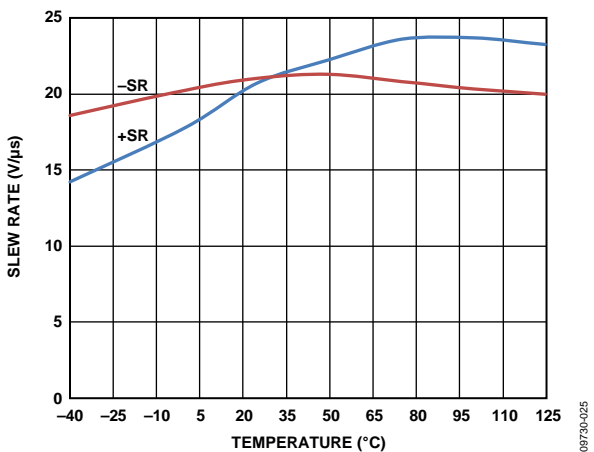


Figure 18. Slew Rate vs. Temperature,  $V_s = \pm 5\text{ V}$  ( $G = 1$ )

09730-025

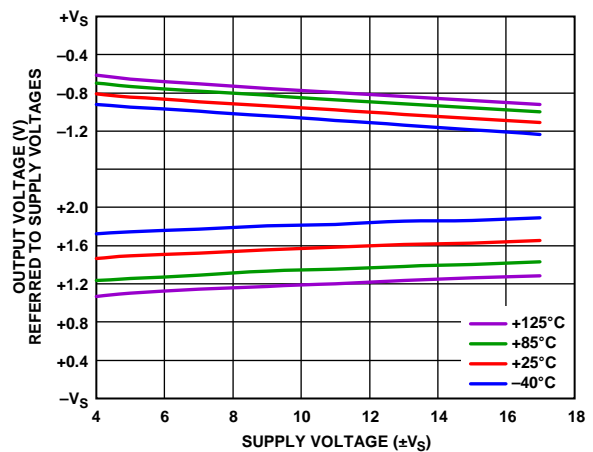


Figure 21. Output Voltage Swing vs. Supply Voltage,  $R_L = 2\text{ k}\Omega$

09730-028

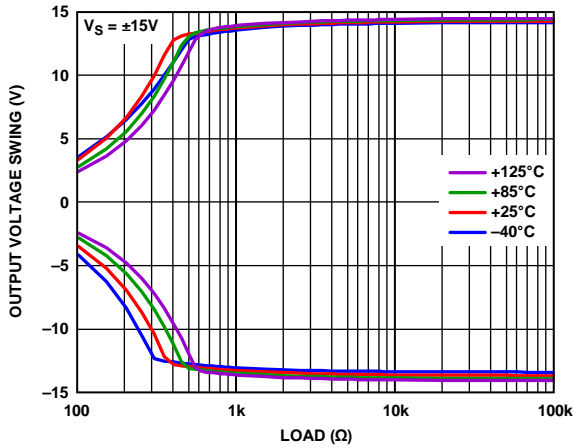


Figure 22. Output Voltage Swing vs. Load Resistance

09730-029

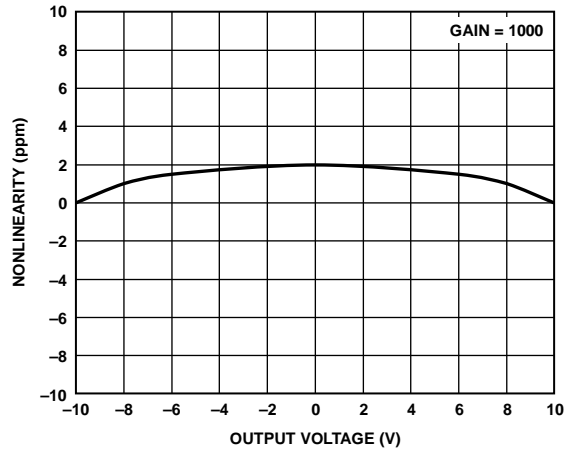


Figure 25. Gain Nonlinearity ( $G = 1000$ ),  $R_L = 10\text{ k}\Omega$

09730-084

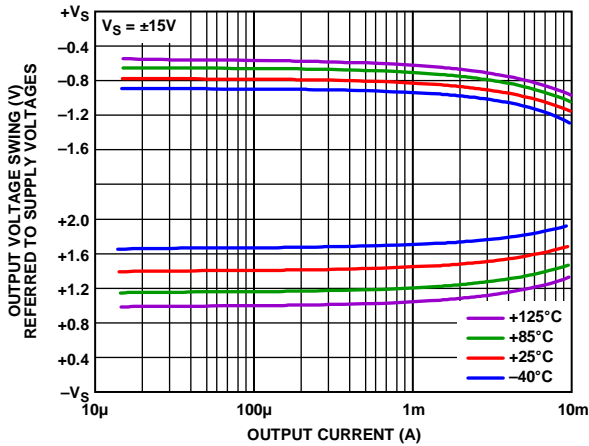


Figure 23. Output Voltage Swing vs. Output Current

09730-030

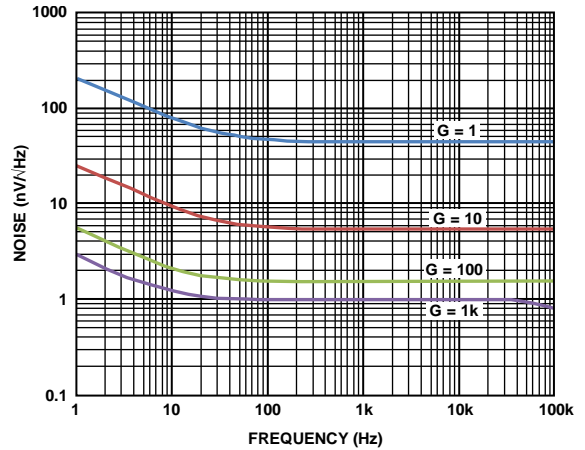


Figure 26. RTI Voltage Noise Spectral Density vs. Frequency

09730-126

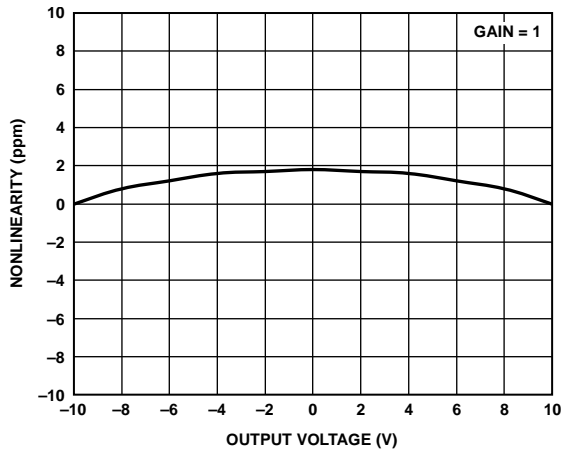


Figure 24. Gain Nonlinearity ( $G = 1$ ),  $R_L = 10\text{ k}\Omega$

09730-083

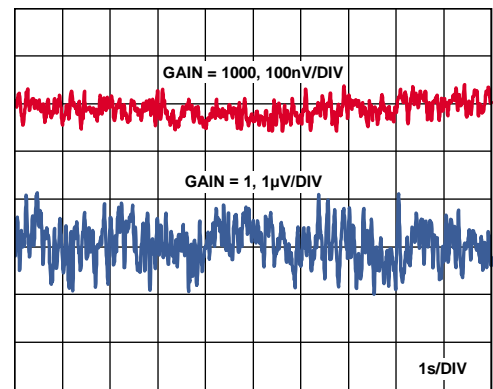


Figure 27. 0.1 Hz to 10 Hz RTI Voltage Noise ( $G = 1$ ,  $G = 1000$ )

09730-086

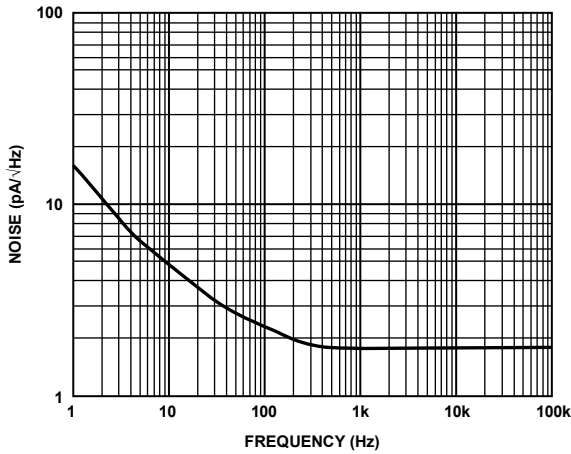


Figure 28. Current Noise Spectral Density vs. Frequency

09730-087

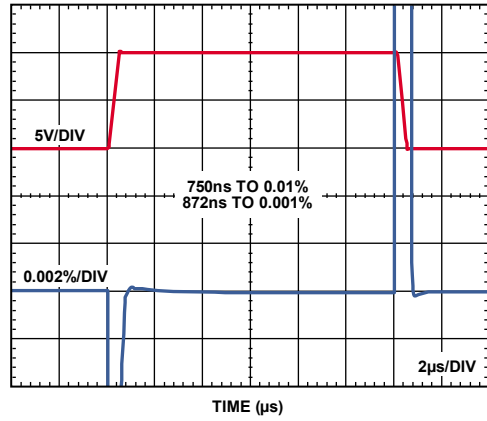


Figure 31. Large Signal Pulse Response and Settling Time ( $G = 1$ ), 10 V Step,  $V_S = \pm 15$  V

09730-090

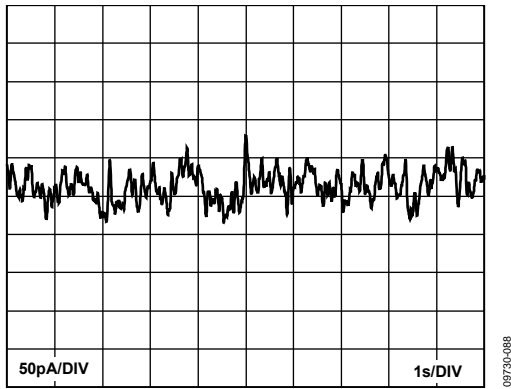


Figure 29. 0.1 Hz to 10 Hz Current Noise

09730-088

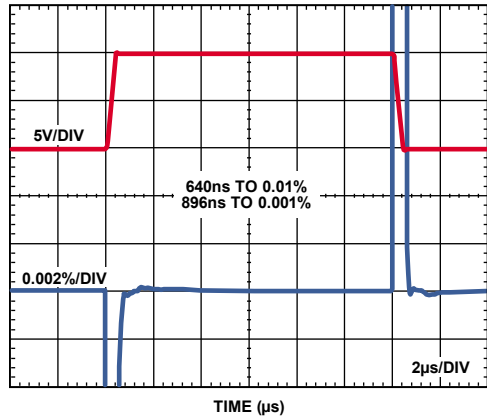


Figure 32. Large Signal Pulse Response and Settling Time ( $G = 10$ ), 10 V Step,  $V_S = \pm 15$  V

09730-091

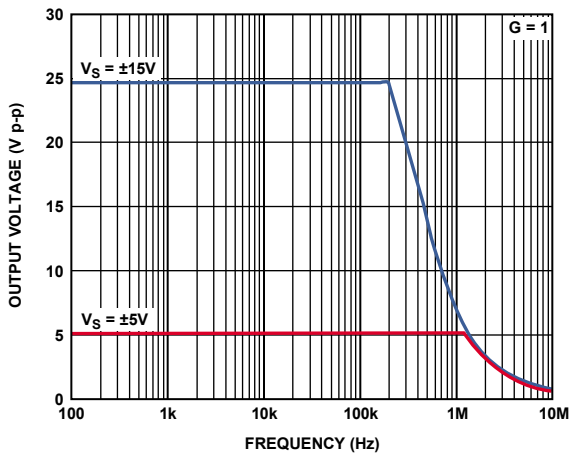


Figure 30. Large Signal Frequency Response

09730-089

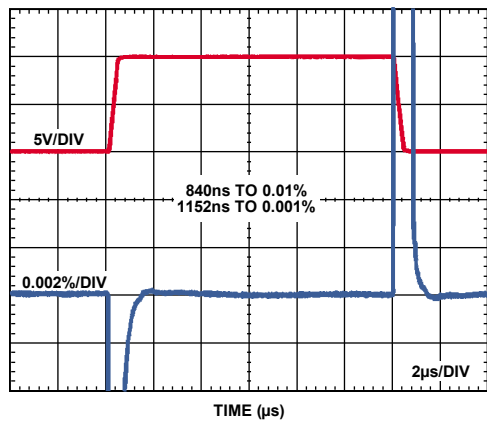


Figure 33. Large Signal Pulse Response and Settling Time ( $G = 100$ ), 10 V Step,  $V_S = \pm 15$  V

09730-040

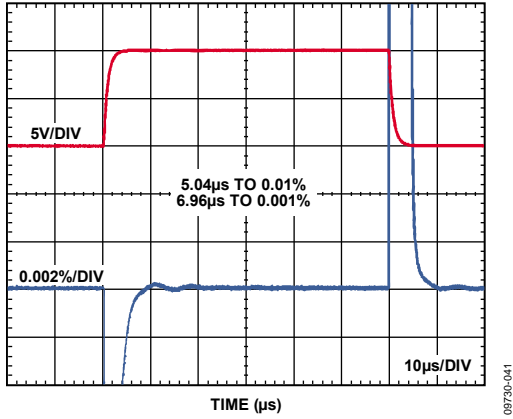


Figure 34. Large Signal Pulse Response and Settling Time ( $G = 1000$ ),  $10\text{ V Step}$ ,  $V_S = \pm 15\text{ V}$

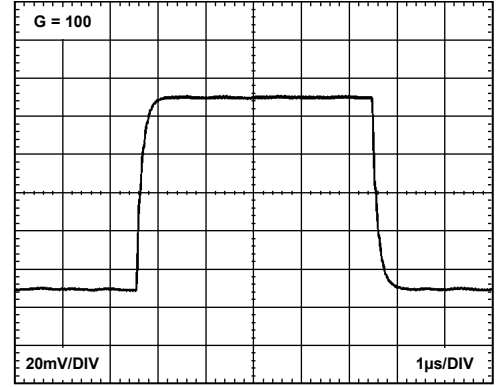


Figure 37. Small Signal Response ( $G = 100$ ),  $R_L = 10\text{ k}\Omega$ ,  $C_L = 100\text{ pF}$

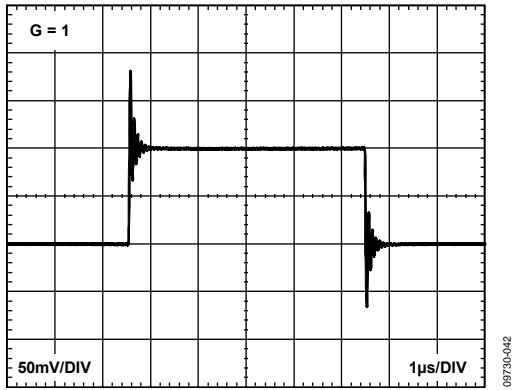


Figure 35. Small Signal Response ( $G = 1$ ),  $R_L = 10\text{ k}\Omega$ ,  $C_L = 100\text{ pF}$

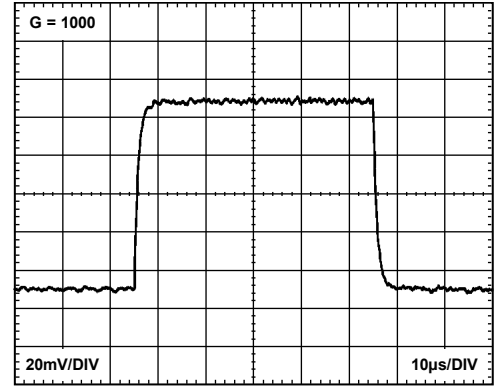


Figure 38. Small Signal Response ( $G = 1000$ ),  $R_L = 10\text{ k}\Omega$ ,  $C_L = 100\text{ pF}$

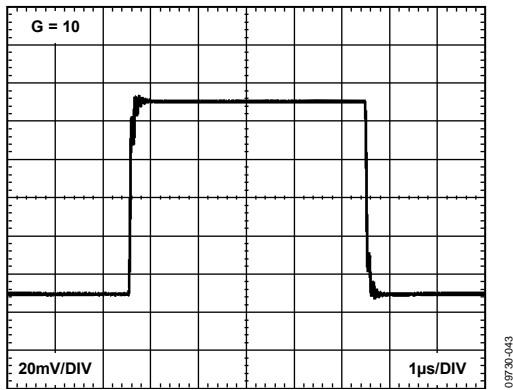


Figure 36. Small Signal Response ( $G = 10$ ),  $R_L = 10\text{ k}\Omega$ ,  $C_L = 100\text{ pF}$

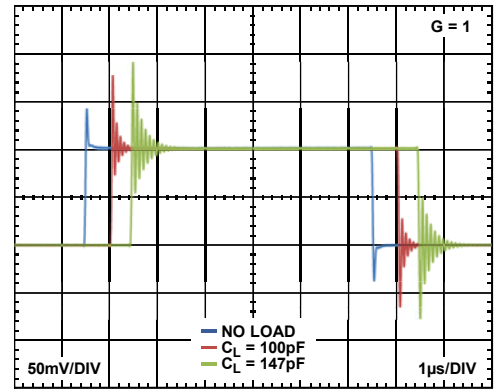


Figure 39. Small Signal Response with Various Capacitive Loads ( $G = 1$ ),  $R_L = \text{Infinity}$

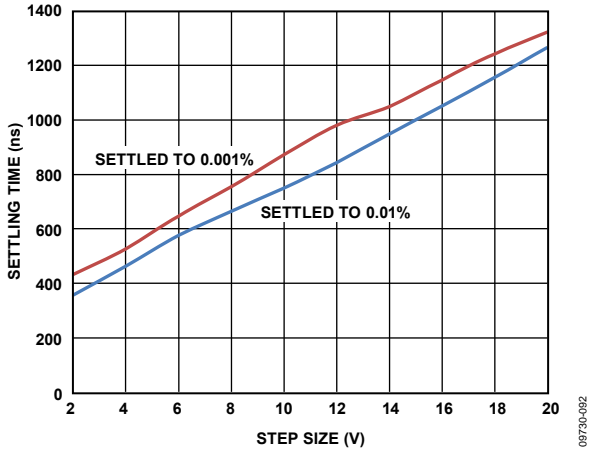


Figure 40. Settling Time vs. Step Size (G = 1)

08730-092

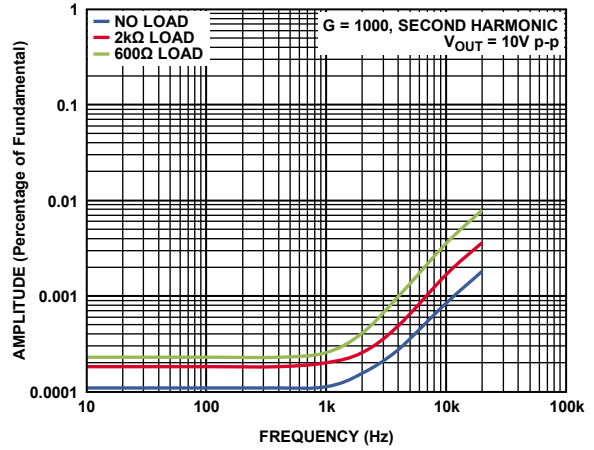


Figure 43. Second Harmonic Distortion vs. Frequency (G = 1000)

08730-098

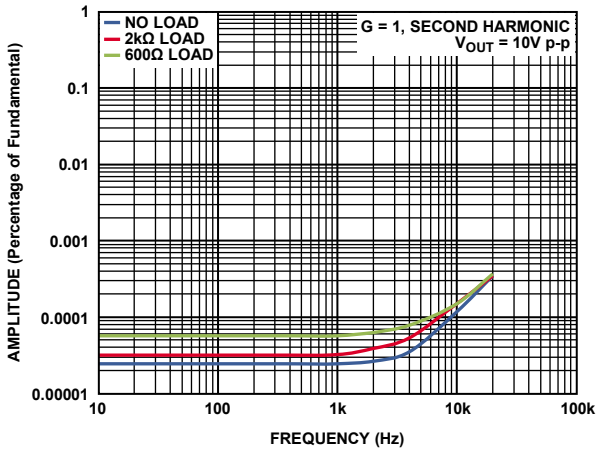


Figure 41. Second Harmonic Distortion vs. Frequency (G = 1)

08730-096

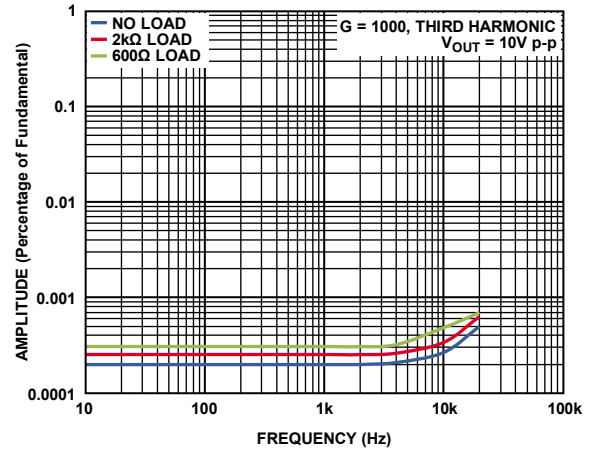


Figure 44. Third Harmonic Distortion vs. Frequency (G = 1000)

08730-099

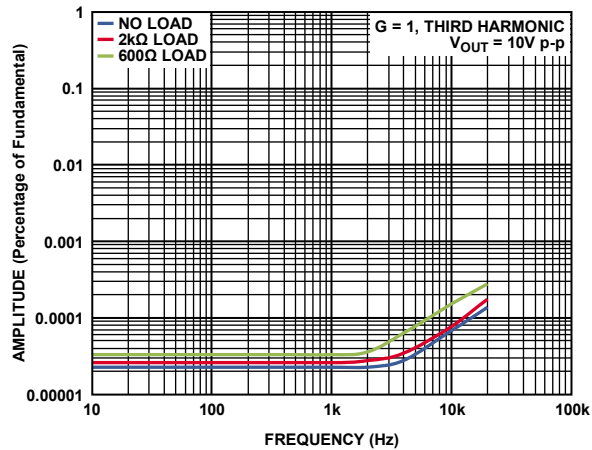


Figure 42. Third Harmonic Distortion vs. Frequency (G = 1)

08730-097

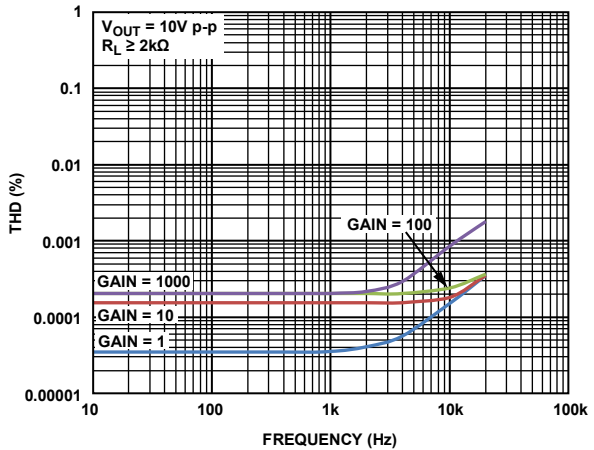


Figure 45. THD vs. Frequency

08730-100

## THEORY OF OPERATION

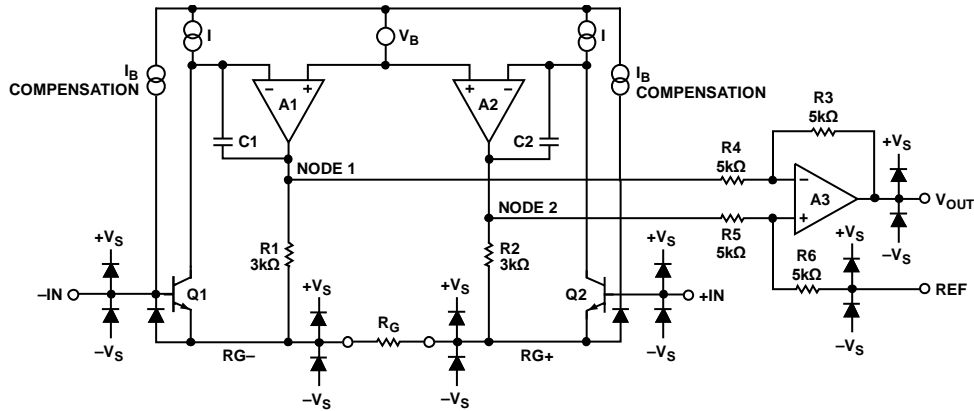


Figure 46. Simplified Schematic

### ARCHITECTURE

The AD8429 is based on the classic 3-op-amp topology. This topology has two stages: a preamplifier to provide differential amplification followed by a difference amplifier that removes the common-mode voltage and provides additional amplification. Figure 46 shows a simplified schematic of the AD8429.

The first stage works as follows. To keep its two inputs matched, Amplifier A1 must keep the collector of Q1 at a constant voltage. It does this by forcing RG– to be a precise diode drop from –IN. Similarly, A2 forces RG+ to be a constant diode drop from +IN. Therefore, a replica of the differential input voltage is placed across the gain setting resistor, RG. The current that flows through this resistance must also flow through the R1 and R2 resistors, creating a gained differential signal between the A2 and A1 outputs.

The second stage is a G = 1 difference amplifier, composed of Amplifier A3 and the R3 through R6 resistors. This stage removes the common-mode signal from the amplified differential signal.

The transfer function of the AD8429 is

$$V_{OUT} = G \times (V_{IN+} - V_{IN-}) + V_{REF}$$

where:

$$G = 1 + \frac{6 \text{ k}\Omega}{R_G}$$

### GAIN SELECTION

Placing a resistor across the RG terminals sets the gain of the AD8429, which can be calculated by referring to Table 5 or by using the following gain equation:

$$R_G = \frac{6 \text{ k}\Omega}{G - 1}$$

Table 5. Gains Achieved Using 1% Resistors

1% Standard Table Value of RG	Calculated Gain
6.04 kΩ	1.993
1.5 kΩ	5.000
665 Ω	10.02
316 Ω	19.99
121 Ω	50.59
60.4 Ω	100.3
30.1 Ω	200.3
12.1 Ω	496.9
6.04 Ω	994.4
3.01 Ω	1994

The AD8429 defaults to G = 1 when no gain resistor is used. Add the tolerance and gain drift of the RG resistor to the specifications of the AD8429 to determine the total gain accuracy of the system. When the gain resistor is not used, gain error and gain drift are minimal.

### RG Power Dissipation

The AD8429 duplicates the differential voltage across its inputs onto the RG resistor. Choose an RG resistor size sufficient to handle the expected power dissipation.

### REFERENCE TERMINAL

The output voltage of the AD8429 is developed with respect to the potential on the reference terminal. This is useful when the output signal must be offset to a precise midsupply level. For example, a voltage source can be tied to the REF pin to level shift the output, allowing the AD8429 to drive a single-supply ADC. The REF pin is protected with ESD diodes and should not exceed either +Vs or –Vs by more than 0.3 V.

For best performance, maintain a source impedance to the REF terminal that is well below  $1\ \Omega$ . As shown in Figure 46, the reference terminal, REF, is at one end of a  $5\ \text{k}\Omega$  resistor.

Additional impedance at the REF terminal adds to this  $5\ \text{k}\Omega$  resistor and results in amplification of the signal connected to the positive input. The amplification from the additional  $R_{REF}$  can be calculated as follows:

$$2(5\ \text{k}\Omega + R_{REF}) / (10\ \text{k}\Omega + R_{REF})$$

Only the positive signal path is amplified; the negative path is unaffected. This uneven amplification degrades CMRR.

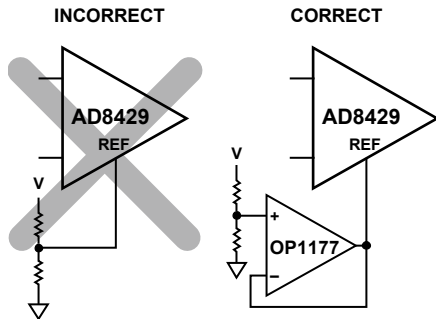


Figure 47. Driving the Reference Pin

## INPUT VOLTAGE RANGE

Figure 4 and Figure 5 show the allowable common-mode input voltage ranges for various output voltages and supply voltages. The 3-op-amp architecture of the AD8429 applies gain in the first stage before removing common-mode voltage with the difference amplifier stage. Internal nodes between the first and second stages (Node 1 and Node 2 in Figure 46) experience a combination of a gained signal, a common-mode signal, and a diode drop. This combined signal can be limited by the voltage supplies even when the individual input and output signals are not limited.

## LAYOUT

To ensure optimum performance of the AD8429 at the PCB level, care must be taken in the design of the board layout. The pins of the AD8429 are arranged in a logical manner to aid in this task.

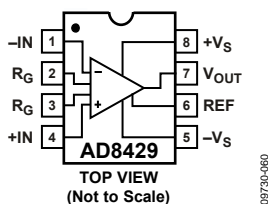


Figure 48. Pinout Diagram

## Common-Mode Rejection Ratio over Frequency

Poor layout can cause some of the common-mode signals to be converted to differential signals before reaching the in-amp. Such conversions occur when one input path has a frequency response that is different from the other. To maintain high CMRR over frequency, closely match the input source impedance and capacitance of each path. Place additional

source resistance in the input path (for example, for input protection) close to the in-amp inputs, which minimizes their interaction with parasitic capacitance from the PCB traces.

Parasitic capacitance at the gain setting pins can also affect CMRR over frequency. If the board design has a component at the gain setting pins (for example, a switch or jumper), choose a component such that the parasitic capacitance is as small as possible.

## Power Supplies and Grounding

Use a stable dc voltage to power the instrumentation amplifier. Noise on the supply pins can adversely affect performance. See the PSRR performance curves in Figure 9 and Figure 10 for more information.

Place a  $0.1\ \mu\text{F}$  capacitor as close as possible to each supply pin. Because the length of the bypass capacitor leads is critical at high frequency, surface-mount capacitors are recommended. A parasitic inductance in the bypass ground trace works against the low impedance created by the bypass capacitor. As shown in Figure 49, a  $10\ \mu\text{F}$  capacitor can be used farther away from the device. For larger value capacitors, intended to be effective at lower frequencies, the current return path distance is less critical. In most cases, this capacitor can be shared by other precision integrated circuits.

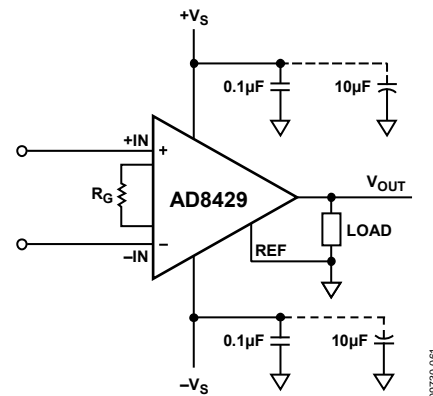


Figure 49. Supply Decoupling, REF, and Output Referred to Local Ground

A ground plane layer is helpful to reduce parasitic inductances. This minimizes voltage drops with changes in current. The area of the current path is directly proportional to the magnitude of parasitic inductances and, therefore, the impedance of the path at high frequency. Large changes in currents in an inductive decoupling path or ground return create unwanted effects, due to the coupling of such changes into the amplifier inputs.

Because load currents flow from the supplies, the load should be connected at the same physical location as the bypass capacitor grounds.

## Reference Pin

The output voltage of the AD8429 is developed with respect to the potential on the reference terminal. Ensure that REF is tied to the appropriate local ground.



### INPUT BIAS CURRENT RETURN PATH

The input bias current of the AD8429 must have a return path to ground. When using a floating source without a current return path, such as a thermocouple, create a current return path, as shown in Figure 50.

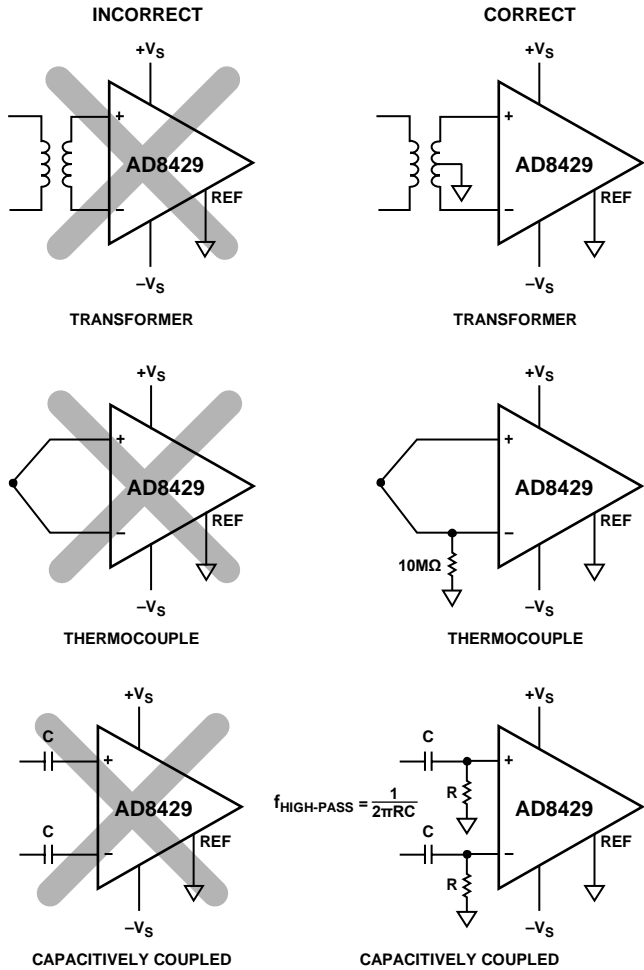


Figure 50. Creating an Input Bias Current Return Path

### INPUT PROTECTION

Do not allow the inputs of the AD8429 to exceed the ratings stated in the Absolute Maximum Ratings section of this data sheet. If this cannot be done, protection circuitry can be added in front of the AD8429 to limit the current into the inputs to a maximum current,  $I_{MAX}$ .

#### Input Voltages Beyond the Rails

If voltages beyond the rails are expected, use an external resistor in series with each input to limit current during overload conditions. The limiting resistor at the input can be computed from

$$R_{PROTECT} \geq \frac{|V_{IN} - V_{SUPPLY}|}{I_{MAX}}$$

Noise sensitive applications may require a lower protection resistance. Low leakage diode clamps, such as the BAV199, can be used at the inputs to shunt current away from the AD8429 inputs, thereby allowing smaller protection resistor values. To ensure current flows primarily through the external protection diodes, place a small value resistor, such as a 33 Ω, between the diodes and the AD8429.

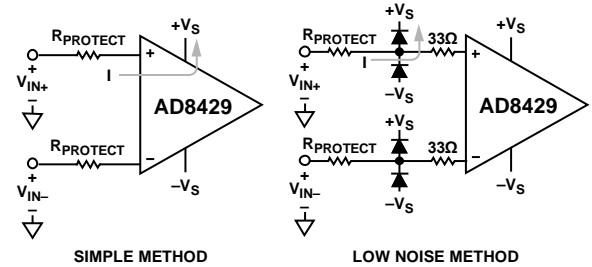


Figure 51. Protection for Voltages Beyond the Rails

#### Large Differential Input Voltage at High Gain

If large differential voltages at high gain are expected, use an external resistor in series with each input to limit current during overload conditions. The limiting resistor at each input can be computed by using the following equation:

$$R_{PROTECT} \geq \frac{1}{2} \left( \frac{|V_{DIFF}| - 1V}{I_{MAX}} - R_G \right)$$

Noise sensitive applications may require a lower protection resistance. Low leakage diode clamps, such as the BAV199, can be used across the inputs to shunt current away from the AD8429 inputs and, therefore, allow smaller protection resistor values.

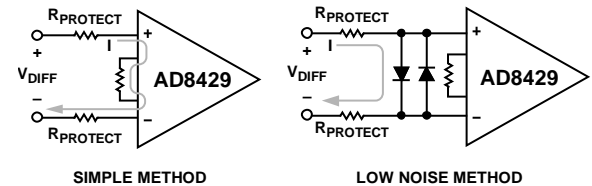


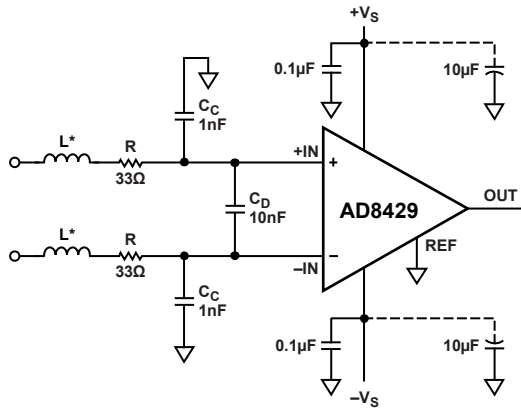
Figure 52. Protection for Large Differential Voltages

#### $I_{MAX}$

The maximum current into the AD8429 inputs,  $I_{MAX}$ , depends on time and temperature. At room temperature, the device can withstand a current of 10 mA for at least one day. This time is cumulative over the life of the device.

#### RADIO FREQUENCY INTERFERENCE (RFI)

RF rectification is often a problem when amplifiers are used in applications that have strong RF signals. The disturbance can appear as a small dc offset voltage. High frequency signals can be filtered with a low-pass RC network placed at the input of the instrumentation amplifier, as shown in Figure 53.



\*CHIP FERRITE BEAD.

Figure 53. RFI Suppression

The filter limits the input signal bandwidth, according to the following relationship:

$$FilterFrequency_{DIFF} = \frac{1}{2\pi R(2C_D + C_C)}$$

$$FilterFrequency_{CM} = \frac{1}{2\pi RC_C}$$

where  $C_D \geq 10 C_C$ .

$C_D$  affects the difference signal, and  $C_C$  affects the common-mode signal. Choose values of  $R$  and  $C_C$  that minimize RFI. A mismatch between  $R \times C_C$  at the positive input and  $R \times C_C$  at the negative input degrades the CMRR of the AD8429. By using a value of  $C_D$  that is one magnitude larger than  $C_C$ , the effect of the mismatch is reduced, and performance is improved.

Resistors add noise; therefore, the choice of resistor and capacitor values depends on the desired tradeoff between noise, input impedance at high frequencies, and RFI immunity. The resistors used for the RFI filter can be the same as those used for input protection.

## CALCULATING THE NOISE OF THE INPUT STAGE

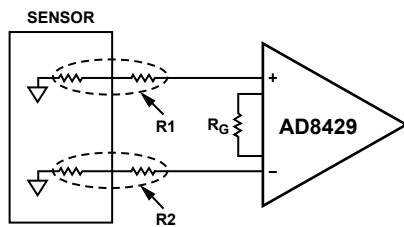


Figure 54. Source Resistance from Sensor and Protection Resistors

The total noise of the amplifier front end depends on much more than the  $1 \text{ nV}/\sqrt{\text{Hz}}$  specification of this data sheet. There are three main contributors: the source resistance, the voltage noise of the instrumentation amplifier, and the current noise of the instrumentation amplifier.

In the following calculations, noise is referred to the input (RTI). In other words, everything is calculated as if it appeared

at the amplifier input. To calculate the noise referred to the amplifier output (RTO), simply multiply the RTI noise by the gain of the instrumentation amplifier.

### Source Resistance Noise

Any sensor connected to the AD8429 has some output resistance. There may also be resistance placed in series with inputs for protection from either overvoltage or radio frequency interference. This combined resistance is labeled  $R_1$  and  $R_2$  in Figure 54. Any resistor, no matter how well made, has an intrinsic level of noise. This noise is proportional to the square root of the resistor value. At room temperature, the value is approximately equal to  $4 \text{ nV}/\sqrt{\text{Hz}} \times \sqrt{(\text{resistor value in k}\Omega)}$ .

For example, assuming that the combined sensor and protection resistance on the positive input is  $4 \text{ k}\Omega$ , and on the negative input is  $1 \text{ k}\Omega$ , the total noise from the input resistance is

$$\sqrt{(4 \times \sqrt{4})^2 + (4 \times \sqrt{1})^2} = \sqrt{64 + 16} = 8.9 \text{ nV}/\sqrt{\text{Hz}}$$

### Voltage Noise of the Instrumentation Amplifier

The voltage noise of the instrumentation amplifier is calculated using three parameters: the device input noise, output noise, and the  $R_G$  resistor noise. It is calculated as follows:

Total Voltage Noise =

$$\sqrt{(\text{Output Noise} / G)^2 + (\text{Input Noise})^2 + (\text{Noise of } R_G \text{ Resistor})^2}$$

For example, for a gain of 100, the gain resistor is  $60.4 \Omega$ . Therefore, the voltage noise of the in-amp is

$$\sqrt{(45/100)^2 + 1^2 + (4 \times \sqrt{0.0604})^2} = 1.5 \text{ nV}/\sqrt{\text{Hz}}$$

### Current Noise of the Instrumentation Amplifier

Current noise is calculated by multiplying the source resistance by the current noise.

For example, if the  $R_1$  source resistance in Figure 54 is  $4 \text{ k}\Omega$ , and the  $R_2$  source resistance is  $1 \text{ k}\Omega$ , the total effect from the current noise is calculated as follows:

$$\sqrt{((4 \times 1.5)^2 + (1 \times 1.5)^2)} = 6.2 \text{ nV}/\sqrt{\text{Hz}}$$

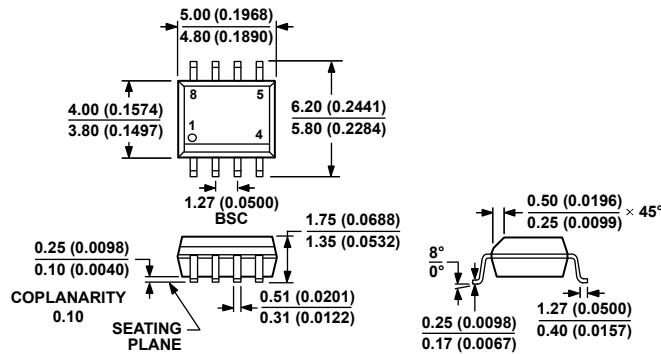
### Total Noise Density Calculation

To determine the total noise of the in-amp, referred to input, combine the source resistance noise, voltage noise, and current noise contribution by the sum of squares method.

For example, if the  $R_1$  source resistance in Figure 54 is  $4 \text{ k}\Omega$ , the  $R_2$  source resistance is  $1 \text{ k}\Omega$ , and the gain of the in-amps is 100, the total noise, referred to input, is

$$\sqrt{8.9^2 + 1.5^2 + 6.2^2} = 11.0 \text{ nV}/\sqrt{\text{Hz}}$$

# OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARDS MS-012-AA  
 CONTROLLING DIMENSIONS ARE IN MILLIMETERS; INCH DIMENSIONS  
 (IN PARENTHESES) ARE ROUNDED-OFF MILLIMETER EQUIVALENTS FOR  
 REFERENCE ONLY AND ARE NOT APPROPRIATE FOR USE IN DESIGN.

012407-A

Figure 55. 8-Lead Standard Small Outline Package [SOIC\_N]  
 Narrow Body  
 (R-8)

Dimensions shown in millimeters and (inches)

## ORDERING GUIDE

Model <sup>1</sup>	Temperature Range	Package Description	Package Option
AD8429ARZ	-40°C to +125°C	8-Lead SOIC_N	R-8
AD8429ARZ-R7	-40°C to +125°C	8-Lead SOIC_N, 7" Tape and Reel	R-8
AD8429BRZ	-40°C to +125°C	8-Lead SOIC_N	R-8
AD8429BRZ-R7	-40°C to +125°C	8-Lead SOIC_N, 7" Tape and Reel	R-8

<sup>1</sup> Z = RoHS Compliant Part.