

# JESD204B Octal Ultrasound AFE with Digital Demodulator

# Data Sheet **[AD9671](http://www.analog.com/AD9671?doc=AD9671.pdf)**

#### <span id="page-0-0"></span>**FEATURES**

**8 channels of LNA, VGA, AAF, ADC, and digital demodulator/ decimator Low power: 150 mW per channel, time gain compensation (TGC) mode, 40 MSPS 62.5 mW per channel, continuous wave (CW) mode; <30 mW in power-down mode 10 mm × 10 mm, 144-ball CSP\_BGA TGC channel input referred noise: 0.82 nV/√Hz, maximum gain Flexible power-down modes Fast recovery from low power standby mode: <2 μs Low noise preamplifier (LNA) Input referred noise: 0.78 nV/√Hz, gain = 21.6 dB Programmable gain: 15.6 dB/17.9 dB/21.6 dB 0.1 dB compression: 1000 mV p-p/750 mV p-p/450 mV p-p Flexible active input impedance matching Variable gain amplifier (VGA) Attenuator range: 45 dB, linear-in-dB gain control Postamplifier (PGA) gain: 21 dB/24 dB/27 dB/30 dB Antialiasing filter (AAF) Programmable, second-order low-pass filter (LPF) from 8 MHz to 18 MHz or 13.5 MHz to 30 MHz and high-pass filter (HPF) Analog-to-digital converter (ADC) Signal-to-noise ratio (SNR): 75 dB, 14 bits up to 125 MSPS JESD204B Subclass 0 coded serial digital outputs CW Doppler (CWD) mode harmonic rejection I/Q demodulator Individual programmable phase rotation Dynamic range per channel: 160 dBFS/√Hz Close-in SNR: 156 dBc/√Hz, 1 kHz offset, −3 dBFS input Digital demodulator/decimator I/Q demodulator with programmable oscillator APPLICATIONS** 

<span id="page-0-1"></span>**Medical imaging/ultrasound Nondestructive testing (NDT)** 

### <span id="page-0-2"></span>**GENERAL DESCRIPTION**

The [AD9671 i](http://www.analog.com/AD9671?doc=AD9671.pdf)s designed for low cost, low power, small size, and ease of use for medical ultrasound applications. It contains eight channels of a VGA with an LNA, a CW harmonic rejection I/Q demodulator with programmable phase rotation, an AAF, an ADC, and a digital demodulator and decimator for data processing and bandwidth reduction.

Each channel features a maximum gain of up to 52 dB, a fully differential signal path, and an active input preamplifier termination. The channel is optimized for high dynamic performance and low power in applications where a small package size is critical.

The LNA has a single-ended to differential gain that is selectable through the serial port interface (SPI). Assuming a 15 MHz noise bandwidth (NBW) and a 21.6 dB LNA gain, the LNA input SNR is 94 dB. In CW Doppler mode, each LNA output drives an I/Q demodulator that has independently programmable phase rotation with 16 phase settings.

Power-down of individual channels is supported to increase battery life for portable applications. Standby mode allows quick power-up for power cycling. In CW Doppler operation, the VGA, AAF, and ADC are powered down. The ADC contains several features designed to maximize flexibility and minimize system cost, such as a programmable clock, data alignment, and programmable digital test pattern generation. The digital test patterns include built-in fixed patterns, built-in pseudorandom patterns, and custom user defined test patterns entered via the SPI.

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1/16-Revision A: Initial Version

## <span id="page-2-0"></span>FUNCTIONAL BLOCK DIAGRAM



## <span id="page-3-0"></span>**SPECIFICATIONS**

### <span id="page-3-1"></span>**AC SPECIFICATIONS**

AVDD1 = 1.8 V, AVDD2 = 3.0 V, DVDD = 1.4 V, DRVDD = 1.8 V, 1.0 V internal ADC reference, full temperature range (0°C to 85°C),  $f_{IN} = 5$  MHz, low bandwidth mode,  $R_S = 50 \Omega$ ,  $R_{FB} = \infty$  (unterminated), LNA gain = 21.6 dB, LNA bias = midhigh, PGA gain = 27 dB, analog gain control, V<sub>GAIN</sub> (V) = (GAIN+) – (GAIN−) = 1.6 V, AAF LPF cutoff = f<sub>SAMPLE</sub>/3 (Mode I/Mode II) = f<sub>SAMPLE</sub>/4.5 (Mode III/ Mode IV), HPF cutoff = LPF cutoff/12.00, Mode I =  $f_{SAMPLE}$  = 40 MSPS, Mode II =  $f_{SAMPLE}$  = 65 MSPS, Mode III =  $f_{SAMPLE}$  = 80 MSPS, Mode IV = 125 MSPS, RF decimator bypassed (Mode I/Mode II), RF decimator enabled (Mode III/Mode IV), digital high-pass filter bypassed, demodulator bypassed, baseband decimator bypassed, JESD204B link parameters: M = 8 and L = 2, unless otherwise noted. All gain setting options are listed, which can be configured via SPI registers, and all power supply currents and power dissipations are listed for the four mode settings (Mode I, Mode II, Mode III, and Mode IV), respectively, via slashes i[n Table 1.](#page-3-2)

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# AD9671 Data Sheet



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<span id="page-6-0"></span>

<sup>1</sup> See th[e AN-835 Application Note,](http://www.analog.com/AN-835?doc=ad9671.pdf) Understanding High Speed ADC Testing and Evaluation, for a complete set of definitions and information about how these tests were completed.

<sup>2</sup> The overrange condition is specified as 6 dB more than the full-scale input range.<br><sup>3</sup> The internal LO frequency, f<sub>io</sub>, is generated from the supplied multiplier local oscillator frequency, f<sub>MLO</sub>, by dividing it up 4, 8, or 16; the MLO signal is named 4LO, 8LO, or 16LO, accordingly.<br><sup>4</sup> Baseband decimation rate  $=$  4 M  $=$  16

 $4$  Baseband decimation rate = 4. M = 16.

### <span id="page-7-0"></span>**DIGITAL SPECIFICATIONS**

AVDD1 = 1.8 V, AVDD2 = 3.0 V, DVDD = 1.4 V, DRVDD = 1.8 V, 1.0 V internal ADC reference, full temperature range (0°C to 85°C), unless otherwise noted.



<span id="page-8-1"></span>

<sup>1</sup> See th[e AN-835 Application Note,](http://www.analog.com/AN-835?doc=ad9671.pdf) Understanding High Speed ADC Testing and Evaluation, for a complete set of definitions and information about how these tests were completed. 2 Specified for LVDS and LVPECL only. 3 Specified for 13 SDIO pins sharing the same connection.

### <span id="page-8-0"></span>**SWITCHING SPECIFICATIONS**

 $AVDD1 = 1.8$  V,  $AVDD2 = 3.0$  V,  $DVDD = 1.4$  V,  $DRVDD = 1.8$  V,  $1.0$  V internal ADC reference,  $L = 2$ ,  $M = 8$ ,  $f_{SAMPLE} = 40$  MHz, lane data rate = 3.2 Gbps, full temperature range (0°C to 85°C), unless otherwise noted.

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<span id="page-9-0"></span>

<sup>1</sup> See th[e AN-835 Application Note,](http://www.analog.com/AN-835?doc=ad9671.pdf) Understanding High Speed ADC Testing and Evaluation, for a complete set of definitions and information about how these tests were completed.

2 Can be adjusted via the SPI.

3 Mode III must have the RF decimator enabled.

4 Mode IV must have the RF decimator enabled.

<sup>5</sup> PLL lock time from 0 Hz to 40 MHz frequency change.

 $6$  Wake-up time is defined as the time required to return to normal operation from power-down mode.

 $7$  The period of the MLO clock signal is represented by  $t_{\text{MLO}}$ .

#### **CLK±, TX\_TRIG± Synchronization Timing Diagram**



**CW Timing Diagram** 



Figure 3. CW Doppler Mode Input MLO±, Continuous Synchronous RESET± Timing, Sampled on the Falling MLO± Edge, 4LO Mode



Figure 4. CW Doppler Mode Input MLO±, Continuous Synchronous RESET± Timing, Sampled on the Falling MLO± Edge, 8LO Mode



Figure 5. CW Doppler Mode Input MLO±, Pulse Synchronous RESET± Timing, 4LO/8LO/16LO Mode



Figure 6. CW Doppler Mode Input MLO±, Pulse Asynchronous RESET± Timing, 4LO/8LO/16LO Mode

## <span id="page-11-0"></span>ABSOLUTE MAXIMUM RATINGS

#### **Table 4.**



Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

#### <span id="page-11-1"></span>**THERMAL IMPEDANCE**

#### **Table 5.Thermal Impedance**



<sup>1</sup> Results are from simulations. Printed circuit board (PCB) is JEDEC multilayer. Thermal performance for actual applications requires careful inspection of the conditions in the application to determine if they are similar to those assumed in these calculations.

#### <span id="page-11-2"></span>**ESD CAUTION**



ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

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## <span id="page-12-0"></span>PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



**NIC = NOT INTERNALLY CONNECTED.**







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11134-008

**Table 6. Pin Function Descriptions** 

Pin No.	<b>Mnemonic</b>	<b>Description</b>			
B5, B6, B8, C5 to C8, D5 to D8, E1, E5 to E8,	<b>GND</b>	Ground. These pins are tied to a quiet analog ground.			
E12, F2, F4, F6, F7, F9, F11, G1, G3, G5 to G8,					
G10, G12, H3 to H6, J4, K1, K2, K4, M1, M12	AVDD1				
F1, F3, F5, F8, F10, F12, G2, G9	<b>DVDD</b>	1.8 V Analog Supply. 1.4 V Digital Supply.			
G4, G11	AVDD <sub>2</sub>	3.0 V Analog Supply.			
E2, E3, E4, E9, E10, E11, J6, K6 <b>B7</b>	<b>CLNA</b>	<b>LNA External Capacitor.</b>			
L1, L12	<b>DRVDD</b>	1.8 V Digital Output Driver Supply.			
C1	LO-E	LNA Analog Inverted Output for Channel E.			
D <sub>1</sub>	LOSW-E	LNA Analog Switched Output for Channel E.			
A1	$LI-E$	LNA Analog Input for Channel E.			
<b>B1</b>	$LG-E$	LNA Ground for Channel E.			
C <sub>2</sub>	$LO-F$	LNA Analog Inverted Output for Channel F.			
D <sub>2</sub>	LOSW-F	LNA Analog Switched Output for Channel F.			
A <sub>2</sub>	$LI-F$	LNA Analog Input for Channel F.			
B <sub>2</sub>	$LG-F$	LNA Ground for Channel F.			
C <sub>3</sub>	$LO-G$	LNA Analog Inverted Output for Channel G.			
D <sub>3</sub>	LOSW-G	LNA Analog Switched Output for Channel G.			
A3	$LI-G$	LNA Analog Input for Channel G.			
B <sub>3</sub>	$LG-G$	LNA Ground for Channel G.			
C4	LO-H	LNA Analog Inverted Output for Channel H.			
D <sub>4</sub>	LOSW-H	LNA Analog Switched Output for Channel H.			
A4	LI-H	LNA Analog Input for Channel H.			
<b>B4</b>	$LG-H$	LNA Ground for Channel H.			
H1	$CLK-$	Clock Input Complement.			
J1	$CLK+$	Clock Input True.			
H <sub>2</sub>	TX_TRIG-	Transmit Trigger Complement.			
J2	TX_TRIG+	Transmit Trigger True.			
H11	ADDR0	Chip Address Bit 0.			
H <sub>10</sub>	ADDR1	Chip Address Bit 1.			
H <sub>9</sub>	ADDR2	Chip Address Bit 2.			
H <sub>8</sub>	ADDR3	Chip Address Bit 3.			
H7	ADDR4	Chip Address Bit 4.			
L2, M2, L3, M3, L10, M10, L11, M11	<b>NIC</b>	Not Internally Connected. These pins are not connected internally. Allow the NIC pins to float, or connect them to ground. Avoid routing high speed signals through these pins because noise coupling may result.			
L4	SYNCINB+	Active Low JESD204B LVDS SYNC Input-True.			
M4	SYNCINB-	Active Low JESD204B LVDS SYNC Input-Complement.			
M <sub>5</sub>	SERDOUT4-	Serial Lane 4 CML Output Data-Complement.			
L5	SERDOUT4+	Serial Lane 4 CML Output Data-True.			
M <sub>6</sub>	SERDOUT3-	Serial Lane 3 CML Output Data-Complement.			
L6	SERDOUT3+	Serial Lane 3 CML Output Data-True.			
M7	SERDOUT2-	Serial Lane 2 CML Output Data-Complement.			
L7	SERDOUT2+	Serial Lane 2 CML Output Data-True.			
M8	SERDOUT1-	Serial Lane 1 CML Output Data-Complement.			
L8	SERDOUT1+	Serial Lane 1 CML Output Data-True.			
M <sub>9</sub>	SYSREF-	Active Low JESD204B LVDS System Reference (SYSREF) Input-Complement.			
L9	SYSREF+	Active Low JESD204B LVDS SYSREF Input-True.			
K11	<b>STBY</b>	Standby Power-Down.			
J11	<b>PDWN</b>	Full Power-Down.			
K12	<b>SCLK</b>	Serial Clock.			
J12	<b>SDIO</b>	Serial Data Input/Output.			
H12	<b>CSB</b>	Chip Select Bar.			



## <span id="page-15-0"></span>TYPICAL PERFORMANCE CHARACTERISTICS

### <span id="page-15-1"></span>**TGC MODE**

Mode I =  $f_{SAMPLE} = 40$  MSPS,  $f_{IN} = 5$  MHz, low bandwidth mode,  $R_S = 50 \Omega$ ,  $R_{FB} = \infty$  (unterminated), LNA gain = 21.6 dB, LNA bias = midhigh, PGA gain = 27 dB,  $V_{GAIN}$  (V) = (GAIN+) – (GAIN–) = 1.6 V, AAF LPF cutoff = fsAMPLE/3, HPF cutoff = LPF cutoff/12.00 (default), RF decimator bypassed, digital demodulator and baseband decimator bypassed, unless otherwise noted.



Figure 11. Gain Error Histogram,  $V_{GAIN} = 0 V$ 

Figure 14. Gain Matching Histogram,  $V_{GAIN} = 1.2$  V









Figure 17. SNR vs. Channel Gain and PGA Gain,  $A_{OUT} = -1.0$  dBFS



Figure 18. SNR vs. Channel Gain and LNA Gain,  $A_{OUT} = -1.0$  dBFS







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Figure 21. Second-Order and Third-Order Harmonic Distortion vs. Input Frequency



Figure 22. Second-Order Harmonic Distortion vs. Channel Gain,  $A_{OUT} = -1.0$  dBFS



Figure 23. Third-Order Harmonic Distortion vs. Channel Gain,  $A_{OUT} = -1.0$  dBFS



Figure 24. Second-Order Harmonic Distortion vs. ADC Output Level (A<sub>OUT</sub>)









Figure 27. LNA Input Impedance Magnitude and Phase, Unterminated







 $R_S = R_{IN} = 100 \Omega$ , LNA Gain = 17.9 dB, PGA Gain = 30 dB, V<sub>GAIN</sub> = 1.6 V

### <span id="page-19-0"></span>**CW DOPPLER MODE**

 $f_{IN} = 5$  MHz,  $f_{LO} = 20$  MHz, 4LO mode,  $R_S = 50 \Omega$ , LNA gain = 21.6 dB, LNA bias = midhigh, all CW channels enabled, phase rotation = 0°.



<span id="page-20-0"></span>

Figure 33. Simplified Block Diagram of a Single Channel

<span id="page-20-2"></span>Each channel in th[e AD9671 c](http://www.analog.com/AD9671?doc=AD9671.pdf)ontains both a TGC signal path and a CW Doppler signal path. Common to both signal paths, the LNA provides four user adjustable input impedance termination options for matching different probe impedances. The CW Doppler path includes an I/Q demodulator with programmable phase rotation needed for analog beamforming. The TGC path includes a differential X-AMP® VGA, an AAF, an ADC, and a digital demodulator and decimator[. Figure 33 s](#page-20-2)hows a simplified block diagram with external components.

### <span id="page-20-1"></span>**TGC OPERATION**

The system gain for TGC operation is distributed as listed in [Table 7.](#page-20-3)

<span id="page-20-3"></span>



Each LNA output is dc-coupled to a VGA input. The VGA consists of an attenuator with a range of −45 dB to 0 dB followed by an amplifier with 21 dB, 24 dB, 27 dB, or 30 dB of gain. The X-AMP gain interpolation technique results in low gain error and uniform bandwidth, and differential signal paths minimize distortion.

The linear in dB gain (law conformance) range of the TGC path is 45 dB. The slope of the gain control interface is 14 dB/V, and the gain control range is −1.6 V to +1.6 V. Equation 1 is the expression for the differential voltage,  $V_{\text{GAIN}}$ , at the gain control interface. Equation 2 is the expression for the VGA attenuation,  $VGA_{ATT}$ , as a function of  $V_{\text{GAN}}$ .

$$
V_{\text{GAIN}}\left(V\right) = \left(\text{GAIN}+\right) - \left(\text{GAIN}-\right) \tag{1}
$$

$$
VGA_{ATT} (dB) = -14 (dB/V) \times (1.6 - V_{GAIN})
$$
 (2)

Then calculate the total channel gain as in Equation 3.

 $ChannelGain(dB) = LNA<sub>GAIN</sub> + VGA<sub>ATT</sub> + PGA<sub>GAIN</sub>$  (3)

In its default condition, the LNA has a gain of 21.6 dB (12×), and the VGA postamplifier gain is 24 dB. If the voltage on the GAIN+ pin is 0 V and the voltage on the GAIN− pin is 1.6 V (44.8 dB attenuation), the total gain of the channel is 0.8 dB if the LNA input is unmatched. The channel gain is −5.2 dB if the LNA is matched to 50  $\Omega$  (R<sub>FB</sub> = 300  $\Omega$ ). However, if the voltage on the GAIN+ pin is 1.6 V and the voltage on the GAIN− pin is 0 V (0 dB attenuation), VGAATT is 0 dB. This results in a total gain of 45.6 dB through the TGC path if the LNA input is unmatched, or in a total gain of 39.6 dB if the LNA input is matched. Similarly, if the LNA input is unmatched and has a gain of 21.6 dB (12×), and the VGA postamp gain is 30 dB, the channel gain is approximately 52 dB with 0 dB VGAATT.

In addition to the analog VGA attenuation described in Equation 2, the attenuation level can be digitally controlled in 3.5 dB increments. Equation 3 is still valid, and the value of  $VGA<sub>ATT</sub>$  is equal to the attenuation level set in Address 0x011, Bits[7:4].

#### **Low Noise Amplifier (LNA)**

Good system sensitivity relies on a proprietary ultralow noise LNA at the beginning of the signal chain, which minimizes the noise contribution in the following VGA. Active impedance control optimizes noise performance for applications that benefit from input impedance matching.

The LNA input, LI-x, is capacitively coupled to the source. An on-chip bias generator establishes dc input bias voltages of approximately 2.2 V and centers the output common-mode levels at 1.5 V (AVDD2 divided by 2). A capacitor, C<sub>LG</sub>, of the same value as the input coupling capacitor, Cs, is connected from the LG-x pin to ground.

The LNA supports three gains, 21.6 dB, 17.9 dB, or 15.6 dB, set through the SPI. Overload protection ensures quick recovery time from large input voltages.

Low value feedback resistors and the current driving capability of the output stage allow the LNA to achieve a low input referred noise voltage of 0.78 nV/ $\sqrt{Hz}$  (at a gain of 21.6 dB). On-chip resistor matching results in precise single-ended gains, which are critical for accurate impedance control. The use of a fully differential topology and negative feedback minimizes distortion. Low second-order harmonic distortion is particularly important in harmonic ultrasound imaging applications.

#### **Active Impedance Matching**

The LNA consists of a single-ended voltage gain amplifier with differential outputs. The negative output is externally available on two output pins, LO-x and LOSW-x, that are controlled via internal switches. This configuration allows the active input impedance synthesis of three different impedance values (and an unterminated value) by connecting up to two external resistances in parallel and controlling the internal switch states via the SPI. For example, with a fixed gain of 8× (17.9 dB), an active input termination is synthesized by connecting a feedback resistor between the negative output pin, LO-x, and the positive input pin, LI-x. This well known technique is used for interfacing multiple probe impedances to a single system. The input resistance (RIN) calculation is shown in Equation 4.

$$
R_{IN} = \frac{(R_{FB1} + 20 \Omega) || (R_{FB2} + 20 \Omega) + 30 \Omega}{(1 + \frac{A}{2})}
$$
(4)

where:

*RFB1* and *RFB2* are the external feedback resistors.

20  $\Omega$  is the internal switch on resistance.

30  $\Omega$  is an internal series resistance common to the two internal switches.

*A*/2 is the single-ended gain or the gain from the LI-x inputs to the LO-x outputs.

 $R_{FB}$  can be equal to  $R_{FB1}$ ,  $R_{FB2}$ , or  $(R_{FB1} + 20 \Omega)||(R_{FB2} + 20 \Omega)$ depending on the connection status of the internal switches.

Because the amplifier has a gain of  $8\times$  from its input to its differential output, it is important to note that the gain, A/2, is the gain from Pin LI-x to Pin LO-x and that it is 6 dB less than the gain of the amplifier, or 12.1 dB  $(4\times)$ . The input resistance is reduced by an internal bias resistor of 6 kΩ in parallel with the source resistance connected to Pin LI-x, with Pin LG-x ac grounded. Use the more accurate Equation 5 to calculate the required  $R_{FB}$  for a desired  $R_{IN}$ , even for higher values of R<sub>IN</sub>.

$$
R_{IN} = \frac{(R_{FB1} + 20 \Omega) || (R_{FB2} + 20 \Omega) + 30 \Omega}{(1 + \frac{A}{2})} || 6 k \Omega
$$
 (5)

For example, to set R<sub>IN</sub> to 200  $\Omega$  with a single-ended LNA gain of 12.1 dB (4×), the value of R<sub>FB1</sub> from Equation 1 must be 950  $\Omega$ while the switch for R<sub>FB2</sub> is open. If the more accurate equation (Equation 5) is used to calculate R<sub>IN</sub>, the value is then 194  $\Omega$ instead of 200 Ω, resulting in a gain error of less than 0.27 dB. Some factors, such as the presence of a dynamic source resistance, may influence the absolute gain accuracy more significantly. At higher frequencies, the input capacitance of the LNA must be considered. The user must determine the level of matching accuracy and adjust RFB accordingly.

RFB is the resulting impedance of the RFB1 and RFB2 combination (se[e Figure 33\)](#page-20-2). Use Register 0x02C in the SPI memory to program th[e AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) for four impedance matching options: three active terminations and unterminated[. Table 8 s](#page-21-0)hows an example of how to select R<sub>FB1</sub> and R<sub>FB2</sub> for 66 Ω, 100 Ω, and 200 Ω input impedance for LNA gain =  $21.6$  dB ( $12\times$ ).

**Table 8. Active Termination Example for LNA Gain = 21.6 dB,**   $R_{FB1} = 650 \Omega$ ,  $R_{FB2} = 1350 \Omega$ 

<span id="page-21-0"></span>

Addr. 0x02C Value	$R_S(\Omega)$	LO-x Switch	LOSW-x <b>Switch</b>	$R_{FB}(\Omega)$	$R_{IN}(\Omega)$ (Eq. 4)
00 (default)	100	On	Off	R <sub>FB1</sub>	100
01	50	On	On	$R_{FB1}$   $R_{FB2}$	66
10	200	Off	On	R <sub>FB2</sub>	200
11	N/A <sup>1</sup>	Off	Off	$\infty$	$\infty$

<sup>1</sup> N/A means not applicable.

The bandwidth (BW) of the LNA is greater than 80 MHz. Ultimately, the BW of the LNA limits the accuracy of the synthesized R<sub>IN</sub>. For R<sub>IN</sub> = R<sub>S</sub> up to about 200  $\Omega$ , the best match is between 100 kHz and 10 MHz, where the lower frequency limit is determined by the size of the ac coupling capacitors, and the upper limit is determined by the LNA BW. Furthermore, the input capacitance and R<sub>s</sub> limit the BW at higher frequencies. [Figure 34 s](#page-21-1)hows  $R_{IN}$  vs. frequency for various values of  $R_{FB}$ .



(Effects of  $R_{SH}$  and  $C_{SH}$  Are Also Shown)

<span id="page-21-1"></span>However, for larger  $R_{IN}$  values, parasitic capacitance starts rolling off the signal BW before the LNA can produce peaking. C<sub>SH</sub> further degrades the match; therefore, do not use C<sub>SH</sub> for values of R<sub>IN</sub> that are greater than 100 Ω.

[Table 9](#page-22-0) lists the recommended values for RFB and C<sub>SH</sub> in terms of R<sub>IN</sub>. C<sub>FB</sub> is needed in series with R<sub>FB</sub> because the dc levels at Pin LO-x and Pin LI-x are unequal.



<span id="page-22-0"></span>**Table 9. Active Termination External Component Values** 

#### **LNA Noise**

The short-circuit noise voltage (input referred noise) is an important limit on system performance. The short-circuit noise voltage for the LNA is 0.78 nV/√Hz at a gain of 21.6 dB, including the VGA noise at a VGA postamp gain of 27 dB. These measurements, which were taken without a feedback resistor, provide the basis for calculating the input noise and noise figure (NF) performance.

[Figure 35 a](#page-22-1)n[d Figure 36](#page-22-2) are simulations of noise figure vs. Rs results with different input configurations and an input referred noise voltage of 2.5 nV/ $\sqrt{Hz}$  for the VGA. Unterminated (R<sub>FB</sub> =  $\infty$ ) operation exhibits the lowest equivalent input noise and noise figure[. Figure 36 s](#page-22-2)hows the noise figure vs. source resistance rising at low RS, where the LNA voltage noise is large compared with the source noise, and at high R<sub>s</sub> due to the noise contribution from R<sub>FB</sub>. The lowest NF is achieved when  $R_s$  matches  $R_{\text{IN}}$ .

[Figure 35 s](#page-22-1)hows the relative noise figure performance. With an LNA gain of 21.6 dB, the input impedance is swept with  $R<sub>s</sub>$  to preserve the match at each point. The noise figures for a source impedance of 50  $\Omega$  are 7 dB, 4 dB, and 2.5 dB for the shunt termination, active termination, and unterminated configurations, respectively. The noise figures for 200  $\Omega$  are 4.5 dB, 1.7 dB, and 1 dB, respectively.



<span id="page-22-1"></span>Figure 35. Noise Figure vs.  $R<sub>S</sub>$  for Shunt Termination, Active Termination Matched and Unterminated Inputs,  $V_{GAIN} = 1.6 V$ 

[Figure 36 s](#page-22-2)hows the noise figure as it relates to  $R<sub>s</sub>$  for various values of R<sub>IN</sub>, which is helpful for design purposes.



Active Termination Matched Inputs,  $V_{GAIN} = 1.6 V$ 

#### <span id="page-22-2"></span>**CLNA Connection**

CLNA (Pin B7) must have a 1 nF capacitor attached to AVDD2.

#### **DC Offset Correction/High-Pass Filter**

The [AD9671](http://www.analog.com/AD9670) LNA architecture is designed to correct for dc offset voltages that can develop on the external  $C_s$  capacitor due to leakage of the Tx/Rx switch during ultrasound transmit cycles. The dc offset correction, as shown i[n Figure 37,](#page-22-3) provides a feedback mechanism to the LG-x input of the LNA to correct for this dc voltage.



Figure 37. Simplified LNA Input Configuration

<span id="page-22-3"></span>The feedback acts as high-pass filter providing dynamic correction of the dc offset. The cutoff frequency of the highpass filter response is dependent on the value of the CLG capacitor, the gain of the LNA (LNA $_{\text{GAN}}$ ) and the trandsconductance ( $g_{\text{m}}$ ) of the feedback transconductance amplifier. The  $g_m$  value is programmed in Register 0x120, Bits[4:3]. Ensure that  $C_s$  is equal to CLG for proper operation.

$-$ work for finger a wood enver convolution we have $\frac{1}{2}$ . The final state of $\frac{1}{2}$									
<b>Address</b> 0x120[4:3]	<b>g</b> <sub>m</sub> (mS)	$LMA_{GAIN} =$ 15.6 dB	$LMAGAIN =$ 17.9 dB	$LMAGAIN =$ 21.6 dB					
00 (default)	0.5	41 kHz	55 kHz	83 kHz					
01	1.0	83 kHz	110 kHz	167 kHz					
10	1.5	133 kHz	178 kHz	267 kHz					
11	2.0	167 kHz	220 kHz	330 kHz					

<span id="page-23-0"></span>Table 10. High-Pass Filter Cutoff Frequency, f<sub>HP</sub>, for C<sub>LG</sub> = 10 nF

For other values of C<sub>LG</sub>, determine the high-pass filter cutoff frequency by scaling the values fro[m Table 10 o](#page-23-0)r calculating based on C<sub>LG</sub>, LNA<sub>GAIN</sub>, and g<sub>m</sub>, as shown in Equation 6.

$$
f_{HP}(C_{LG}) = \frac{1}{2 \times \pi} \times LNA_{GAIN} \times \frac{g_m}{C_{LG}} = f_{HP} \times \frac{10 \text{ nF}}{C_{LG}}
$$
 (6)

where *fHP* is the high-pass filter cutoff frequency (se[e Table 10\)](#page-23-0).

### **Variable Gain Amplifier (VGA)**

The differential X-AMP VGA provides precise input attenuation and interpolation. It has a low input referred noise of 2.5 nV/ $\sqrt{Hz}$  and excellent gain linearity. The VGA is driven by a fully differential input signal from the LNA. The X-AMP architecture produces a linear in dB gain law conformance and low distortion levels—deviating only ±0.5 dB or less from the ideal. The gain slope is monotonic with respect to the control voltage and is stable with variations in process, temperature, and supply. The resulting total gain range is 45 dB, which allows for range loss at the endpoints.

The X-AMP inputs are part of a PGA that completes the VGA. The PGA in the VGA can be programmed to a gain of 21 dB, 24 dB, 27 dB, or 30 dB, allowing optimization of channel gain for different imaging modes in the ultrasound system. The VGA bandwidth is greater than 100 MHz. The input stage is designed to ensure excellent frequency response uniformity across the gain setting. For TGC mode, this input stage minimizes time delay variation across the gain range.

### <span id="page-23-2"></span>**Gain Control**

The analog gain control interface, GAIN±, is a differential input. VGAIN varies the gain of all VGAs through the interpolator by selecting the appropriate input stages connected to the input attenuator. The nominal  $V_{\text{GAN}}$  range is 14 dB/V from  $-1.6$  V to +1.6 V, with the best gain linearity from approximately −1.44 V to +1.44 V, where the error is typically less than ±0.5 dB. For VGAIN voltages of greater than 1.44 V and less than −1.44 V, the error increases. The value of GAIN± can exceed the supply voltage by 1 V without gain foldover.

Gain control response time is typically 750 ns to settle within 10% of the final value for a change from minimum to maximum gain.

The differential input pins, GAIN+ and GAIN−, can interface to an amplifier, as shown i[n Figure 38.](#page-23-1) Decouple and drive the GAIN+ and GAIN− pins to accommodate a 3.2 V full-scale input.



<span id="page-23-1"></span>Use Address 0x011, Bits[7:4], to disable the analog gain control and to control the attenuator digitally. The control range is 45 dB and the step size is 3.5 dB.

### **VGA Noise**

In a typical application, a VGA compresses a wide dynamic range input signal to within the input span of an ADC. The input referred noise of the LNA limits the minimum resolvable input signal, whereas the output referred noise, which depends primarily on the VGA, limits the maximum instantaneous dynamic range that can be processed at any one particular gain control voltage. This latter limit is set in accordance with the total noise floor of the ADC.

The output referred noise is a flat 40 nV/ $\sqrt{Hz}$  (postamp gain = 24 dB) over most of the gain range because it is dominated by the fixed output referred noise of the VGA. At the high end of the gain control range, the noise of the LNA and the source prevail. The input referred noise reaches its minimum value near the maximum gain control voltage, where the input referred contribution of the VGA is miniscule.

At lower gains, the input referred noise and, therefore, the noise figure increase as the gain decreases. The instantaneous dynamic range of the system is not lost, however, because the input capacity increases as the input referred noise increases. The contribution of the ADC noise floor has the same dependence. The important relationship is the magnitude of the VGA output noise floor relative to that of the ADC.

Gain control noise is a concern in very low noise applications. Thermal noise in the gain control interface can modulate the channel gain. The resulting noise is proportional to the output signal level and is usually evident only when a large signal is present. Take care to minimize noise impinging at the GAIN± inputs. Use an external RC filter to remove  $V_{GAN}$  source noise. Ensure that the filter bandwidth is sufficient to accommodate the desired control bandwidth and attenuate unwanted switching noise from the external DACs used to drive the gain control.

The [AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) can bypass the GAIN± inputs and control the gain of the attenuator digitally (see the [Gain Control s](#page-23-2)ection). This mode removes any external noise contributions when active gain control is not needed.

### **Antialiasing Filter (AAF)**

The filter that the signal reaches prior to the ADC is used to reject dc signals and to band limit the signal for antialiasing. The antialiasing filter is a combination of a single-pole, high-pass filter and a second-order, low-pass filter. Configure the highpass filter as a ratio of the low-pass filter cutoff frequency using Address 0x02B, Bits[1:0].

The filter uses on-chip tuning to trim the capacitors and, in turn, to set the desired low-pass cutoff frequency and reduce variations. The default −3 dB low-pass filter cutoff is 1/3, 1/4.5, or 1/6 of the ADC sample clock rate. The cutoff can be scaled to 0.75, 0.8, 0.9, 1.0, 1.13, 1.25, or 1.45 times this frequency using Address 0x00F. The cutoff tolerance  $(\pm 10\%)$  is maintained from 8 MHz to 18 MHz for low bandwidth mode or 13.5 MHz to 30 MHz for high bandwidth mode.

[Table 11 a](#page-24-0)nd [Table 12 c](#page-25-0)alculate the valid SPI-selectable low-pass filter settings and expected cutoff frequencies for the low bandwidth and high bandwidth modes at the minimum sample

frequency and the maximum sample frequency in each speed mode.

Tuning is normally off to avoid changing the capacitor settings during critical times. The tuning circuit is enabled through the SPI. It is disabled automatically after 512 cycles of the ADC sample clock. Initialize the tuning of the filter after initial power-up and after reprogramming of the filter cutoff scaling or the ADC sample rate. The tuning is initiated using Address 0x02B, Bit 6.

Four SPI-programmable settings allow users to vary the highpass filter cutoff frequency as a function of the low-pass cutoff frequency. Two examples are shown in [Table 13:](#page-26-0) an 8 MHz lowpass cutoff frequency and an 18 MHz low-pass cutoff frequency. In both cases, as the ratio decreases, the amount of rejection on the low end frequencies increases. Therefore, making the entire AAF frequency pass band narrow can reduce low frequency noise or maximize dynamic range for harmonic processing.



<span id="page-24-0"></span>



<span id="page-25-0"></span>





#### <span id="page-26-0"></span>**Table 13. High-Pass Filter Cutoff Options**



<sup>1</sup> Ratio = low-pass filter cutoff frequency/high-pass filter cutoff frequency.

#### **AAF/VGA Test Mode**

For debug and testing, there is a bypass switch to view the AAF output on the GPO2 and GPO3 pins. Enable this mode via SPI Address 0x109, Bit 4. The differential AAF output of only one channel can be accessed at a time. The dc output voltage is 1.5 V (or AVDD2/2) and the maximum ac output voltage is 2 V p-p.

#### **ADC**

The [AD9671 u](http://www.analog.com/ad9671?doc=ad9671.pdf)ses a pipelined ADC architecture. The quantized output from each stage is combined into a 14-bit result in the digital correction logic. The pipelined architecture permits the first stage to operate on a new input sample and the remaining stages to operate on preceding samples. Sampling occurs on the rising edge of the clock.

The output staging block aligns the data, corrects errors, and passes the data to the output buffers. The data is then serialized and aligned to the frame and output clocks.

#### **Clock Input Considerations**

For optimum performance, clock th[e AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) sample clock inputs (CLK+ and CLK−) with a differential signal. This signal is typically ac-coupled into the CLK+ and CLK− pins via a transformer or capacitors. These pins are biased internally and require no additional bias.

[Figure 39 s](#page-26-1)hows the preferred method for clocking the [AD9671.](http://www.analog.com/ad9671?doc=ad9671.pdf)  A low jitter clock source, such as the Valpey Fisher oscillator, VFAC3AHL-1 80.000, is converted from single-ended to differential using an RF transformer. The back to back Schottky diodes across the secondary transformer limit clock excursions

into th[e AD9671 t](http://www.analog.com/ad9671?doc=ad9671.pdf)o approximately 0.8 V p-p differential. This limit prevents the large voltage swings of the clock from feeding through to other portions of th[e AD9671,](http://www.analog.com/ad9671?doc=ad9671.pdf) and it preserves the fast rise and fall times of the signal, which are critical to low jitter performance.



<span id="page-26-1"></span>If a low jitter clock is available, another option is to ac couple a

differential positive emitter-coupled logic (PECL) signal to the sample clock input pins, as shown i[n Figure 40.](#page-26-2) Analog Devices, Inc., offers a family of clock drivers with excellent jitter performance, including th[e AD9516-0,](http://www.analog.com/AD9516-0?doc=ad9671.pdf) [AD9516-1,](http://www.analog.com/AD9516-1?doc=ad9671.pdf) [AD9516-2,](http://www.analog.com/AD9516-2?doc=ad9671.pdf) [AD9516-3,](http://www.analog.com/AD9516-3?doc=ad9671.pdf)  an[d AD9516-5 \(](http://www.analog.com/AD9516-5?doc=ad9671.pdf)these five devices are represented by AD9516-x in [Figure 40,](#page-26-2) [Figure 41,](#page-27-0) an[d Figure 42\)](#page-27-1), as well as th[e AD9524.](http://www.analog.com/AD9524?doc=ad9671.pdf) 



<span id="page-26-2"></span>

A third option is to ac couple a differential LVDS signal to the sample clock input pins, as shown i[n Figure 41.](#page-27-0)



Figure 41. Differential LVDS Sample Clock

11134-042

1134-042

<span id="page-27-0"></span>In some applications, it is acceptable to drive the sample clock inputs with a single-ended CMOS signal. In such applications, drive CLK+ directly from a CMOS gate, and bypass the CLK− pin to ground with a 0.1 μF capacitor (se[e Figure 42\)](#page-27-1).



#### <span id="page-27-1"></span>**Clock Duty Cycle Considerations**

Typical high speed ADCs use both clock edges to generate a variety of internal timing signals. As a result, these ADCs can be sensitive to the clock duty cycle. Commonly, a 5% tolerance is required on the clock duty cycle to maintain dynamic performance characteristics. Th[e AD9671 c](http://www.analog.com/ad9671?doc=ad9671.pdf)ontains a duty cycle stabilizer (DCS) that retimes the nonsampling edge, providing an internal clock signal with a nominal 50% duty cycle. This DCS allows a wide range of clock input duty cycles without affecting the performance of th[e AD9671.](http://www.analog.com/ad9671?doc=ad9671.pdf) When the DCS is on, noise and distortion performance are nearly flat for a wide range of duty cycles. However, some applications may require the DCS function to be off. When the DCS function is off, the dynamic range performance can be affected.

The duty cycle stabilizer uses a delay-locked loop (DLL) to create the nonsampling edge. As a result, any changes to the sampling frequency require approximately eight clock cycles to allow the DLL to acquire and lock to the new rate.

#### **Clock Jitter Considerations**

High speed, high resolution ADCs are sensitive to the quality of the clock input. Calculate the degradation in SNR at a given input frequency  $(f_A)$  due only to aperture jitter  $(t_I)$  as follows:

SNR Degradation = 
$$
20 \times \log 10(1/2 \times \pi \times f_A \times t_J)
$$
 (7)

In this equation, the rms aperture jitter represents the root mean square of all jitter sources, including the clock input, analog input signal, and ADC aperture jitter (se[e Figure 43\)](#page-27-2). Treat the clock input as an analog signal in cases where aperture jitter may affect the dynamic range of th[e AD9671.](http://www.analog.com/ad9671?doc=ad9671.pdf) Separate power supplies for clock drivers from the ADC output driver supplies to avoid modulating the clock signal with digital noise. Low jitter, crystal controlled oscillators make the best clock sources, such as the Valpey Fisher VFAC3 series. If the clock is generated from another type of source (by gating, dividing, or other methods), it is retimed by the original clock during the last step.

For more information on how jitter performance relates to ADCs, refer to th[e AN-501 Application Note a](http://www.analog.com/AN-501?doc=AD9671.pdf)nd the [AN-756](http://www.analog.com/AN-756?doc=AD9671.pdf)  [Application Note.](http://www.analog.com/AN-756?doc=AD9671.pdf)



<span id="page-27-2"></span>**Power Dissipation and Power-Down Mode** 

The power dissipated by th[e AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) is proportional to its sample rate. The digital power dissipation does not vary significantly because it is determined primarily by the DRVDD supply and the bias current of the LVDS output drivers. The [AD9671 f](http://www.analog.com/ad9671?doc=ad9671.pdf)eatures scalable LNA bias currents (see [Table 33,](#page-47-0)  Address 0x012). The default LNA bias current settings are midhigh.

By asserting the PDWN pin high, th[e AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) is placed into power-down mode. In this state, the device typically dissipates 5 mW. During power-down, the LVDS output drivers are placed into a high impedance state. Th[e AD9671 r](http://www.analog.com/ad9671?doc=ad9671.pdf)eturns to normal operating mode when the PDWN pin is pulled low. This pin is only 1.8 V tolerant. To drive the PDWN pin from a 3.3 V logic level, insert a 1 kΩ resistor in series with this pin to limit the current.

By asserting the STBY pin high, th[e AD9671 i](http://www.analog.com/ad9671?doc=ad9671.pdf)s placed in standby mode. In this state, the device typically dissipates 725 mW. During standby, the entire device is powered down except the internal references. The LVDS output drivers are placed into a high impedance state. This mode is well suited for applications that require power savings because it allows the device to be powered down when not in use and then quickly powers up. The time to power up the device is also greatly reduced. Th[e AD9671 r](http://www.analog.com/ad9671?doc=ad9671.pdf)eturns to normal operating mode when the STBY pin is pulled low. This pin is only 1.8 V tolerant. To

drive the STBY pin from a 3.3 V logic level, insert a 1 kΩ resistor in series with this pin to limit the current.

In power-down mode, low power dissipation is achieved by shutting down the reference, reference buffer, PLL, and biasing networks. The decoupling capacitors on VREF are discharged when entering power-down mode and must be recharged when returning to normal operation. As a result, the wake-up time is related to the time spent in power-down mode: shorter cycles result in proportionally shorter wake-up times. To restore the device to full operation, approximately 375 μs is required when using the recommended 1 μF and 0.1 μF decoupling capacitors on the VREF pin and the 0.01 μF decoupling capacitors on the GAIN $\pm$  pins. Most of this time is dependent on gain decoupling; higher value decoupling capacitors on the GAIN± pins result in longer wake-up times.

A number of other power-down options are available when using the SPI port interface. The user can individually power down each channel or place the entire device into standby mode. When fast wake-up times are required, standby mode allows the user to keep the internal PLL powered up. The wake-up time is slightly dependent on gain. To achieve a 2 μs wake-up time when the device is in standby mode, apply 0.8 V to the GAIN± pins.

#### **Power and Ground Connection Recommendations**

When connecting power to th[e AD9671,](http://www.analog.com/ad9671?doc=ad9671.pdf) use two separate 1.8 V supplies: one for analog (AVDD1) and one for digital (DRVDD). If only one 1.8 V supply is available, route it to the AVDD1 pin first and then tap it off and isolate it with a ferrite bead or a filter choke preceded by decoupling capacitors for the DRVDD pin.

If the user does not use the digital demodulator/decimator functions for post ADC processing, the DVDD pin can be tied to the 1.8 V DRVDD supply. When this is done, route the DVDD supply first, tap it off, and isolate it with a ferrite bead or filter choke preceded by decoupling capacitors for the DRVDD pin. It is not recommended to use the same supply for AVDD1, DVDD, and DRVDD.

For both high and low frequencies, use several decoupling capacitors on all supplies. Place these capacitors near the point of entry at the PCB level and near the device, with minimal trace lengths.

When using th[e AD9671,](http://www.analog.com/ad9671?doc=ad9671.pdf) a single PCB ground plane is sufficient. With proper decoupling and smart partitioning of the analog, digital, and clock sections of the PCB, optimum performance can be easily achieved.

#### <span id="page-28-1"></span>**Advanced Power Control**

For an ultrasound system, not all channels are needed during all scanning periods. The POWER\_START and POWER\_STOP values in the vector profile can be used to delay the channel

startup and turn the channel off after a certain number of samples. These counters are relative to TX\_TRIG±. The analog circuitry needs to power up before the digital one and the advance time (POWER\_SETUP) for powering up the analog circuitry, before POWER\_START, is set up in Address 0x112 (see [Table 33\)](#page-47-0).



## <span id="page-28-0"></span>**DIGITAL OUTPUTS AND TIMING**

#### **JESD204B Transmit Top Level Description**

The [AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) digital output complies with the JEDEC Standard JESD204B, *Serial Interface for Data Converters*. JESD204B is a protocol to link the [AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) to a digital processing device over a serial interface up to 5 Gbps link speeds. The benefits of the JESD204B interface include a reduction in required board area for data interface routing, and enables smaller packages for converter and logic devices. The [AD9671 s](http://www.analog.com/ad9671?doc=ad9671.pdf)upports single, dual, or quad lane interfaces.

#### <span id="page-28-2"></span>**JESD204B Overview**

The JESD204B data transmit block, as shown in [Figure 45,](#page-29-0)  assembles the parallel channel data from the ADC or digital processing block into frames and uses 8B/10B encoding as well as optional scrambling to form serial output data. Lane synchronization is supported through the use of special characters during the initial establishment of the link, and additional synchronization is embedded in the data stream thereafter. A matching external receiver is required to lock onto the serial data stream and recover the data and clock. For additional details on the JESD204B interface, users are encouraged to refer to the JESD204B standard.

The [AD9671 J](http://www.analog.com/ad9671?doc=ad9671.pdf)ESD204B transmit block maps the eight channel outputs over a link. A link can be configured to use either single, dual, or quad serial differential outputs, which are called lanes. The JESD204B specification refers to a number of parameters to define the link, and these parameters must match between the JESD204B transmitter [\(AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) output) and receiver.

The JESD204B link is described according to the parameters listed i[n Table 14.](#page-29-1)



#### <span id="page-29-1"></span>**Table 14. JESD204B Parameters**



Figure 45[. AD9671 T](http://www.analog.com/ad9671?doc=ad9671.pdf)ransmit Link Simplified Block Diagram

<span id="page-29-0"></span>[Figure 45 s](#page-29-0)hows a simplified block diagram of the [AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) JESD204B link. By default, th[e AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) is configured to use eight channels and four lanes. Channel A and Channel B data is output to SERDOUT1±, Channel C and Channel D data is output to SERDOUT2±, Channel E and Channel F data is output to SERDOUT3±, and Channel G and Channel H data is output to SERDOUT4±. Th[e AD9671 a](http://www.analog.com/ad9671?doc=ad9671.pdf)llows other configurations such as combining the outputs of the eight channels onto a single lane.

By default in th[e AD9671,](http://www.analog.com/ad9671?doc=ad9671.pdf) the 14-bit converter word from each converter is broken into two octets (eight bits of data). Bit 0 (MSB) through Bit 7 are in the first octet. The second octet contains Bit 8 through Bit 13 (LSB) and two tail bits. The tail bits can be configured as zeros or a pseudorandom number sequence.

The two resulting octets can be scrambled. Scrambling is optional but is available to avoid spectral peaks when transmitting similar digital data patterns. The scrambler uses a self synchronizing polynomial-based algorithm defined by the equation:  $1 + x^{14} +$  $x<sup>15</sup>$ . The descrambler in the receiver must be a self synchronizing version of the scrambler polynomial.

The two octets are then encoded with an 8B/10B encoder. The 8B/10B encoder works by taking eight bits of data (an octet) and encoding them into a 10-bit symbol[. Figure 46 s](#page-32-0)hows how the 14-bit data is taken from the ADC, the tail bits are added, the two octets are scrambled, and how the octets are encoded into two 10-bit symbols[. Figure 46 i](#page-32-0)llustrates the default data format.

At the data link layer, in addition to the 8B/10B encoding, the character replacement allows the receiver to monitor frame alignment. The character replacement process occurs on the frame and multiframe boundaries, and implementation depends on which boundary is occurring and if scrambling is enabled.

If scrambling is disabled, the following applies. If the last scrambled octet of the last frame of the multiframe equals the last octet of the previous frame, the transmitter replaces the last octet with the control character  $/A$  = /K28.3/. On other frames within the multiframe, if the last octet in the frame equals the last octet of the previous frame, the transmitter replaces the last octet with the control character /F/ = /K28.7/.

If scrambling is enabled, the following applies. If the last octet of the last frame of the multiframe equals 0x7C, the transmitter replaces the last octet with the control character /A/ = /K28.3/. On other frames within the multiframe, if the last octet equals 0xFC, the transmitter replaces the last octet with the control character  $/F/ =$  /K28.7/.

Refer to JEDEC Standard JESD204B (July 2011) for additional information about the JESD204B interface. Section 5.1 describes the transport layer and data format details, and Section 5.2 describes scrambling and descrambling.

### **JESD204B Synchronization Details**

The [AD9671 i](http://www.analog.com/ad9671?doc=ad9671.pdf)s a JESD204B Subclass 0 device and establishes synchronization of the link through three control signals, TX\_ TRIG, SYSREF, and SYNCINB, and typically a common device clock. SYSREF, TX\_TRIG, and SYNCINB are assumed to be common to all converter devices for alignment purposes at the system level.

The synchronization process is accomplished over three phases: code group synchronization (CGS) phase, initial lane alignment sequence (ILAS) phase, and data transmission phase. Note that if scrambling is enabled, the bits are not actually scrambled until the data transmission phase. The CGS and ILAS phases do not use scrambling.

#### **CGS Phase**

In this phase, the JESD204B transmit block transmits /K28.5/ characters in response to a synchronization request from the receiver (SYNCINB asserted). The receiver (external logic device) must locate K28.5 characters in its input data stream using clock and data recovery (CDR) techniques.

After a certain number of consecutive K28.5 characters are detected on all link lanes, the receiver can optionally initiate a SYS\_REF edge so that th[e AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) transmit data establishes a local multiframe clock (LMFC) internally. The [AD9671 i](http://www.analog.com/ad9671?doc=ad9671.pdf)s a Subclass 0 device that does not mandate SYS\_REF for multidevice synchronization. The use of SYS\_REF reduces the latency variation between devices and reduces the absolute latency of each device to some extent. However, SYS\_REF does not meet the full requirements of a JESD204B Subclass 1 device, and the primary synchronization tool on the [AD9671 i](http://www.analog.com/ad9671?doc=ad9671.pdf)s to use the global TX\_TRIG signal to embed a START\_CODE simultaneously into the data stream for all devices.

After synchronizing all lanes, the receiver or logic device deasserts the SYNCINB signal (SYNCINB± goes high), and the transmitter block begins the ILAS phase, if enabled, on the next internal LMFC boundary.

#### **ILAS Phase**

In the ILAS phase, the transmitter sends out a known pattern and the receiver aligns all lanes of the link and verifies the parameters of the link.

The ILAS phase begins after SYNCINB± is deasserted (goes high). The transmit block begins to transmit four multiframes. Dummy samples are inserted between the required characters so that full multiframes are transmitted.

The four multiframes have the following properties:

- Multiframe 1 begins with an /R/ character (K28.0) and ends with an /A/ character (K28.3).
- Multiframe 2 begins with an /R/ character, followed by a /Q/ (K28.4) character and link configuration parameters over 14 configuration octets (see [Table 15\)](#page-30-0), and ends with an /A/ character. Many of the parameter values are of the notation of the value − 1.
- Multiframe 3 is the same as Multiframe 1.
- Multiframe 4 is the same as Multiframe 1.

#### **Data Transmission Phase**

By the end of the ILAS phase, data transmission starts. Initiating a global TX\_TRIG signal resets any sampling edges within the ADC and replaces a sample with the START\_CODE (see Address 0x18B and Address 0x18C i[n Table 33\)](#page-47-0). Aligning the data on all lanes based on the START\_CODE guarantees the synchronization across multiple lanes and across multiple devices.

In the data transmission phase, frame alignment is monitored with control characters. Character replacement is used at the end of frames. Character replacement in the transmitter occurs in the following instances:

- If scrambling is disabled and the last octet of the frame or multiframe equals the octet value of the previous frame.
- If scrambling is enabled and the last octet of the multiframe is equal to 0x7C, or the last octet of a frame is equal to 0xFC.



### <span id="page-30-0"></span> $T_{\text{A}}$   $T_{\text{A}}$   $T_{\text{A}}$   $T_{\text{A}}$   $T_{\text{A}}$   $T_{\text{A}}$

## AD9671 Data Sheet

#### **Link Setup Parameters**

The following steps demonstrate how to configure th[e AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) JESD204B interface and the outputs.

- 1. Disable lanes before changing the configuration.
- 2. Select the converter and lane configuration.
- 3. Configure the tail bits and control bits.
- 4. Set the lane identification values.
- 5. Set the number of frame per multiframe, K.
- 6. Enable scramble, SCR.
- 7. Set the lane synchronization options.
- 8. Verify FCHK, checksum of JESD204B interface parameters.
- 9. Set additional digital output configuration options.
- 10. Reenable lane(s) after configuration.

### **Disable Lanes**

Before modifying the JESD204B link parameters, disable the link and hold it in reset. This is accomplished by writing a Logic 1 to Address 0x142, Bit 0.

### **Converter and Lane Configuration**

If the digital demodulator/decimator is disabled, the JESD204B M parameter (number of converters) is set to 8 (Address  $0x153 =$ 0x07). Otherwise  $M = 16$  when the channel output is complex data.

The lane configuration is set in Address 0x150, Bits[1:0] such that  $00 =$  one lane per link,  $01 =$  two lanes per link, or  $11 =$  four lanes per link. The channel data (A to H) is placed on the JESD204B lanes accordin[g Table 16.](#page-31-0) 

#### <span id="page-31-0"></span>**Table 16. Channel to JESD204B Lane Mapping**



### **Configure the Tail Bits and Control Bits**

With  $N' = 16$  and  $N = 14$ , two tail bits are available per sample for transmitting additional information over the JESD204B link. Tail bits are dummy bits sent over the link to complete the two octets and do not convey any information about the input signal. Tail bits can be fixed zeros (default) or pseudorandom numbers (Address 0x142, Bit 6).

### **Set Lane Identification Values**

JESD204B allows parameters to identify the device and lane. These parameters are transmitted during the ILAS phase, and they are accessible in the internal registers.

There are three identification values: device identification (DID), bank identification (BID), and lane identification (LID). DID and BID are device specific; therefore, they can be used for link identification.





### **Set Number of Frames per Multiframe, K**

Per the JESD204B specification, a multiframe is defined as a group of K successive frames, where K is between 1 and 32, and it requires that the number of octets be between 17 and 1024. The K value is set to 32 by default in Register 0x152, Bits[4:0]. Note that Register 0x152 represents a value of  $K - 1$ .

The K value can be changed; however, it must comply with a few conditions. The [AD9671 u](http://www.analog.com/ad9671?doc=ad9671.pdf)ses a fixed value for octets per frame, F. K must also be a multiple of 4 and conform to the following equation:

### $32 \ge K \ge$  Ceil (17/*F*)

The JESD204B specification also requires that the number of octets per multiframe  $(K \times F)$  be between 17 and 1024. The F value is fixed based on the value of M and L. F can be read from Address 0x151.

$$
F = \frac{M \times 2}{L}
$$

### **Enable Scramble, SCR**

Scrambling can be enabled or disabled by setting Address 0x150, Bit 7. By default, scrambling is enabled. Per the JESD204B protocol, scrambling is only functional after the lane synchronization is complete.

### **Set Lane Synchronization Options**

Most of the synchronization features of the JESD204B interface are enabled by default for typical applications. In some cases, these features can be disabled or modified as follows.

ILAS enabling is controlled in Address 0x142, Bits[3:2] and is enabled by default. Optionally, to support some unique instances of the interfaces (such as NMCDA-SL), the JESD204B interface can be programmed to either disable the ILAS sequence or continually repeat the ILAS sequence. Additionally, the ILAS can be repeated for a fixed count, as programmed in Address 0x145, Bits[7:0].

The [AD9671 h](http://www.analog.com/ad9671?doc=ad9671.pdf)as fixed values of some of the JESD204B interface parameters, and they are as follows:

- $N' = 16$ : number of bits per sample is 16. Read only value from Address 0x155, Bits[3:0] = 15 (N' – 1).
- CF = 0: number of control words per frame clock cycle per converter is 0, in Address 0x157, Bits[4:0].

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The [AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) calculates values for some JESD204B parameters based on other settings, particularly the quick configuration register selection. The following read only values are available in the register map for verification:

- F: octets per frame can be 32, 16, 8, or 4; read the value (F − 1) from Address 0x151, Bits[4:0]
- M: number of converters per link can be 8 or 16; read the value (M − 1) from Address 0x153, Bits[3:0]
- S: samples per converter per frame is 1 by default; read the value  $(S - 1)$  from Address 0x156, Bit 0.

### **Verify FCHK, Checksum of JESD204B Interface Parameters**

The JESD204B parameters can be verified through a checksum value (FCHK) of the JESD204B interface parameters. Each lane has a FCHK value associated with it. The FCHK value is transmitted during the ILAS second multiframe and can be read from the internal registers.

Checksum value is the modulo 256 sum of the parameters listed as Octet 0 to Octet 10 in [Table 18.](#page-32-1) Checksum is calculated by adding the parameter fields before they are packed into the octets.

The FCHK value for the lane configuration for data coming out of SERDOUT1± can be read from Address 0x15A. Similarly, FCHK for the lane defined for SERDOUT2± can be read from Address 0x15B.

<span id="page-32-1"></span>



#### **Set Additional Digital Output Configuration Options**

The JESD204B outputs are configured by default to produce a peak differential voltage of 262 mV. This voltage satisfies the JESD204B specification for a transmit eye mask for an LV-OIF-11G-SR-based operation target of between 180 mV and 385 mV peak differential voltage, but other peak differential voltages can be accommodated. Address 0x015, Bits[6:4] settings allow output peak voltages. Additional options include the following:

- Invert polarity of the serial output data: Address 0x014, Bit 2
- Flip (mirror) 10-bit word before output: Address 0x143, Bit 0
- Channel data format (offset binary, twos complement, gray code): Address 0x014, Bits[1:0]
- Options for interpreting the signal on the SYNCINB± pin: Address 0x156, Bit 5

#### **Reenable Lanes After Configuration**

After modifying the JESD204B link parameters, enable the link and then the synchronization process can begin. This enable is accomplished by writing a Logic 0 to Address 0x142, Bit 0.

<span id="page-32-0"></span>

Figure 46[. AD9671 D](http://www.analog.com/ad9671?doc=ad9671.pdf)igital Processing of JESD204B Lanes



<span id="page-33-0"></span>

#### **Frame and Lane Alignment Monitoring and Correction**

Frame alignment monitoring and correction is part of the JESD204B specification. The 14-bit word requires two octets to transmit all the data. The two octets (MSB and LSB), where  $F = 2$ , make up a frame. During normal operating conditions frame alignment is monitored via alignment characters that are inserted under certain conditions at the end of a frame. [Table 19](#page-33-0)  summarizes the conditions for character insertion along with the expected characters under the various operation modes. If lane synchronization is enabled, the replacement character value depends on whether the octet is at the end of a frame or at the end of a multiframe.

Based on the operating mode, the receiver can ensure that it is still synchronized to the frame boundary by correctly receiving the replacement characters.

#### **Super Frame and Output Zero Stuffing**

To handle the various decimation rates and to handle complex (IQ) vs. real samples, a wrapper around the JESD204B transmitter was created. Each word in the standard JESD204B frame represents a word in the super frame. However, in most cases, the frame boundary for the super-frame does not occur at the same time as the JESD204B frame boundary.

As the decimation rates increase, relatively large amounts of zero stuffing can occur. The zero stuffer can be configured to add additional codes into the data stream to facilitate super frame synchronization.

It is highly recommended to configure the device to autocalculate the size of the JESD204B and the super frames.

#### **Digital Outputs and Timing**

The [AD9671 h](http://www.analog.com/ad9671?doc=ad9671.pdf)as differential digital outputs that power up by default. The driver current is derived on chip and sets the output current at each output equal to a nominal 3 mA. Each output presents a 100  $\Omega$  dynamic internal termination to reduce unwanted reflections.

Th[e AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) digital outputs can interface with custom ASICs and FPGA receivers, providing superior switching performance in noisy environments. Single point-to-point network topologies are recommended with a single differential 100 Ω termination resistor placed as close to the receiver logic as possible.

For receiver inputs that provide their own common-mode bias, or whose input common-mode requirements are not within the bounds of th[e AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) DRVDD supply, use an ac-coupled

connection as shown i[n Figure 47.](#page-33-1) Place a 0.1 μF series capacitor on each output pin and use a 100  $\Omega$  differential termination close to the receiver side. The 100  $Ω$  differential termination results in a nominal 600 mV p-p differential swing at the receiver. In the case where the receiver inputs do not provide their own common-mode bias, single-ended 50  $\Omega$ terminations can be used. When single-ended terminations are used, the termination voltage ( $V_{\text{RXCM}}$ ) must be chosen to match the input requirements of the receiver.

For receivers whose input common-mode voltage requirements match the output common-mode voltage (DRVDD/2) of the [AD9671,](http://www.analog.com/ad9671?doc=ad9671.pdf) a dc-coupled connection can be used. The common mode of the digital output automatically biases itself to half of DRVDD  $(0.9 V for DRVDD = 1.8 V)$  (see [Figure 48\)](#page-33-2).

If there is no far end receiver termination or if there is poor differential trace routing, timing errors may result. To avoid such timing errors, it is recommended that the trace length be less than six inches and that the differential output traces be adjacent and at equal lengths.

[Figure 49](#page-34-0) throug[h Figure 54 s](#page-34-1)how examples of the digital output (default) data eyes, time interval error (TIE) jitter histograms, and bathtub curves.

<span id="page-33-2"></span><span id="page-33-1"></span>

#### **MASK HITS1: EYE DIAGRAM 400 1 – 300 200 100** VOLTAGE (mV) **VOLTAGE (mV) 0 –100 –200 –300 EYE: ALL BITS OFFSET: 0.0018 MASK: TEMP\_MSK ULS: 8000; 993330, TOTAL: 8000; 993330** 11134-149 **–400** 11134-149 **–400 –200 0 200 400 TIME (ps)**

<span id="page-34-0"></span>Figure 49. Digital Outputs Data Eye, External 100 Ω Terminations at 2.5 Gbps



Figure 50. Digital Outputs Histogram, External 100 Ω Terminations at 2.5 Gbps





Figure 52. Digital Outputs Data Eye, External 100 Ω Terminations at 5.0 Gbps



Figure 53. Digital Outputs Histogram, External 100 Ω Terminations at 5.0 Gbps

<span id="page-34-1"></span>

Additional SPI options allow the user to further increase the output driver voltage swing of all four outputs to drive longer trace lengths (see Address 0x015 in [Table 33\)](#page-47-0). Even though this produces sharper rise and fall times on the data edges and is less prone to bit errors, the power dissipation of the DRVDD supply increases when this option is used. See the Memory Map section for more details.

#### **Preemphasis**

Preemphasis enables the receiver eye diagram mask to be met in conditions where the interconnect insertion loss is not in accordance with the JESD204B specification. In conditions where preemphasis is not needed to achieve sufficient signal integrity for the link, it is best to disable the preemphasis to conserve power. Enabling preemphasis on a short link and increasing the deemphasis value too high may cause the receiver eye diagram to fail in cases where it passes with no de-emphasis. The transmitter eye diagram does not necessarily pass when preemphasis is enabled. Furthermore, using more preemphasis than necessary may increase EMI; therefore, consider EMI when choosing an insertion loss compensation strategy. To enable preemphasis, write a Logic 1 to Address 0x015, Bit 1.

There are several methods to select test data patterns on the JESD204B link, as shown i[n Figure 55.](#page-36-0) These methods serve different purposes in the testing process of establishing the link.

The processed samples from the ADC can be replaced by nine digital output test pattern options. The replacement is initiated through the SPI using Address 0x00D, Bits[3:0]. These options are useful when validating receiver capture and timing. See [Table 21 f](#page-36-1)or the output test mode bit sequencing options. Some test patterns have two serial sequential words, which the user can alternate in various ways, depending on the test pattern chosen. Note that some patterns may not adhere to the data format select option. In addition, custom user defined test

patterns are assigned in the user pattern registers (Address 0x019 through Address 0x020). All test mode options except PN sequence short and PN sequence long can support 8-bit to 14-bit word lengths to verify data capture to the receiver.

The PN sequence short pattern produces a pseudorandom bit sequence that repeats itself every  $2^9 - 1$  bits, or 511 bits. For a description of the PN sequence short pattern and how it is generated, see Section 5.1 of the ITU-T O.150 (05/96) standard. The only difference from the standard is that the starting value is a specific value instead of all 1s (see [Table 20 f](#page-35-0)or the initial values).

The PN sequence long pattern produces a pseudorandom bit sequence that repeats itself every  $2^{23} - 1$  bits, or 8,388,607 bits. For a description of the PN sequence long pattern and how it is generated, see Section 5.6 of the ITU-T O.150 (05/96) standard. The only differences from the standard are that the starting value is a specific value instead of all 1s and that th[e AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) inverts the bit stream (se[e Table 20 f](#page-35-0)or the initial values). The output sample size depends on the selected bit length.

#### <span id="page-35-0"></span>**Table 20. PN Sequence Initial Values**



See the [Memory Map s](#page-45-0)ection for information on how to change these additional digital output timing features through the SPI.

Test patterns are initiated at the input of the scrambler block by setting Address  $0x144$ , Bits[5:4] = 10 or at the output of the 8B/10B encoder by setting Address 0x144, Bits $[5:4] = 01$ . The test pattern generated is selected in Address 0x144, Bits[3:0], and is specified i[n Table 22.](#page-36-2) 

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#### **Digital Output Test Patterns**





#### <span id="page-36-1"></span><span id="page-36-0"></span>**Table 21. Flexible Output Test Modes—Address 0x00D**



#### <span id="page-36-2"></span>**Table 22. Flexible Output Test Modes—Address 0x144**



### **SDIO Pin**

The SDIO pin is required to operate the SPI. The SDIO pin has an internal 30 kΩ pull-down resistor that pulls it low and is only 1.8 V tolerant. To drive the SDIO pin from a 3.3 V logic level, insert a 1 kΩ resistor in series with this pin to limit the current.

### **SCLK Pin**

The SCLK pin is required to operate the SPI. The SCLK pin has an internal 30 kΩ pull-down resistor that pulls it low and is only 1.8 V tolerant. To drive the SCLK pin from a 3.3 V logic level, insert a 1 kΩ resistor in series with this pin to limit the current.

#### **CSB Pin**

The CSB pin is required to operate the SPI. The CSB pin has an internal 70 k $\Omega$  pull-up resistor that pulls it high and is only 1.8 V tolerant. To drive the CSB pin from a 3.3 V logic level, insert a 1 kΩ resistor in series with this pin to limit the current.

### **RBIAS Pin**

To set the internal core bias current of the ADC, place a resistor nominally equal to 10.0 k $\Omega$  to ground at the RBIAS pin. Using a resistor other than the recommended 10.0 kΩ resistor for RBIAS degrades the performance of the device. Therefore, use at least a 1% tolerance on this resistor to achieve consistent performance.

#### **VREF Pin**

A stable and accurate 0.5 V voltage reference is built into the [AD9671](http://www.analog.com/AD9674?doc=AD9674.pdf). This voltage reference is amplified internally by a factor of 2, setting VREF to 1.0 V, which results in a full-scale differential input span of 2.0 V p-p for the ADC. VREF is set internally by default, but the user can drive the VREF pin externally with a 1.0 V reference to achieve more accuracy. However, th[e AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) does not support ADC full-scale ranges less than 2.0 V p-p.

When applying the decoupling capacitors to the VREF pin, use ceramic, low equivalent series resistance (ESR) capacitors. Ensure that these capacitors are near the reference pin and on the same layer of the PCB as th[e AD9671](http://www.analog.com/AD9674?doc=AD9674.pdf). The VREF pin must have both a 0.1 μF capacitor and a 1 μF capacitor that are connected in parallel to analog ground. These capacitor values are recommended for the ADC to properly settle and acquire the next valid sample.

### **GPOx Pins**

Use the general-purpose output pins, GPO0, GPO1, GPO2, and GPO3, in a system to provide programmable inputs to other chips in the system. The value of each pin is set via Address 0x00E to either Logic 0 or Logic 1 (se[e Table 33\)](#page-47-0).

### **ADDRx Pins**

Use the chip address pins to address individua[l AD9671 d](http://www.analog.com/ad9671?doc=ad9671.pdf)evices in a system. Chip address mode is enabled using Address 0x115, Bit 5 (see [Table 33\)](#page-47-0). If the value written to Bits[4:0] matches the value on the chip address bit pins (ADDR4 to ADDR0), the device is selected and any subsequent SPI writes or reads to addresses indicated as chip registers are written only to that device. If chip address mode is disabled, write all addresses regardless of the value on the address pins.

### **TX\_TRIG± Pins**

The TX\_TRIG± function has several uses within th[e AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) and is initiated with an external hardware trigger either on the TX\_ TRIG± pins or by a software trigger by setting Address 0x10C, Bit 5 to 1. The hardware trigger has the advantage of guaranteed synchronous triggering of multiple [AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) devices in a system. The setup and hold time for each TX\_TRIG± hardware input is given i[n Table 3 a](#page-8-2)s 1 ns. Due to the asynchronous SPI function, the software trigger cannot guarantee synchronization of multiple [AD9671 d](http://www.analog.com/ad9671?doc=ad9671.pdf)evices. If the TX\_TRIG± hardware trigger is not used, tie the TX\_TRIG± pins in a low logic state.

The TX\_TRIG± function is used to reset circuits in the digital demodulator and decimator (see the [Baseband Demodulator](#page-41-0)  [and Decimator](#page-41-0) section), initiate the advanced power mode (see the [Advanced Power Control](#page-28-1) section), and synchronize the data serialization in the JESD204B block (see the [JESD204B](#page-28-2)  [Overview](#page-28-2) section).

### <span id="page-37-0"></span>**ANALOG TEST TONE GENERATION**

The [AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) can generate analog test tones that the user can then switch to the input of the LNA of each channel for channel gain calibration. The test tone amplitude at the LNA output is dependent on LNA gain, as shown i[n Table 23.](#page-37-1) 

<span id="page-37-1"></span>**Table 23. Test Signal Fundamental Amplitude at LNA Output** 

Address 0x116[3:2], <b>Analog Test Tones</b>	<b>LNA Gain</b> 15.6 dB	<b>LNA Gain</b> 17.9 dB	<b>LNA Gain</b> 21.6 dB
00 (default)	80 mV p-p	98 mV p-p	119 mV p-p
01	160 mV p-p	196 mV p-p	238 mV p-p
10	320 mV p-p	391 mV p-p	476 mV p-p
11	Reserved	Reserved	Reserved

Calculate the test signal amplitude at the input to the ADC given the LNA gain, attenuator control voltage, and the PGA gain[. Table 24](#page-37-2) an[d Table 25](#page-37-3) list example calculations.

<span id="page-37-2"></span>



<span id="page-37-3"></span>



### <span id="page-38-0"></span>**CW DOPPLER OPERATION**

Each channel of th[e AD9671 i](http://www.analog.com/ad9671?doc=ad9671.pdf)ncludes an I/Q demodulator. Each demodulator has an individual programmable phase shifter. The I/Q demodulator is ideal for phased array beamforming applications in medical ultrasound. Each channel can be programmed for 16 phase settings/360° (or 22.5°/step), selectable via the SPI port. The device has a RESET± input that is used to synchronize the LO dividers of each channel. If multipl[e AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) devices are used, a common reset across the array ensures a synchronized phase for all channels. If the RESET± input is not used, tie each input pin to ground. Internal to th[e AD9671,](http://www.analog.com/ad9671?doc=ad9671.pdf) the individual Channel I and Channel Q outputs are current summed. If multiple [AD9671 d](http://www.analog.com/ad9671?doc=ad9671.pdf)evices are used, current sum and convert the I and Q outputs from each [AD9671 t](http://www.analog.com/ad9671?doc=ad9671.pdf)o a voltage using an external transimpedance amplifier.

#### **Quadrature Generation**

The internal 0° and 90° LO phases are digitally generated by a divide-by-M logic circuit, where M is 4, 8, or 16. The internal divider is selected via Address 0x02E, Bits[2:0] (se[e Table 33\)](#page-47-0). The divider is dc-coupled and inherently broadband; the maximum LO frequency is limited only by its switching speed. Ensure that the duty cycle of the quadrature LO signals is as near 50% as possible for the 4LO and 8LO modes. The 16LO mode does not require a 50% duty cycle. Furthermore, the divider is implemented such that the MLO signal reclocks the final flip-flops that generate the internal LO signals and thereby minimizes noise introduced by the divide circuitry.

For optimum performance, the MLO signal input is driven differentially, as on th[e AD9671 e](http://www.analog.com/ad9671?doc=ad9671.pdf)valuation board. The commonmode voltage on each pin is approximately 1.2 V with the nominal 3 V supply. It is important to ensure that the MLO source have very low phase noise (jitter), a fast slew rate, and an adequate input level to obtain optimum performance of the CW signal chain.

Beamforming applications require a precise channel-to-channel phase relationship for coherence among multiple channels. The RESET<sup> $\pm$ </sup> input is provided to synchronize the LO divider circuits in differen[t AD9671 d](http://www.analog.com/ad9671?doc=ad9671.pdf)evices when they are used in arrays. The RESET± input is a synchronous edge-triggered input that resets the dividers to a known state after power is applied to multiple [AD9671 d](http://www.analog.com/ad9671?doc=ad9671.pdf)evices. The RESET± signal can be either a continuous signal or a single pulse, and it can be either synchronized with the MLO± clock edge (recommended) or it can be asynchronous. If a

continuous signal is used for the RESET± then it has to be at the LO rate. For synchronous RESET±, the device can be configured to sample the RESET± signal with either the falling or rising edge of the MLO± clock, which makes it easier to align the RESET± signal with the opposite MLO± clock edge. Register 0x02E is used to configure the RESET signal behavior. Synchronize the RESET± input to the MLO signal input. Achieve accurate channel-tochannel phase matching via a common clock on the RESET± input when using more than on[e AD9671.](http://www.analog.com/ad9671?doc=ad9671.pdf) 

### **I/Q Demodulator and Phase Shifter**

The I/Q demodulators consist of double-balanced, harmonic rejection, passive mixers. The RF input signals are converted into currents by transconductance stages that have a maximum differential input signal capability of matching the LNA output full scale. These currents are then presented to the mixers that convert them to baseband ( $RF - LO$ ) and  $2 \times RF$  ( $RF + LO$ ). The signals are phase shifted according to the codes that are programmed into the SPI latch (see [Table 26\)](#page-38-1). The phase shift function is an integral part of the overall circuit. The phase shift listed i[n Table 26 i](#page-38-1)s defined as being between the baseband I or Q channel outputs. As an example, for a common signal applied to a pair of RF inputs to a[n AD9671,](http://www.analog.com/ad9671?doc=ad9671.pdf) the baseband outputs are in phase for matching phase codes. However, if the phase code for Channel 1 is 0000 and the phase code for Channel 2 is 0001, Channel 2 leads Channel 1 by 22.5°.

<span id="page-38-1"></span>



## <span id="page-39-0"></span>DIGITAL DEMODULATOR/DECIMATOR

The [AD9671 c](http://www.analog.com/ad9671?doc=ad9671.pdf)ontains digital processing capability. Each channel has three stages of processing that are available: RF decimator, baseband (BB) demodulator, and baseband decimator. For test purposes, the input to the demodulator/ decimator can serve as a test waveform. Normally, the input is the output of the ADC. The output of the demodulator/decimator is sent to the framer/serializer for output formatting.

The maximum data rate of the BB demodulator and decimator is 65 MSPS. Therefore, if the sample of the ADC is greater than 65 MSPS, enable the RF decimator (fixed rate of 2). The ADC resolution is 14 bits. The maximum resolution at the output of the digital processing is 16 bits. Saturation of the ADC is determined after the dc offset calibration to ensure maximum dynamic range. Depending on decimation rate, the loss in output SNR due to truncation to 16 bits is negligible.

### <span id="page-39-1"></span>**VECTOR PROFILE**

To minimize the time needed to reconfigure device settings during operation, the device supports configuration profiles. The user can store up to 32 profiles in the device. A profile is selected by a 5-bit index. A profile consists of a 64-bit vector, as described i[n Table 27.](#page-39-2) Each parameter is concatenated to form the 64-bit profile vector. The profile memory starts at Register 0xF00 and ends at Register 0xFFF. Write the memory in either stream or address selected data mode. However, the user must read the memory using stream mode. When writing or reading in

stream mode while the SPI configuration is set to MSB first mode (default setting for Register 0x000), the write/read address needs to refer to the last register address, not the first one. For example, when writing or reading the first profile that spans the address space between Register 0xF00 and Register 0xF07, with the SPI port configured as MSB first, the referenced address must be Register 0xF07 to allow reading or writing the 64 profile bits in MSB mode. For more information about stream mode, see the [AN-877 Application Note,](http://www.analog.com/an-877?doc=AD9671.pdf) *Interfacing to High Speed ADCs via SPI*.

There is a buffer used to store the current profile data. When the profile index is written in Register 0x10C, the selected profile is read from memory and stored in the current profile buffer. The profile memory is read/written in the SPI clock domain. After the SPI writes the profile index value, it takes four SPI clock cycles to read the profile from RAM and store it in the current profile buffer. If the SPI is in LSB mode, these additional SPI clock cycles are provided when the profile index register is written. If the SPI is in MSB mode, an additional byte must be read or written to update the profile buffer.

Updating profile memory does not affect the data in the profile buffer. The profile index register must be written to cause a refresh of the current profile data, even if the profile index register is written with the same value.



Figure 56. Simplified Block Diagram of a Single Channel of Demodulator/Decimator

<span id="page-39-2"></span>



### <span id="page-40-0"></span>**RF DECIMATOR**

The input to the RF decimator is either the ADC output data or a test waveform, as described in th[e Digital Test Waveforms](#page-42-0) section. The test waveforms are enabled per channel using Address 0x11A (see [Table 33\)](#page-47-0).

### **DC Offset Calibration**

The user can reduce dc offset through a manual system calibration process. Measure the dc offset of every channel in the system and then set a calibration value using Address 0x110 and Address 0x111. Note that these registers are both chip and local addresses, meaning that they are accessed using the chip address and device index. Bypass the dc offset calibration using Address 0x10F, Bits[2:0].

### **Multiband AAF and Decimate by 2**

The multiband filter is a finite impulse response (FIR) filter. It is programmable with low or high bandwidth filtering. The filter requires 11 input samples to populate the filter. The decimation rate is fixed at  $2\times$ . Therefore, the decimation frequency is  $f_{DEC}$  = f<sub>SAMPLE</sub>/2[. Figure 57](#page-40-1) an[d Figure 58](#page-41-1) show the frequency response of the filter, depending on the mode[. Figure 57](#page-40-1) shows the attenuation amplitude over the Nyquist frequency range. [Figure 58 s](#page-41-1)hows the pass band response as nearly flat.



<span id="page-40-1"></span>Figure 57. AAF Frequency Response (Frequency Scale Assumes  $f_{ADC} = 2 \times f_{DEC} = 40 MHz$ 



<span id="page-41-1"></span> $f_{ADC} = 2 \times f_{DEC} = 40 MHz$ 

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### **High-Pass Filter**

The user can apply a second-order Butterworth, high-pass infinite impulse response (IIR) filter after the RF decimator. The filter has a cutoff of 700 kHz for an encode clock of 50 MHz. The filter has a settling time of 2.5 μs. Therefore, if the ADC clock is 50 MHz, ignore the first 125 samples (2.5 μs/0.02 μs). Bypass or enable the filter in the vector profile if the filter is enabled in Register 0x113, Bit 5. If the filter is bypassed by setting Register  $0x113$ , Bit  $5 = 1$ , the filter cannot be enabled from the vector profile.

### <span id="page-41-0"></span>**BASEBAND DEMODULATOR AND DECIMATOR**

The demodulator downconverts the RF signal to a baseband quadrature signal. The excess oversampling is reduced by the decimator.

#### **Numerically Controlled Oscillator**

The numerically controlled oscillator (NCO) generates I and Q signals (cos and –sin) for the demodulator. A division of the effective sample clock generates the oscillator frequency. If the RF decimator is bypassed, the effective sample clock is the same as the ADC clock. If the RF decimator is enabled, the effective clock rate is ½ the ADC sample clock frequency. The divider is set in the vector profile. The oscillator has a frequency resolution of 1 kHz. To synchronize different devices, the NCO is reset upon assertion of TX\_TRIG±.

### **Decimation Filter**

The purpose of the decimation filter is to band limit the demodulated signal prior to decimation. The filter is a polyphase FIR filter and uses 16 taps per decimation with symmetrical coefficients. Therefore, there are eight unique 14-bit coefficients per decimation. The decimation rate and a pointer to the coefficients used by the filter are set in the vector profile. Digital gain from 1 to 128 is applied to the filter response. The digital gain compensation is set in the vector profile.

The filter is reset upon assertion of TX\_TRIG±. The decimation filter takes  $32\times$  the decimation input samples or 32 output samples to populate.

#### **Coefficient Memory**

The coefficient memory stores the eight coefficients per decimation, with a maximum decimation of 32, in a coefficient memory block. At a maximum decimation of  $32$ ,  $32 \times 8 = 256$ coefficients is needed. The coefficient memory is available at SPI Address 0x1000 to Address 0x1FFF. This memory is sufficient space to store up to 2048 coefficients. Each vector profile has a pointer, P, to the coefficient block within coefficient memory.

Coefficients are written using the SPI in stream mode during startup. Coefficients are written in  $14$ -bit  $\times$  8-word = 112-bit blocks. There are 256 coefficient blocks. The 14 bits × 8-word coefficients are packed into 14 bytes × 8 bits, as shown i[n Table 29.](#page-42-2)

Writes and reads from a coefficient block must begin on a coefficient block boundary and an entire coefficient block must be written or read. After a coefficient block is written, the coefficient block address automatically increments/decrements (depending on the LSB/MSB SPI setting in Register 0x000) to the next coefficient block.

Having a direct map between SPI memory address and coefficient block address requires a divide by 7, which is not simple to accomplish in hardware (the address must be mapped within a single cycle). Therefore, each block is padded to a 16-byte boundary, but the SPI does not need to shift in these extra two bytes when loading coefficient memory sequentially. If the SPI is configured LSB first, SPIADDR[3:0] is all 0s. If the SPI is configured MSB first, SPIADDR[3:0] is all 1s. In other words, in LSB mode, the referenced addresses for the coefficient memory blocks are 0x1000, 0x2000, and so on, whereas in MSB SPI mode, the referenced block addresses are 0x100F, 0x200F, and so on.

Coefficient block order and how words/bytes are split across each other are shown i[n Table 29.](#page-42-2) When the SPI is configured LSB first,  $CO[0] = BO[0]$  is written first, and  $C7[13] = B13[7]$  is written last. When the SPI is configured MSB first,  $C7[13] =$ B13[7] is written first, and  $CO[0] = BO[0]$  is written last.

The position of a coefficient, Cn, in memory is determined from its index (i, j) by

$$
n = M(1 + i) - (1 + j)
$$
, if *i* is even (8)

$$
n = M \times i + j, \text{ if } i \text{ is odd} \tag{9}
$$

where

*M* is the decimation factor.

*j* is the decimation phase from 0 to  $M - 1$ .

*i* is the index within the coefficient block, from 0 to 7.

Due to symmetry, Coefficient C0 is multiplied by the newest and oldest samples.

As an example, the coefficient memory for a decimation factor of  $M = 4$  is shown in Table 28.

The upper 16 bits of the filter output are used as the data output of the channel. The filter output may have gain applied according to g, from the vector profile. Additionally, a gain of 4 can be applied using the filter output gain in Register 0x113, Bit 4.

<span id="page-42-3"></span>**Table 28. Coefficient Memory for M = 4** 

	Index (i)							
<b>Decimation Phase (j)</b>		ш						
	28	$\sim$ $\mathcal{L}_{\ell}$	20	19	1 Z			
	29	26	21	18	ن ا	10		
	30	25	22		14			
	31	24	23	16	ت ا			

#### <span id="page-42-2"></span>**Table 29. Coefficient Block Mapping into SPI Memory Location**



#### <span id="page-42-0"></span>**DIGITAL TEST WAVEFORMS**

Digital test waveforms can be used in the digital processing block instead of the ADC output. To enable digital test waveforms, use Address 0x11B. Enable each channel individually in Address 0x11A.

#### **Waveform Generator**

For testing and debugging, use a programmable waveform generator in place of ADC data. The waveform generator can vary offset, amplitude, and frequency. The generator uses the ADC sample frequency, f<sub>SAMPLE</sub>, and ADC full-scale amplitude, AFULL-SCALE, as references. The values are set in Address 0x117, Address 0x118, and Address 0x119 (se[e Table 33\)](#page-47-0).

$$
x = C + A \times \sin(2 \times \pi \times N) \tag{10}
$$

$$
N = \frac{f_{SAMPLE} \times n}{64}
$$
, see Address 0x117 (11)

$$
A = \frac{A_{FULL-SCALE}}{2^x}
$$
, see Address 0x118 (12)

$$
C = A_{\text{FULL-SCALE}} \times a \times 2^{-(13-b)}, \text{see Address 0x119} \tag{13}
$$

#### **Channel ID and Ramp Generator**

In Channel ID test mode, the output is a concatenated value. Bits[6:0] are a ramp. Bit 7 is 0 in real data mode or I channel and 1 for Q channel in complex data mode. Bits[10:8] are the channel ID such that Channel A is coded as 000 and Channel B is 001. Bits[15:11] are the chip address.

#### **Filter Coefficients**

To check the filter coefficients, use a sequence of 1 followed by 0s for the input to the decimating FIR filter. The number of 0s is the decimation rate times the number of taps (16). The output shifter outputs the LSBs of the filter.

### <span id="page-42-1"></span>**DIGITAL BLOCK POWER SAVING SCHEME**

To reduce power consumption in the digital block, the demodulator and decimation filter start in an idle state after running the chip (Register 0x008, Bits[2:0] = 000). In the digital idle state, the chip JESD204B block outputs zeroes and there is no unnecessary digital processing of the ADC output data. The digital block only switches to a running state when the negative edge of the TX\_TRIG± pulse is detected, or with a software TX\_TRIG $\pm$  write (Register 0x10C, Bit 5 = 1).

To put the digital block back into the idle state (while the rest of the chip is still running) and to save power, enact one of the following three events: raise the TX\_TRIG± signal high, write to the profile index (Register 0x10C, Bits[0:4]), or allow the power stop to expire by using the advanced power control feature. [Figure 59 i](#page-42-4)llustrates the digital block power saving scheme.



<span id="page-42-4"></span>Figure 59. Digital Block Power Saving Scheme

# <span id="page-43-0"></span>SERIAL PORT INTERFACE (SPI)

Th[e AD9671 S](http://www.analog.com/ad9671?doc=ad9671.pdf)PI allows the user to configure the signal chain for specific functions or operations through the structured register space provided inside the chip. The SPI offers the user added flexibility and customization, depending on the application. Addresses are accessed via the serial port and can be written to or read from via the port. Memory is organized into bytes that can be further divided into fields, as documented in th[e Memory](#page-45-0)  [Map s](#page-45-0)ection. For detailed operational information, see th[e AN-877](http://www.analog.com/an-877?doc=AD9671.pdf)  [Application Note,](http://www.analog.com/an-877?doc=AD9671.pdf) *Interfacing to High Speed ADCs via SPI*.

Three pins define the serial port interface: SCLK, SDIO, and CSB (se[e Table 30\)](#page-43-2). The SCLK (serial clock) pin synchronizes the read and write data presented to the device. The SDIO (serial data input/output) pin is a dual-purpose pin that allows data to be sent to and read from the internal memory map registers of the device. The CSB (chip select bar) pin is an active low control that enables or disables the read and write cycles.

#### <span id="page-43-2"></span>**Table 30. Serial Port Pins**



The falling edge of CSB, in conjunction with the rising edge of SCLK, determines the start of the framing sequence. During the instruction phase, a 16-bit instruction is transmitted, followed by one or more data bytes, which is determined by Bit Field W0 and Bit Field W1. An example of the serial timing and its definitions are shown i[n Figure 61 a](#page-44-0)nd [Table 31.](#page-44-1) 

During normal operation, CSB signals to the device that SPI commands are to be received and processed. When CSB is brought low, the device processes SCLK and SDIO to execute instructions. Normally, CSB remains low until the communication cycle is complete. However, if connected to a slow device, CSB can be brought high between bytes, allowing older microcontrollers enough time to transfer data into shift registers. CSB can be stalled when transferring one, two, or three bytes of data. When W0 and W1 are set to 11, the device enters streaming mode and continues to process data, either reading or writing, until CSB is taken high to end the communication cycle. CSB being high allows complete memory transfers without the need for additional instructions. Regardless of the mode, if CSB is taken high in the middle of a byte transfer, the SPI state machine is reset, and the device waits for a new instruction.

The SPI port can be configured to operate in different manners. CSB can also be tied low to enable 2-wire mode. When CSB is tied low, SCLK and SDIO are the only pins required for

communication. Although the device is synchronized during power-up, exercise caution when using 2-wire mode to ensure that the serial port remains synchronized with the CSB line. When operating in 2-wire mode, use a 1-, 2-, or 3-byte transfer exclusively. Without an active CSB line, streaming mode can be entered but not exited.

In addition to word length, the instruction phase determines whether the serial frame is a read or write operation, allowing the serial port to be used both to program the chip and to read the contents of the on-chip memory. If the instruction is a readback operation, performing a readback causes the serial data input/output (SDIO) pin to change direction from an input to an output at the appropriate point in the serial frame.

The user can send data in MSB first mode or LSB first mode. MSB first mode is the default at power-up and is changed by adjusting the configuration register (Address 0x000). For more information about this and other features, see th[e AN-877](http://www.analog.com/AN-877?doc=AD9671.pdf)  [Application Note,](http://www.analog.com/AN-877?doc=AD9671.pdf) *Interfacing to High Speed ADCs via SPI*.

#### <span id="page-43-1"></span>**HARDWARE INTERFACE**

The pins described in [Table 30 c](#page-43-2)onstitute the physical interface between the programming device and the serial port of the [AD9671.](http://www.analog.com/ad9671?doc=ad9671.pdf) The SCLK and CSB pins function as inputs when using the SPI. The SDIO pin is bidirectional, functioning as an input during write phases and as an output during readback.

If multiple SDIO pins share a common connection, ensure that proper V<sub>OH</sub> levels are met[. Figure 60](#page-43-3) shows the number of SDIO pins that can be connected together and the resulting V<sub>OH</sub> level, assuming the same load for each [AD9671.](http://www.analog.com/ad9671?doc=ad9671.pdf) 



<span id="page-43-3"></span>This interface is flexible enough to be controlled either by serial programmable read only memories (PROMs) or by PIC microcontrollers, which provide the user with an alternative to a full SPI controller for programming the device (see th[e AN-812](http://www.analog.com/an-812?doc=AD9671.pdf)  [Application Note,](http://www.analog.com/an-812?doc=AD9671.pdf) *Microcontroller-Based Serial Port Interface (SPI®) Boot Circuit*).



Figure 61. Serial Timing Details

### <span id="page-44-1"></span><span id="page-44-0"></span>**Table 31. Serial Timing Definitions**



## <span id="page-45-1"></span><span id="page-45-0"></span>MEMORY MAP **READING THE MEMORY MAP TABLE**

Each row in the memory map register table has eight bit locations. The memory map is roughly divided into three sections: the chip configuration register map (Address 0x000 to Address 0x19C), the profile register map (Address 0xF00 to Address 0xFFF), and the coefficient register map (Address 0x1000 to Address 0x1FFF). Registers that are designated as local registers use the device index in Address 0x004 and Address 0x005 to determine to which channels of a device the command is applied. Registers that are designated as chip registers use the chip address mode in Address 0x115 to determine whether the device is to be updated by writing to the chip register.

The first column of the memory map indicates the register address, and the default value is shown in the second rightmost column. The Bit 7 (MSB) column is the start of the default hexadecimal value given. For example, Address 0x011, the LNA and VGA gain adjustment register, has a default value of 0x06, meaning that Bit  $7 = 0$ , Bit  $6 = 0$ , Bit  $5 = 0$ , Bit  $4 = 0$ , Bit  $3 = 0$ , Bit  $2 = 1$ , Bit  $1 = 1$ 1, and Bit  $0 = 0$ , or 0000 0110 in binary. This setting is the default for GAIN $\pm$  pins enabled, PGA gain = 24 dB and LNA gain = 21.6 dB.

For more information about the SPI memory map and other functions, see th[e AN-877 Application Note,](http://www.analog.com/AN-877?doc=AD9671.pdf) *Interfacing to High Speed ADCs via SPI*.



### <span id="page-45-6"></span>**Table 32[. AD9671 S](http://www.analog.com/ad9671?doc=ad9671.pdf)PI Write Start-Up Sequence Example**

### <span id="page-45-2"></span>**RESERVED LOCATIONS**

Do not write to undefined memory locations except when writing the default values suggested in this data sheet. Addresses that have values marked as 0 must be considered reserved and have a 0 written into their registers during power-up.

#### <span id="page-45-3"></span>**DEFAULT VALUES**

After a reset, critical registers are automatically loaded with default values. These values are indicated in [Table 33,](#page-47-0) where an X refers to an undefined feature (don't care).

#### <span id="page-45-4"></span>**LOGIC LEVELS**

An explanation of various registers follows: "bit is set" is synonymous with "bit is set to Logic 1" or "writing Logic 1 for the bit." Similarly, "bit is cleared" is synonymous with "bit is set to Logic 0" or "writing Logic 0 for the bit."

### <span id="page-45-5"></span>**RECOMMENDED START-UP SEQUENCE**

To save system power during programming, th[e AD9671 p](http://www.analog.com/ad9671?doc=ad9671.pdf)owers up in power-down mode. To start the device up and initialize the data interface, the SPI commands listed i[n Table 32 a](#page-45-6)re recommended. At a minimum, write the profile memory for an index of 0 (Address 0xF00 to Address 0xF07; se[e Table 27\)](#page-39-2). If additional profiles and coefficient memory are required, write these after Profile File Memory 0.



<sup>1</sup> Setting the profile index requires an additional SPI write in SPI MSB mode before the chip is run to complete the current profile buffer update.<br><sup>2</sup> Bunning the chip from full nower-down mode requires 375 us wake-un ti

<sup>2</sup> Running the chip from full power-down mode requires 375 µs wake-up time as listed in Table 3.<br><sup>3</sup> The software TX\_TRIG trigger switches the demodulator/decimator digital block to a running state. It may not be needed the digital block.

4 Tuning the filters requires 512 ADC clock cycles.

<span id="page-47-0"></span>**Table 33[. AD9671 M](http://www.analog.com/ad9671?doc=ad9671.pdf)emory Map Registers** 

Addr. (Hex)	Register <b>Name</b>	Bit 7 (MSB)	Bit 6	Bit 5	Bit 4	Bit 3	Bit 2	Bit 1	Bit 0 (LSB)	<b>Default</b> Value	<b>Comments</b>
<b>Chip Configuration Registers</b>											
0x000	<b>CHIP</b> PORT_ <b>CONFIG</b>	$\mathbf 0$	LSB first $0 =$ off (default) $1 =$ on	SPI reset $0 =$ off (default) $1 =$ on	1	1	SPI reset $0 =$ off (default) $1 =$ on	LSB first $0 = \text{off}$ (default) $1 =$ on	$\mathbf 0$	0x18 0xA7	<b>Nibbles</b> mirrored so that LSB or MSB first mode is set correctly, regardless of shift mode. SPI reset reverts all registers (including the JESD ones), except Req. 0x000 to their default values and Reg. 0x000, Bit 2 and Bit 5 are auto- matically cleared. Default is
0x001	CHIP_ID	Chip ID Bits[7:0] $AD9671 = 0 \times A7$ (default)									unique chip ID, different for each device; read only register.
0x002	CHIP_ <b>GRADE</b>	X	X	Speed mode (identify device variants of chip ID) 00: Mode I (40 MSPS) (default) 01: Mode II (65 MSPS) 10: Mode III (80 MSPS) 11: Mode III (125 MSPS)		X	Χ	$\mathsf{x}$	$\mathsf{X}$	0x0X	Speed mode used to differentiate ADC speed power modes (must update Reg. 0x0FF to initiate mode setting).
	Device Index and Update Registers										
0x004	<b>DEVICE</b> INDEX_2	$\mathsf X$	$\pmb{\mathsf{X}}$	Χ	X	Data Channel H $0 =$ off $1 = \text{on}$ (default)	Data Channel G $0 =$ off $1 =$ on (default)	Data Channel F $0 =$ off $1 = on$ (default)	Data Channel E $0 =$ off $1 =$ on (default)	0x0F	<b>Bits are</b> set to de- termine which on-chip device receives the next write command.
0x005	DEVICE_ INDEX_1	Χ	$\pmb{\mathsf{X}}$	1	$\mathbf{1}$	Data Channel D $0 =$ off $1 = on$ (default)	Data Channel C $0 =$ off $1 = on$ (default)	Data Channel B $0 =$ off $1 = on$ (default)	Data Channel A $0 =$ off $1 = on$ (default)	0x3F	<b>Bits are</b> set to de- termine which on-chip device receives the next write command.

<span id="page-48-1"></span><span id="page-48-0"></span>

<span id="page-49-1"></span><span id="page-49-0"></span>



# AD9671 Data Sheet





# AD9671 Data Sheet





# AD9671 Data Sheet









### <span id="page-58-0"></span>**MEMORY MAP REGISTER DESCRIPTIONS**

For more information about the SPI memory map and other functions, consult th[e AN-877 Application Note,](http://www.analog.com/AN-877?doc=AD9671.pdf) *Interfacing to High Speed ADCs via SPI*.

#### **Update (Register 0x0FF)**

All registers except Register 0x002 are updated as soon as they are written. Writing to Register 0x0FF (the value written is don't care) initializes and updates the speed mode (Address 0x002) and resets all other registers to their default values (analog and ADC registers only; not the JESD204B registers, Register 0x000, or Register 0x002). Set the speed mode in Register 0x002 and write to Register 0x0FF at the beginning of the setup of the SPI writes after the device is powered up to avoid rewriting other registers after Register 0x0FF is written.

#### **Profile Index and Software TX\_TRIG (Register 0x10C)**

The vector profile is selected using the profile index in Register 0x10C, Bits[4:0]. The software TX\_TRIG control in Bit 5 generates a TX\_TRIG signal internal to the device. This signal is asynchronous to the ADC sample clock. Therefore, do not use this signal to align the data output, reset the digital demodulator and decimator, or initiate advanced power mode across multiple devices in the system. The external pin-driven TX\_TRIG± control is recommended for systems that require synchronization of these features across multiple [AD9671](http://www.analog.com/ad9671?doc=ad9671.pdf) devices.