20 GHz to 54 GHz, GaAs, pHEMT, MMIC, 31 dBm (1 W) Power Amplifier

Data Sheet **ADPA7008CHIP**

FEATURES

Output P1dB: 30.5 dBm typical at 22 GHz to 42 GHz
P_{SAT}: 31 dBm typical at 22 GHz to 42 GHz
Gain: 18 dB typical at 22 GHz to 42 GHz
Input return loss: 22 dB typical at 22 GHz to 42 GHz
Output return loss: 23 dB typical at 22 GHz to 42 GHz
Output IP3: 38 dBm typical at 22 GHz to 42 GHz
Supply voltage: 5 V typical at 1500 mA
50 Ω matched input and output
Die size: 3.610 mm × 3.610 mm × 0.102 mm

APPLICATIONS

Military and space
Test instrumentation
Satellite communications

FUNCTIONAL BLOCK DIAGRAM

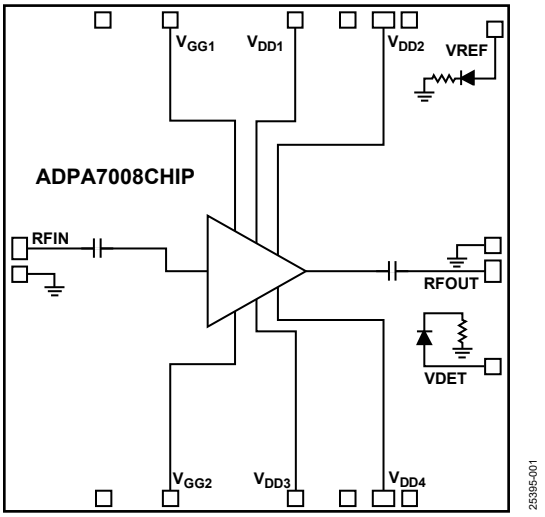

Figure 1.

GENERAL DESCRIPTION

The ADPA7008CHIP is a gallium arsenide (GaAs), pseudomorphic high electron mobility transistor (pHEMT), monolithic microwave integrated circuit (MMIC), 31 dBm saturated output power (1 W) distributed power amplifier that operates from 20 GHz to 54 GHz. The amplifier provides a gain of 18 dB, an output power for 1 dB compression (P1dB) of 30.5 dBm, and a typical output third-order intercept (IP3) of 38 dBm at 22 GHz to 42 GHz. The ADPA7008CHIP requires 1500 mA from a 5 V supply voltage (V_{DD}) and features inputs and outputs that are internally matched to 50 Ω, facilitating integration into multichip modules (MCMs). All data is taken with the RFIN and RFOUT pads connected via one 0.076 mm (3 mil) ribbon bond of 0.076 mm (3 mil) minimal length.

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Rev. 0 **Document Feedback**

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REVISION HISTORY

3/2021—Revision 0: Initial Version

SPECIFICATIONS

20 GHz TO 22 GHz FREQUENCY RANGE

T_A = 25°C, supply voltage (V_{DD}) = 5 V, quiescent supply current (I_{DQ}) = 1500 mA, and 50 Ω matched input and output, unless otherwise noted. Adjust V_{GG1} from −1.5 V to 0 V to achieve I_{DQ} = 1500 mA typical.

Table 1.

Parameter	Symbol	Min	Typ	Max	Unit	Test Conditions/Comments
FREQUENCY RANGE		20		22	GHz	
GAIN		14.5	17		dB	
Gain Flatness			±0.8		dB	
Gain Variation Over Temperature			0.036		dB/°C	
NOISE FIGURE			7.5		dB	
RETURN LOSS						
Input			21		dB	
Output			22		dB	
OUTPUT						
Output Power for 1 dB Compression	P1dB	26.5	29		dBm	
Saturated Output Power	P_{SAT}		30.5		dBm	
Output Third-Order Intercept	IP3		37		dBm	Output power (P_{OUT}) per tone = 14 dBm with 1 MHz tone spacing
SUPPLY						
Quiescent Current	I_{DQ}		1500		mA	Adjust V_{GG1} to achieve I_{DQ} = 1500 mA typical
Voltage	V_{DD}	4	5		V	

22 GHz TO 42 GHz FREQUENCY RANGE

T_A = 25°C, V_{DD} = 5 V, I_{DQ} = 1500 mA, and 50 Ω matched input and output, unless otherwise noted. Adjust V_{GG1} from −1.5 V to 0 V to achieve I_{DQ} = 1500 mA typical.

Table 2.

Parameter	Symbol	Min	Typ	Max	Unit	Test Conditions/Comments
FREQUENCY RANGE		22		42	GHz	
GAIN		15.5	18		dB	
Gain Flatness			±0.8		dB	
Gain Variation Over Temperature			0.022		dB/°C	
NOISE FIGURE			6.0		dB	
RETURN LOSS						
Input			22		dB	
Output			23		dB	
OUTPUT						
Output Power for 1 dB Compression	P1dB	28	30.5		dBm	
Saturated Output Power	P_{SAT}		31		dBm	
Output Third-Order Intercept	IP3		38		dBm	P_{OUT} per tone = 14 dBm with 1 MHz tone spacing
SUPPLY						
Quiescent Current	I_{DQ}		1500		mA	Adjust V_{GG1} to achieve I_{DQ} = 1500 mA typical
Voltage	V_{DD}	4	5		V	

42 GHz TO 50 GHz FREQUENCY RANGE

T_A = 25°C, V_{DD} = 5 V, I_{DQ} = 1500 mA, and 50 Ω matched input and output, unless otherwise noted. Adjust V_{GG1} from −1.5 V to 0 V to achieve I_{DQ} = 1500 mA typical.

Table 3.

Parameter	Symbol	Min	Typ	Max	Unit	Test Conditions/Comments
FREQUENCY RANGE		42		50	GHz	
GAIN		14.5	17		dB	
Gain Flatness			±0.55		dB	
Gain Variation Over Temperature			0.019		dB/°C	
NOISE FIGURE			6.5		dB	
RETURN LOSS						
Input			20		dB	
Output			24		dB	
OUTPUT						
Output Power for 1 dB Compression	P1dB	25	27.5		dBm	
Saturated Output Power	P_{SAT}		28		dBm	
Output Third-Order Intercept	IP3		37		dBm	P_{OUT} per tone = 14 dBm with 1 MHz tone spacing
SUPPLY						
Quiescent Current	I_{DQ}		1500		mA	Adjust V_{GG1} to achieve I_{DQ} = 1500 mA typical
Voltage	V_{DD}	4	5		V	

50 GHz TO 54 GHz FREQUENCY RANGE

T_A = 25°C, V_{DD} = 5 V, I_{DQ} = 1500 mA, and 50 Ω matched input and output, unless otherwise noted. Adjust V_{GG1} from −1.5 V to 0 V to achieve I_{DQ} = 1500 mA typical.

Table 4.

Parameter	Symbol	Min	Typ	Max	Unit	Test Conditions/Comments
FREQUENCY RANGE		50		54	GHz	
GAIN			18.5		dB	
Gain Flatness			±0.8		dB	
Gain Variation Over Temperature			0.012		dB/°C	
NOISE FIGURE			7.0		dB	
RETURN LOSS						
Input			16		dB	
Output			17		dB	
OUTPUT						
Output Power for 1 dB Compression	P1dB		26		dBm	
Saturated Output Power	P_{SAT}		28		dBm	
Output Third-Order Intercept	IP3		37		dBm	P_{OUT} per tone = 14 dBm with 1 MHz tone spacing
SUPPLY						
Quiescent Current	I_{DQ}		1500		mA	Adjust V_{GG1} to achieve I_{DQ} = 1500 mA typical
Voltage	V_{DD}	4	5		V	

ABSOLUTE MAXIMUM RATINGS

Table 5.

Parameter	Rating
Drain Bias Voltage (V_{DDx})	6.0 V
V_{GGx}	−1.6 V to 0 V
RF Input Power (RFIN)	20 dBm
Continuous Power Dissipation (P_{DISS}), T_A = 85°C (Derate 170 mW/°C Above 85°C)	15.3 W
Junction Temperature to Maintain 1,000,000 Hour Mean Time to Failure (MTTF)	175°C
Nominal Junction Temperature (T_J = 85°C, V_{DD} = 5 V, I_{DQ} = 1500 mA)	129°C
Temperature Range	
Storage	−65°C to +150°C
Operating	−55°C to +85°C

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

THERMAL RESISTANCE

Thermal performance is directly linked to the carrier or substrate on which the die is mounted. Careful attention is needed with each material used in the thermal path below the IC.

θ_{JC} is the channel to case thermal resistance, channel to bottom of die using die attach epoxy.

Table 6. Thermal Resistance

Package Type	θ_{JC}	Unit
C-10-12	5.87	°C/W

ELECTROSTATIC DISCHARGE (ESD) RATINGS

The following ESD information is provided for handling of ESD sensitive devices in an ESD protected area only.

Human body model (HBM) per ANSI/ESDA/JEDEC JS-001.

ESD Ratings for ADPA7008CHIP

Table 7. ADPA7008CHIP, 10-Pad Die

ESD Model	Withstand Threshold (V)	Class
HBM	±250	1A

ESD CAUTION

ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

PIN CONFIGURATION AND FUNCTION DESCRIPTIONS

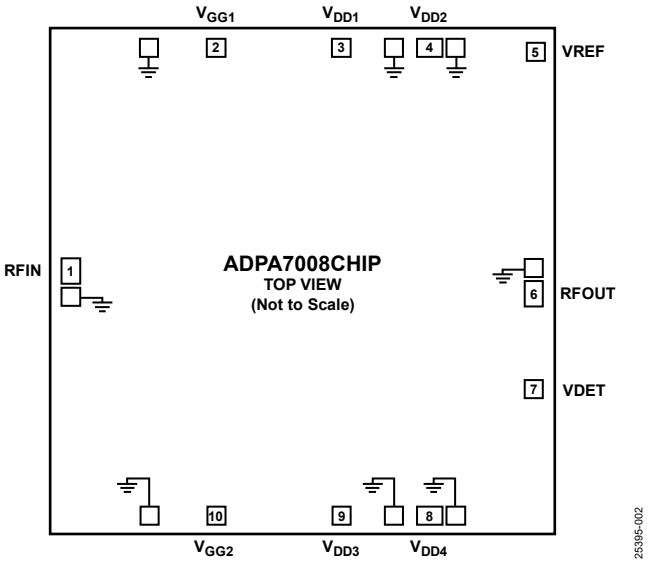

Figure 2. Pin Configuration

Table 8. Pin Function Descriptions

Pin No.	Mnemonic	Description
1	RFIN	RF Signal Input. This pad is ac-coupled and matched to 50 Ω. See Figure 6 for the interface schematic.
2, 10	V_{GG1}, V_{GG2}	Amplifier Gate Controls. External bypass capacitors of 4.7 µF, 0.01 µF, and 100 pF are required for these pads. Adjust V_{GG1} from −1.5 V to 0 V to achieve the desired quiescent current. See Figure 7 for the interface schematic.
3, 4, 8, 9	V_{DD1}, V_{DD2}, V_{DD4}, V_{DD3}	Drain Biases for the Amplifier. External bypass capacitors of 4.7 µF, 0.01 µF, and 100 pF are required for these pads. See Figure 9 for the interface schematic.
5	VREF	Reference Diode Voltage. Use this pad for temperature compensation of the VDET RF output power measurements. Used in combination with VDET, this voltage provides temperature compensation to the VDET RF output power measurements. See Figure 4 for the interface schematic.
6	RFOUT	RF Signal Output. This pad is ac-coupled and matched to 50 Ω. See Figure 8 for the interface schematic.
7	VDET	Detector Diode Used for Measuring the RF Output Power. Detection via this pad requires the application of a dc bias voltage through an external series resistor. Used in combination with VREF, the difference detector voltage, VREF − VDET, is a temperature compensated dc voltage proportional to the RF output power. See Figure 5 for the interface schematic.
Die Bottom	GND	Ground. The die bottom must be connected to RF and dc ground. See Figure 3 for the interface schematic.

INTERFACE SCHEMATICS

Figure 3. GND Interface Schematic

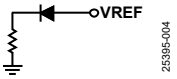

Figure 4. VREF Interface Schematic

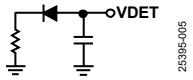

Figure 5. VDET Interface Schematic

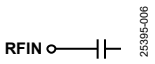

Figure 6. RFIN Interface Schematic

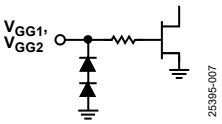

Figure 7. V_{GG1}, V_{GG2} Interface Schematic

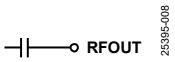

Figure 8. RFOUT Interface Schematic

Figure 9. V_{DD1} to V_{DD4} Interface Schematic

TYPICAL PERFORMANCE CHARACTERISTICS

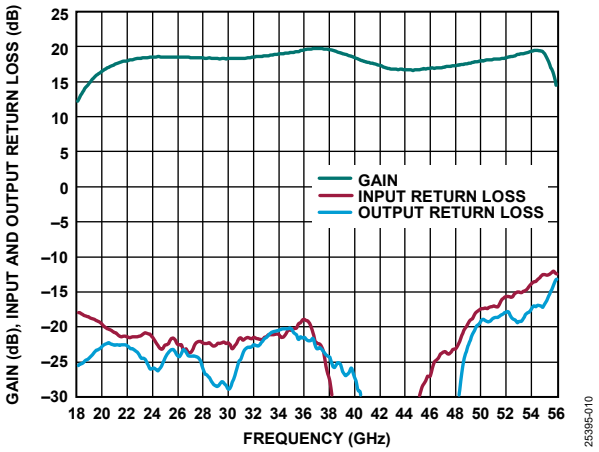

Figure 10. Gain, Input and Output Return Loss vs. Frequency, V_{DD} = 5 V, I_{DQ} = 1500 mA

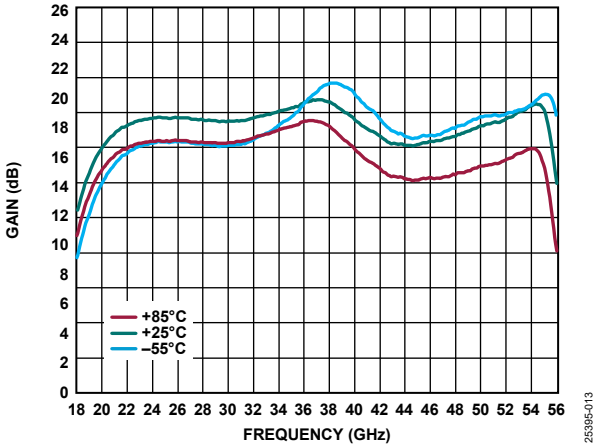

Figure 13. Gain vs. Frequency for Various Temperatures, V_{DD} = 5 V, I_{DQ} = 1500 mA

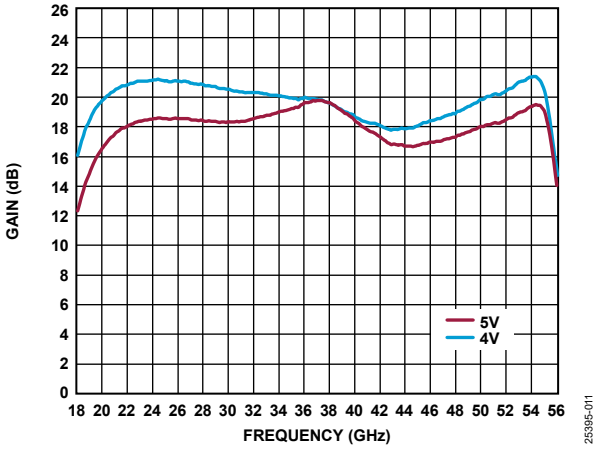

Figure 11. Gain vs. Frequency for Various Supply Voltages, I_{DQ} = 1500 mA

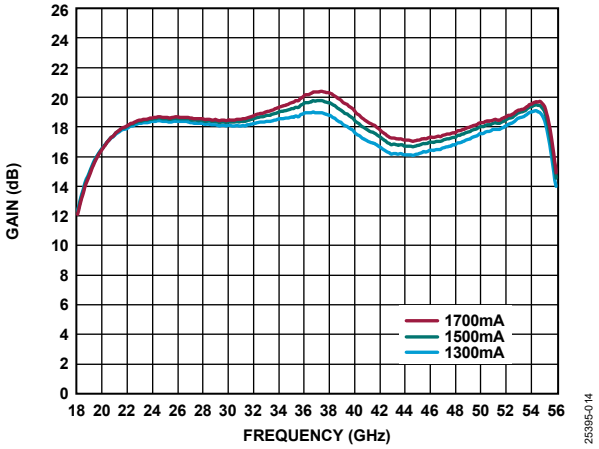

Figure 14. Gain vs. Frequency for Various Supply Currents, V_{DD} = 5 V

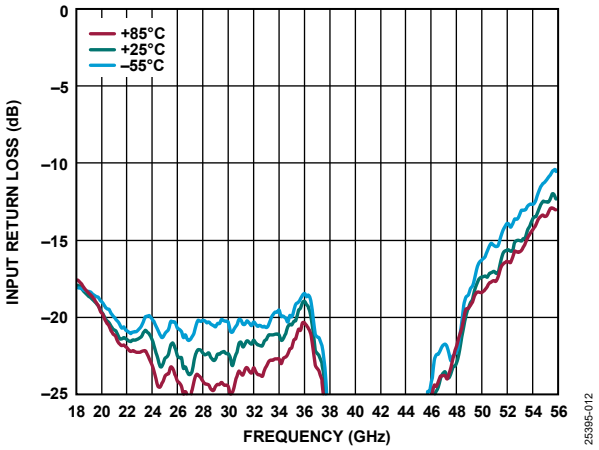

Figure 12. Input Return Loss vs. Frequency for Various Temperatures, V_{DD} = 5 V, I_{DQ} = 1500 mA

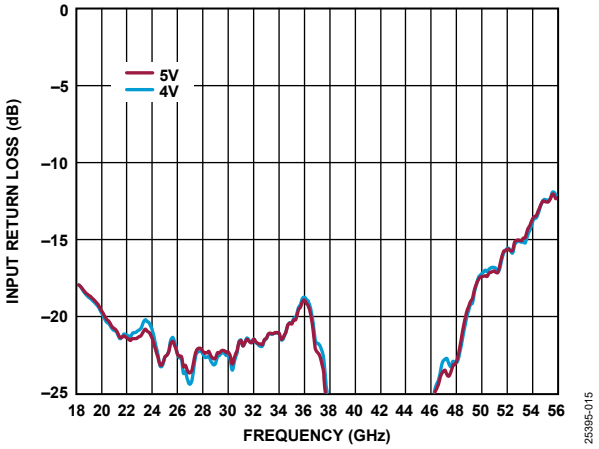

Figure 15. Input Return Loss vs. Frequency for Various Supply Voltages, I_{DQ} = 1500 mA

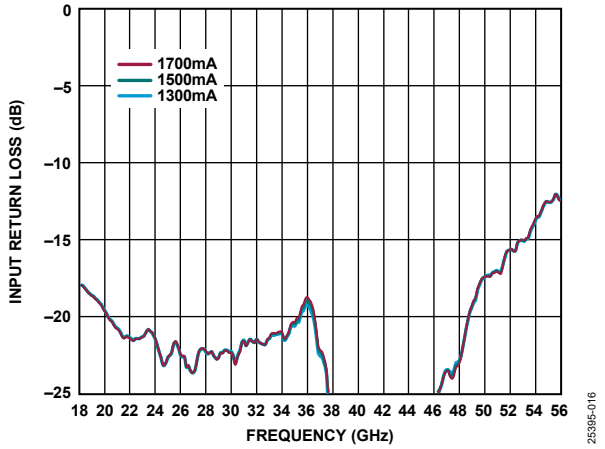

Figure 16. Input Return Loss vs. Frequency for Various Supply Currents, V_{DD} = 5 V

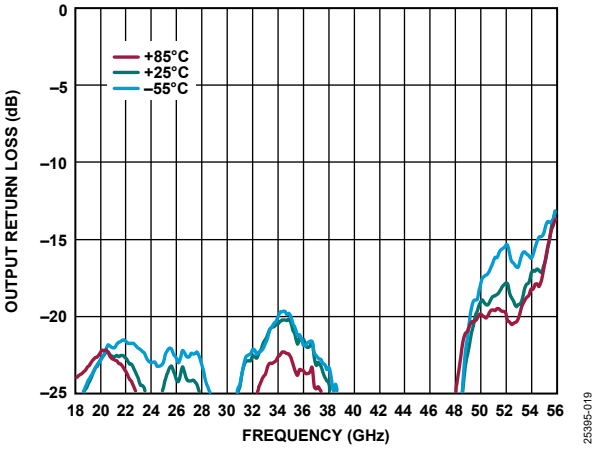

Figure 19. Output Return Loss vs. Frequency for Various Temperatures, V_{DD} = 5 V, I_{DQ} = 1500 mA

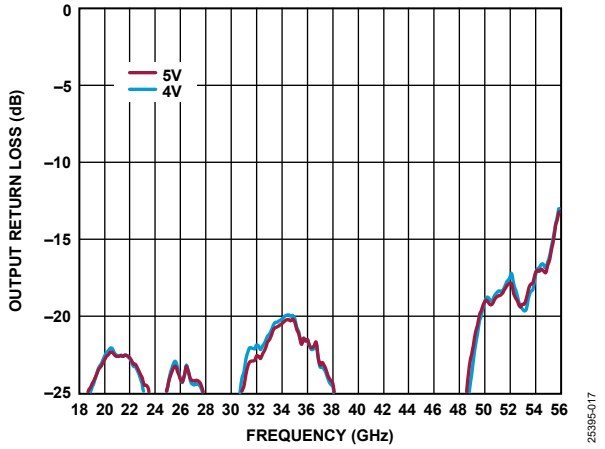

Figure 17. Output Return Loss vs. Frequency for Various Supply Voltages, I_{DQ} = 1500 mA

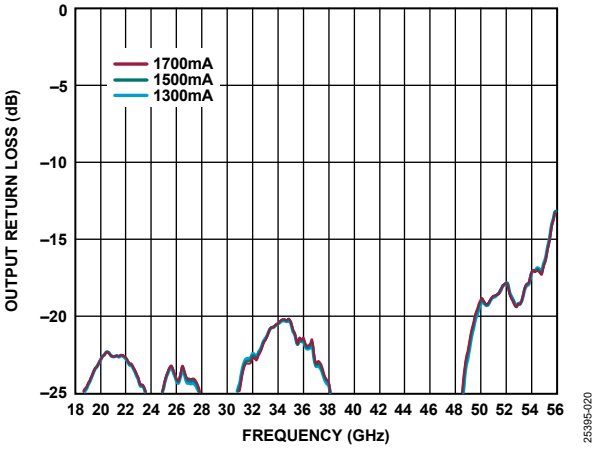

Figure 20. Output Return Loss vs. Frequency for Various Supply Currents, V_{DD} = 5 V

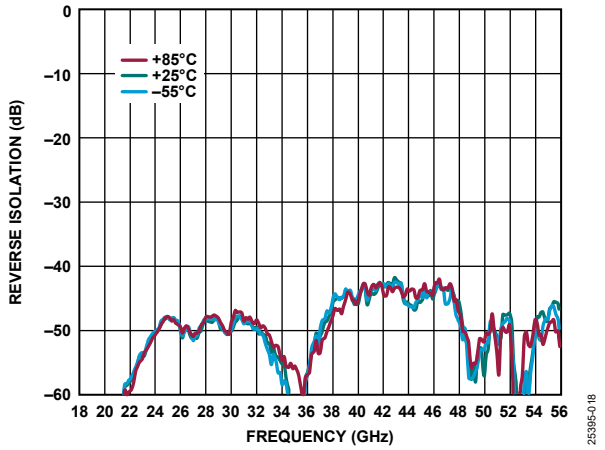

Figure 18. Reverse Isolation vs. Frequency for Various Temperatures, V_{DD} = 5 V, I_{DQ} = 1500 mA

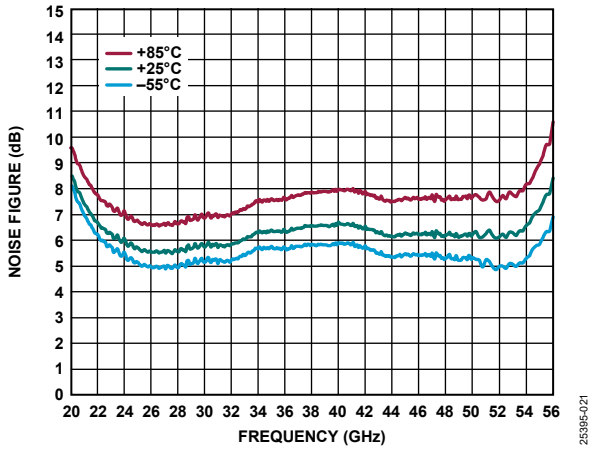

Figure 21. Noise Figure vs. Frequency for Various Temperatures, V_{DD} = 5 V, I_{DQ} = 1500 mA

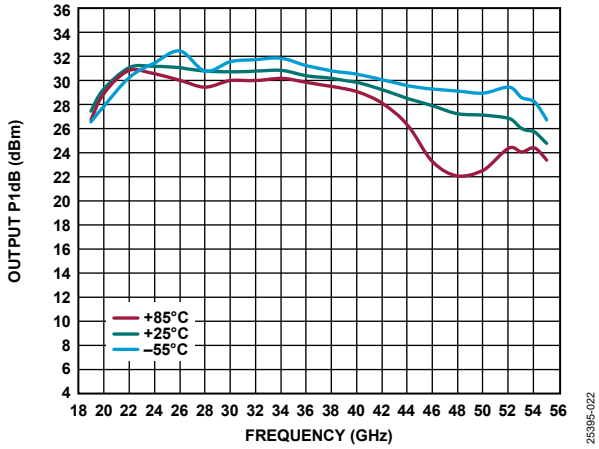

Figure 22. Output P1dB vs. Frequency for Various Temperatures, V_{DD} = 5 V, I_{DQ} = 1500 mA

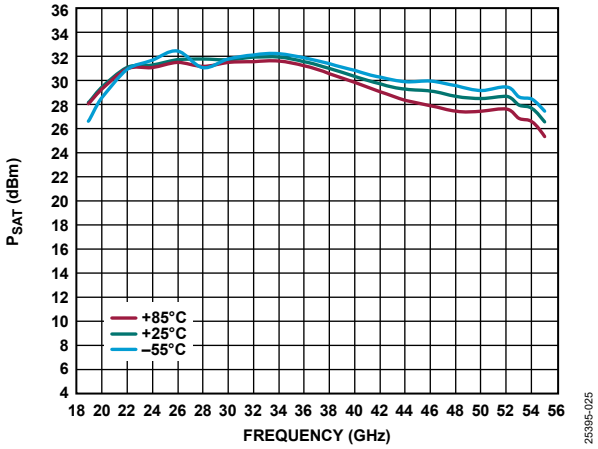

Figure 25. P_{SAT} vs. Frequency for Various Temperatures, V_{DD} = 5 V, I_{DQ} = 1500 mA

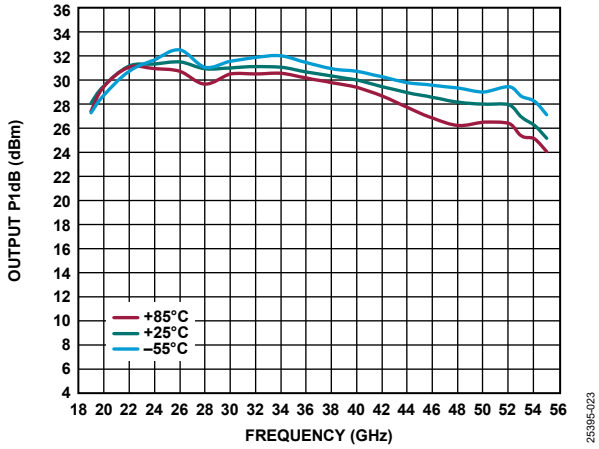

Figure 23. Output P1dB vs. Frequency for Various Temperatures, V_{DD} = 5 V, I_{DQ} = 1700 mA

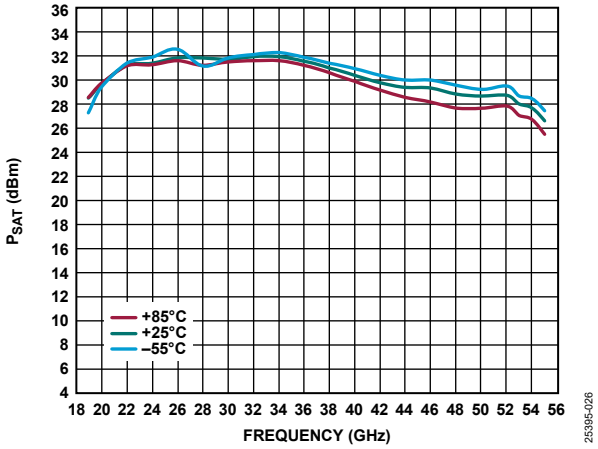

Figure 26. P_{SAT} vs. Frequency for Various Temperatures, V_{DD} = 5 V, I_{DQ} = 1700 mA

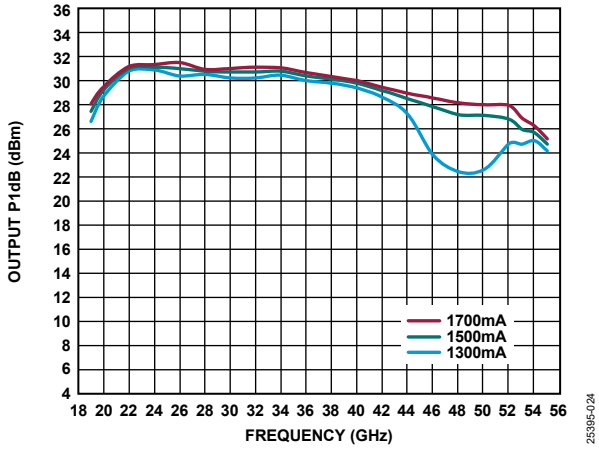

Figure 24. Output P1dB vs. Frequency for Various Supply Currents, V_{DD} = 5 V

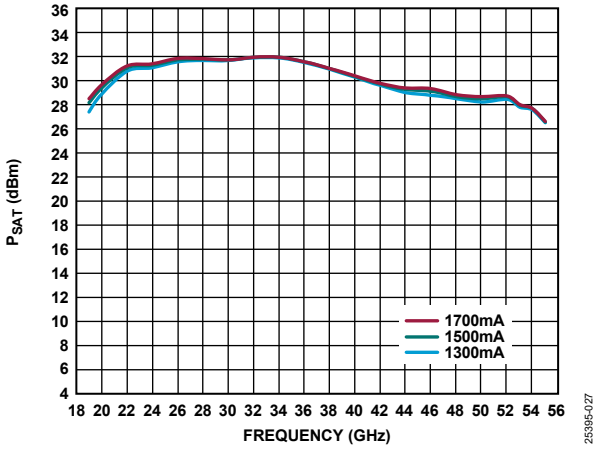

Figure 27. P_{SAT} vs. Frequency for Various Supply Currents, V_{DD} = 5 V

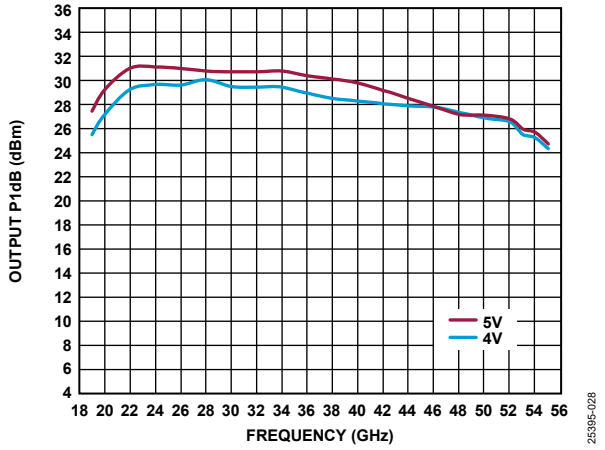

Figure 28. Output P1dB vs. Frequency for Various Supply Voltages, I_{DQ} = 1500 mA

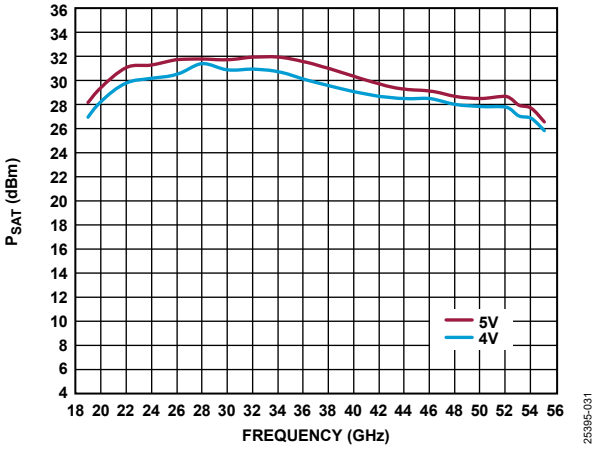

Figure 31. P_{SAT} vs. Frequency for Various Voltages, I_{DQ} = 1500 mA

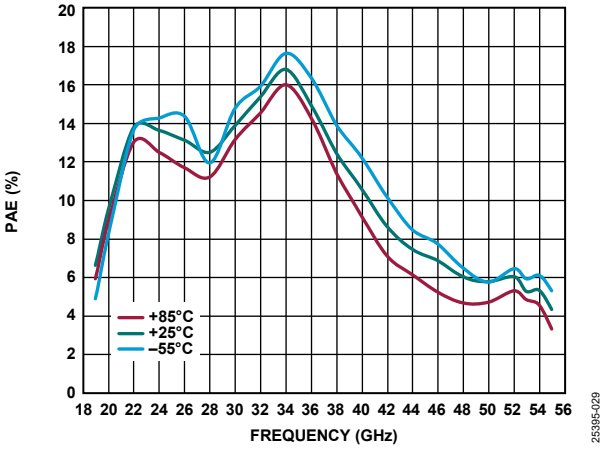

Figure 29. Power Added Efficiency (PAE) vs. Frequency for Various Temperatures, V_{DD} = 5 V, I_{DQ} = 1500 mA, PAE at P_{SAT} (dBm)

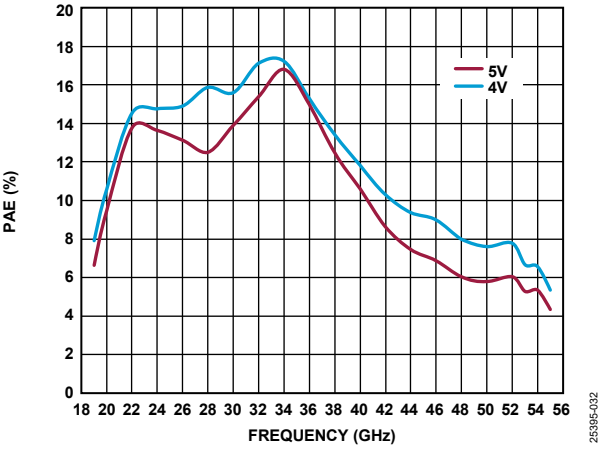

Figure 32. PAE vs. Frequency for Various Supply Voltages, I_{DQ} = 1500 mA, PAE at P_{SAT} (dBm)

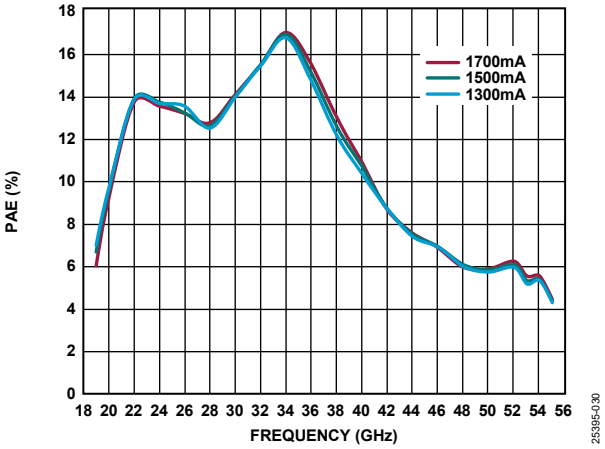

Figure 30. PAE vs. Frequency for Various Supply Currents, V_{DD} = 5 V, PAE at P_{SAT} (dBm)

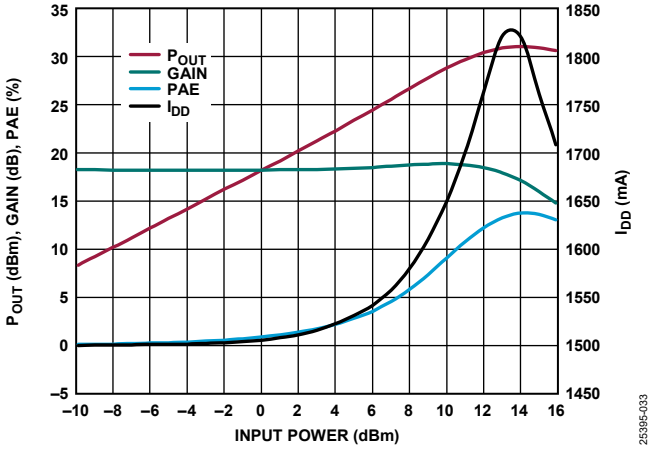

Figure 33. P_{OUT}, Gain, PAE, and Drain Current with RF Applied (I_{DD}) vs. Input Power, 22 GHz, V_{DD} = 5 V, I_{DQ} = 1500 mA

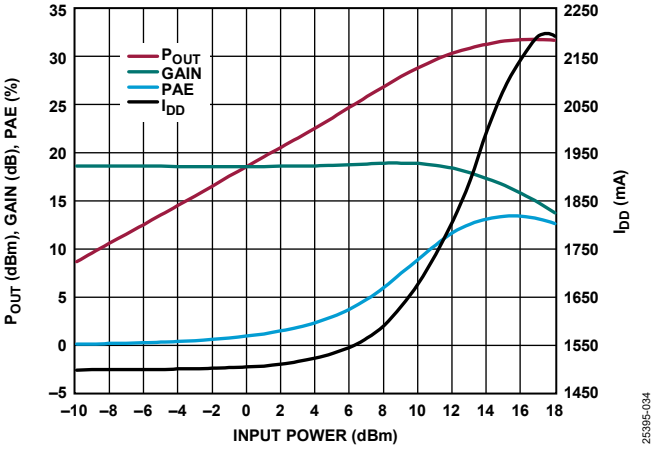

Figure 34. P_{OUT}, Gain, PAE, and I_{DD} vs. Input Power, 26 GHz, V_{DD} = 5 V, I_{DQ} = 1500 mA

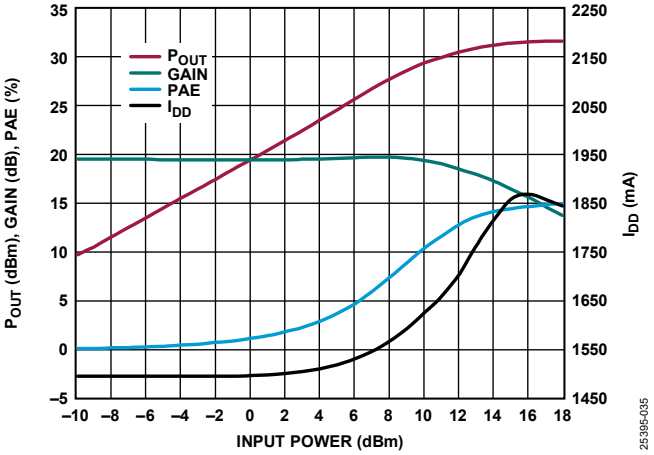

Figure 35. P_{OUT}, Gain, PAE, and I_{DD} vs. Input Power, 36 GHz, V_{DD} = 5 V, I_{DQ} = 1500 mA

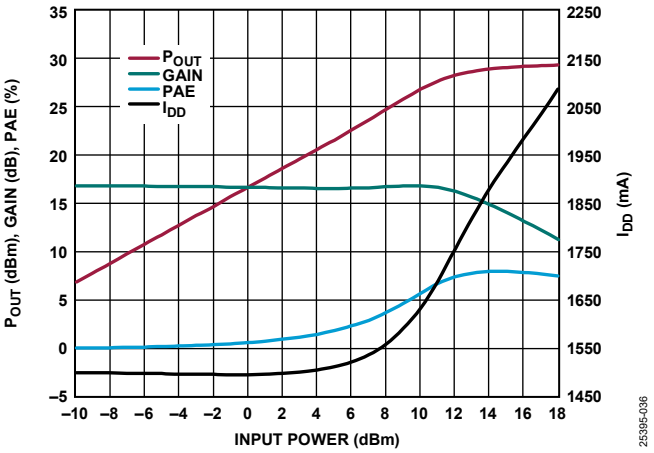

Figure 36. P_{OUT}, Gain, PAE, and I_{DD} vs. Input Power, 44 GHz, V_{DD} = 5 V, I_{DQ} = 1500 mA

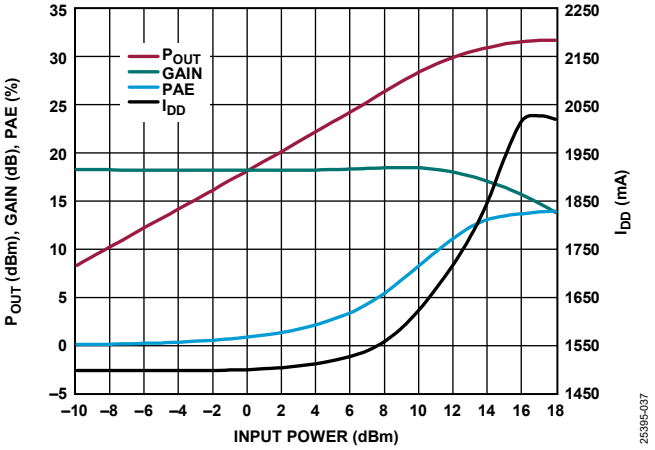

Figure 37. P_{OUT}, Gain, PAE, and I_{DD} vs. Input Power, 30 GHz, V_{DD} = 5 V, I_{DQ} = 1500 mA

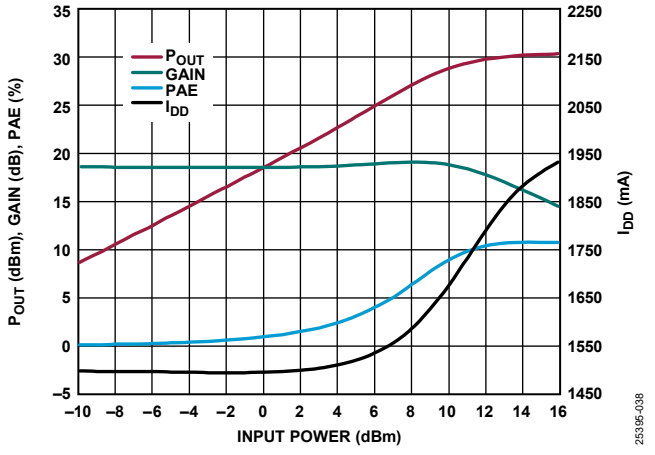

Figure 38. P_{OUT}, Gain, PAE, and I_{DD} vs. Input Power, 40 GHz, V_{DD} = 5 V, I_{DQ} = 1500 mA

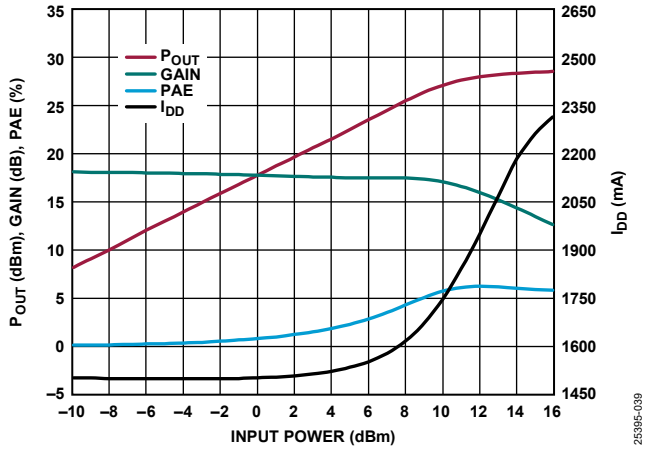

Figure 39. P_{OUT}, Gain, PAE, and I_{DD} vs. Input Power, 50 GHz, V_{DD} = 5 V, I_{DQ} = 1500 mA

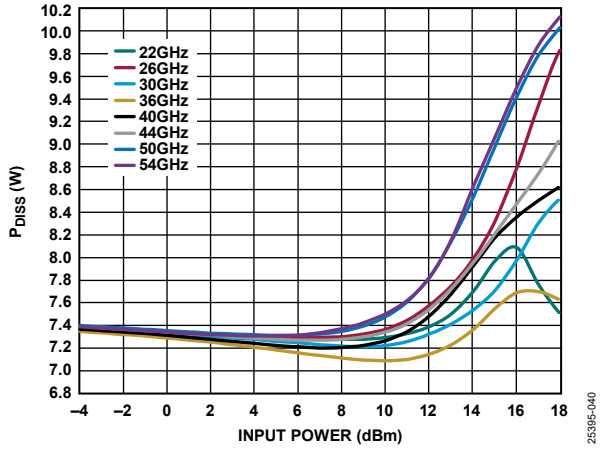

Figure 40. P_{DISS} vs. Input Power for Various Frequencies at T_A = 85°C, V_{DD} = 5 V, I_{DQ} = 1500 mA

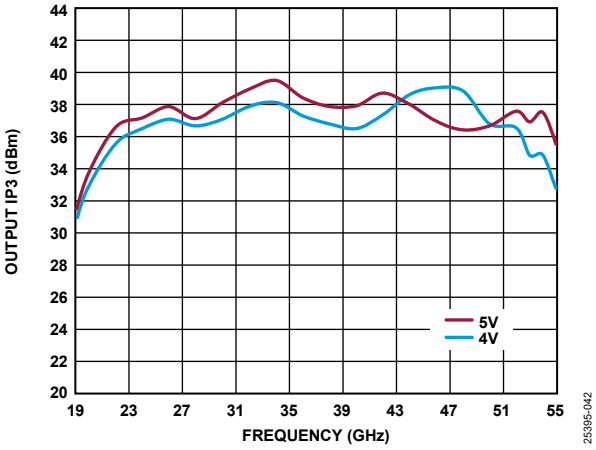

Figure 43. Output IP3 vs. Frequency for Various Supply Voltages, P_{OUT} per Tone = 14 dBm, I_{DQ} = 1500 mA

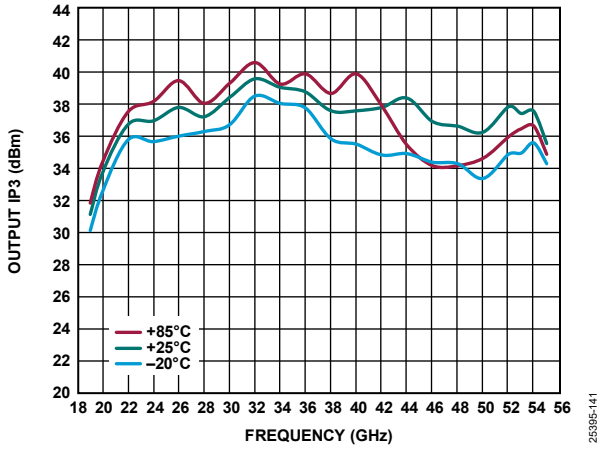

Figure 41. Output IP3 vs. Frequency at –20°C, +25°C, and +85°C, P_{OUT} per Tone = 14 dBm, V_{DD} = 5 V, I_{DQ} = 1500 mA

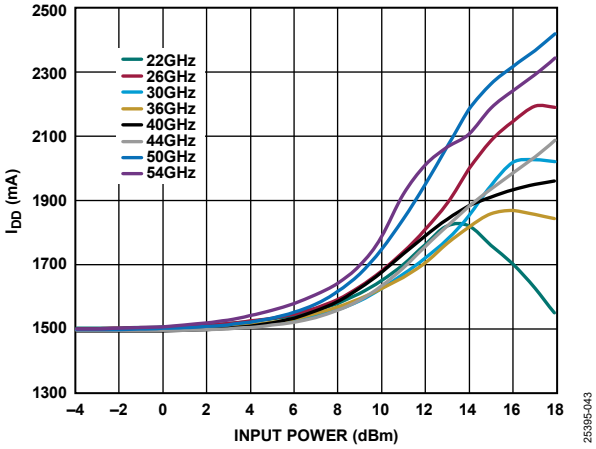

Figure 44. I_{DD} vs. Input Power at Various Frequencies, V_{DD} = 5 V, I_{DQ} = 1500 mA

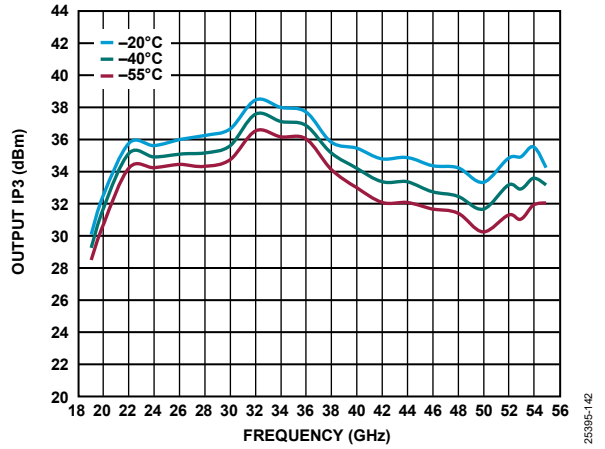

Figure 42. Output IP3 vs. Frequency at –20°C, –40°C, and –55°C, P_{OUT} per Tone = 14 dBm, V_{DD} = 5 V, I_{DQ} = 1500 mA

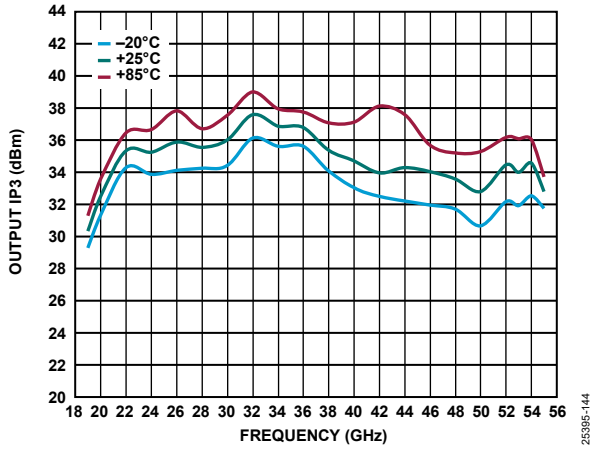

Figure 45. Output IP3 vs. Frequency at –20°C, +25°C, and +85°C, P_{OUT} per Tone = 14 dBm, V_{DD} = 5 V, I_{DQ} = 1700 mA

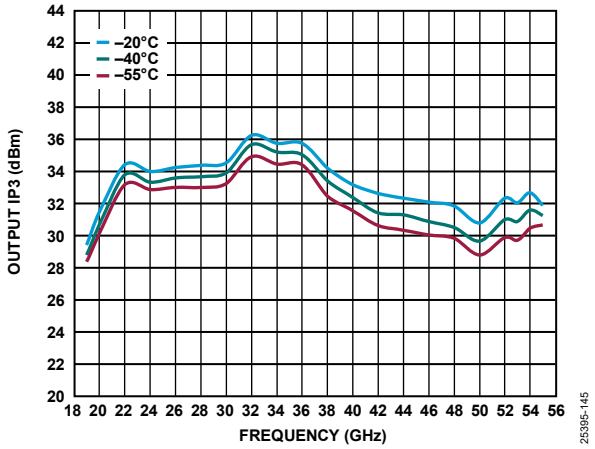

Figure 46. Output IP3 vs. Frequency at −20°C, −40°C, and −55°C, P_{OUT} per Tone = 14 dBm, V_{DD} = 5 V, I_{DQ} = 1700 mA

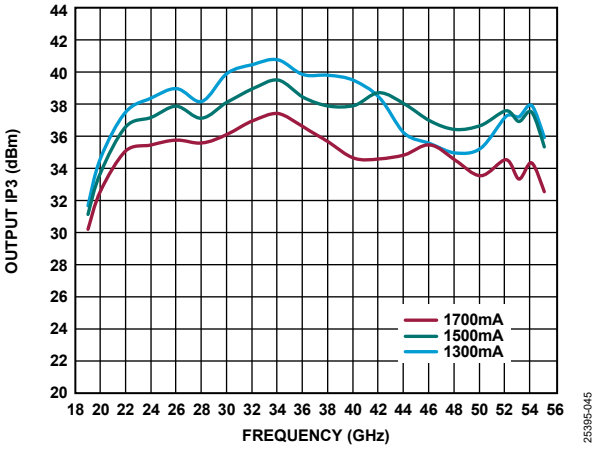

Figure 47. Output IP3 vs. Frequency for Various Supply Currents, P_{OUT} per Tone = 14 dBm, V_{DD} = 5 V

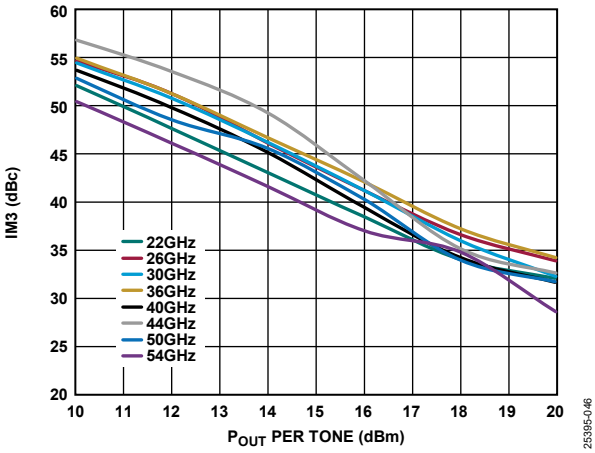

Figure 48. Third-Order Intermodulation Distortion (IM3) vs. P_{OUT} per Tone, V_{DD} = 4 V, I_{DQ} = 1500 mA

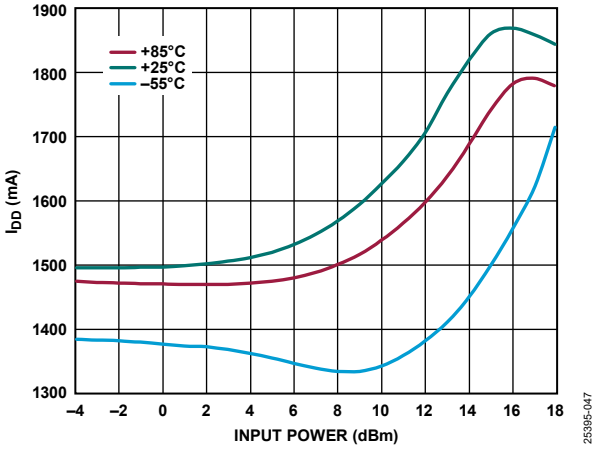

Figure 49. I_{DD} vs. Input Power for Various Temperatures at 36 GHz, V_{DD} = 5 V, I_{DQ} = 1500 mA

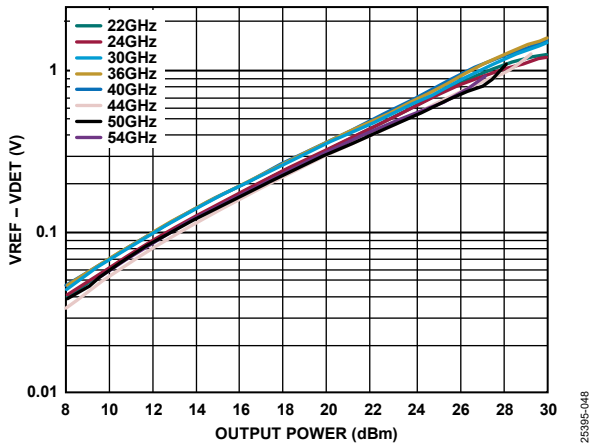

Figure 50. Detector Voltage (VREF − VDET) vs. Output Power for Various Frequencies

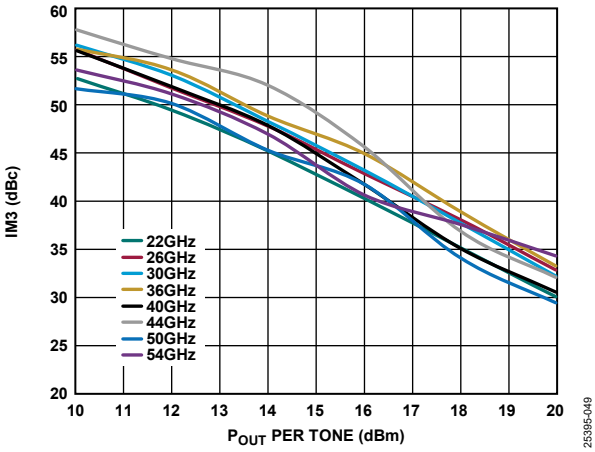

Figure 51. IM3 vs. P_{OUT} per Tone, V_{DD} = 5 V, I_{DQ} = 1500 mA

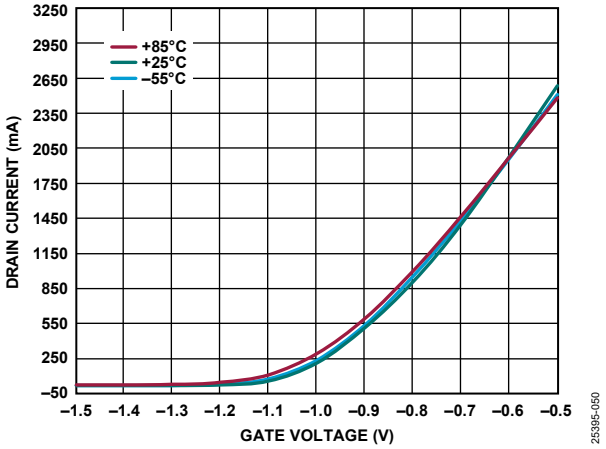

Figure 52. Drain Current vs. Gate Voltage for Various Temperatures, V_{DD} = 5 V, I_{DQ} = 1500 mA

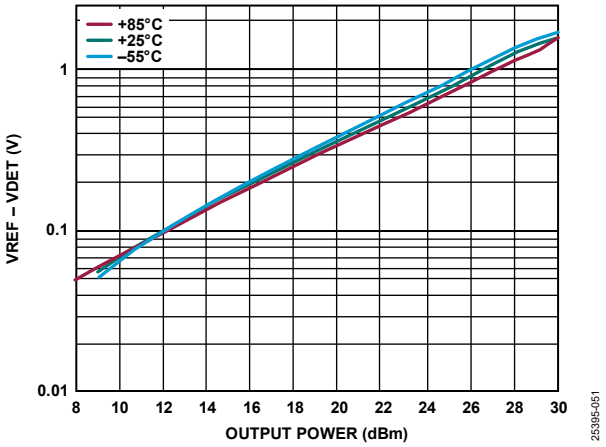

Figure 53. Detector Voltage (VREF – VDET) vs. Output Power for Various, Temperatures at 36 GHz

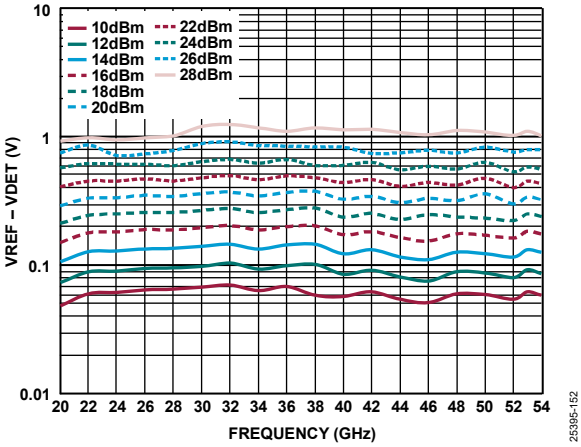

Figure 54. Detector Voltage (VREF – VDET) vs. Frequency for Various Output Powers

THEORY OF OPERATION

The architecture of the ADPA7008CHIP, a medium power amplifier, is shown in Figure 55. The ADPA7008CHIP uses two cascaded, four-stage amplifiers operating in quadrature between six 90° hybrids.

The input signal is divided evenly into two, and then each signal is divided into two again. Each of these new paths are amplified through four independent gain stages. The amplified signals are then combined at the output. This balanced amplifier approach forms an amplifier with a combined gain of 18 dB and a P_{SAT} value of 31 dBm.

A portion of the RF output signal is directionally coupled to a diode for detection of the RF output power. When the diode is dc biased, the diode rectifies the RF power and makes the RF power available for measurement as a dc voltage at VDET. To allow temperature compensation of VDET, an identical and symmetrically located circuit, minus the coupled RF power, is available via VREF. Taking the difference of VREF – VDET provides a temperature compensated signal that is proportional to the RF output (see Figure 55).

The 90° hybrids ensure that the input and output return losses are greater than 14 dB. See the application circuits shown in Figure 56 and Figure 57 for further details on biasing the various blocks.

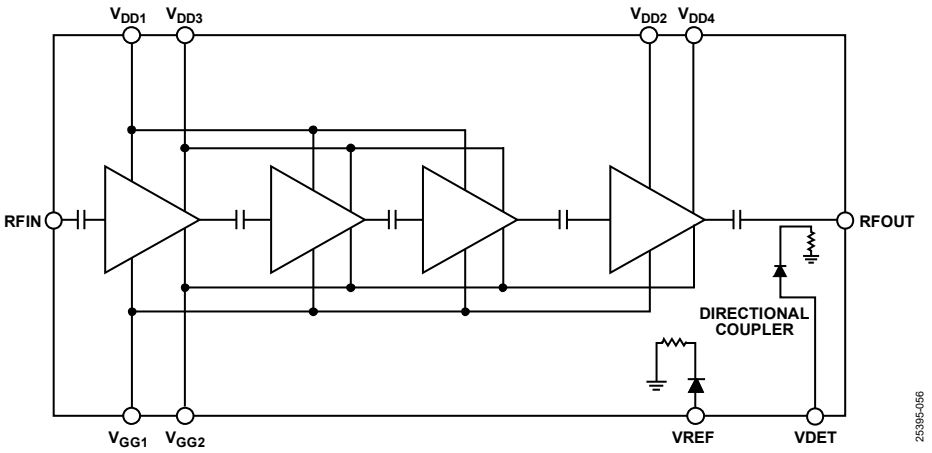

Figure 55. ADPA7008CHIP Architecture

APPLICATIONS INFORMATION

The ADPA7008CHIP is a GaAs, pHEMT, MMIC power amplifier. Capacitive bypassing is required for all V_{GGx} and V_{DDx} pads. V_{GG1} is the gate bias pad for the top cascaded amplifiers. V_{GG2} is the gate bias pad for the bottom cascaded amplifiers. V_{DD1} and V_{DD3} are the drain bias pads for the top cascaded amplifiers. V_{DD2} and V_{DD4} are the drain bias pads for the bottom cascaded amplifiers.

All measurements for this device were taken using the primary application circuit (see Figure 56) and were configured as shown in the assembly diagram (see Figure 65).

The recommended bias sequence during power-up is as follows:

1. Connect GND to RF and dc ground.
2. Set the gate bias voltages, V_{GG1} and V_{GG2}, to −1.5 V.
3. Set all the drain bias voltages, V_{DDx}, to 5 V.
4. Increase the gate bias voltages, V_{GG1} and V_{GG2}, to achieve an I_{DQ} of 1500 mA.
5. Apply the RF signal.

The recommended bias sequence during power-down is as follows:

1. Turn off the RF signal.
2. Decrease the gate bias voltages, V_{GG1} and V_{GG2}, to −1.5 V to achieve a I_{DQ} = 0 mA (approximately).
3. Decrease all the drain bias voltages, V_{DDx}, to 0 V.
4. Increase the gate bias voltages, V_{GG1} and V_{GG2}, to 0 V.

The V_{DD} = 5 V and I_{DQ} = 1500 mA bias conditions are recommended to optimize overall performance. Unless otherwise noted, the data shown was taken using the recommended bias conditions. Operation of the ADPA7008CHIP at different bias conditions may provide performance that differs from what is shown in Table 1, Table 2, Table 3, and Table 4. Biasing the ADPA7008CHIP for higher drain current typically results in higher P1dB and gain at the expense of increased power consumption (see Table 9).

TYPICAL APPLICATION CIRCUIT

Figure 56 shows the primary application circuit. Figure 57 shows the alternate primary application circuit.

Table 9. Power Selection Table[1, 2]

I_{DQ} (mA)	Gain (dB)	P1dB (dBm)	Output IP3 (dBm)	P_{DISS} (W) at P_{SAT}	V_{GGx} (V)
1300	18.9	30.0	39.8	7.9	−0.65
1500	19.6	30.4	38.4	8.4	−0.6
1700	20.1	30.7	36.6	8.9	−0.55

[1] Data taken at the following nominal bias conditions: V_{DD} = 5 V, T_A = 25°C, and frequency = 36 GHz.
[2] Adjust V_{GG1} from −1.5 V to 0 V to achieve the desired drain current.

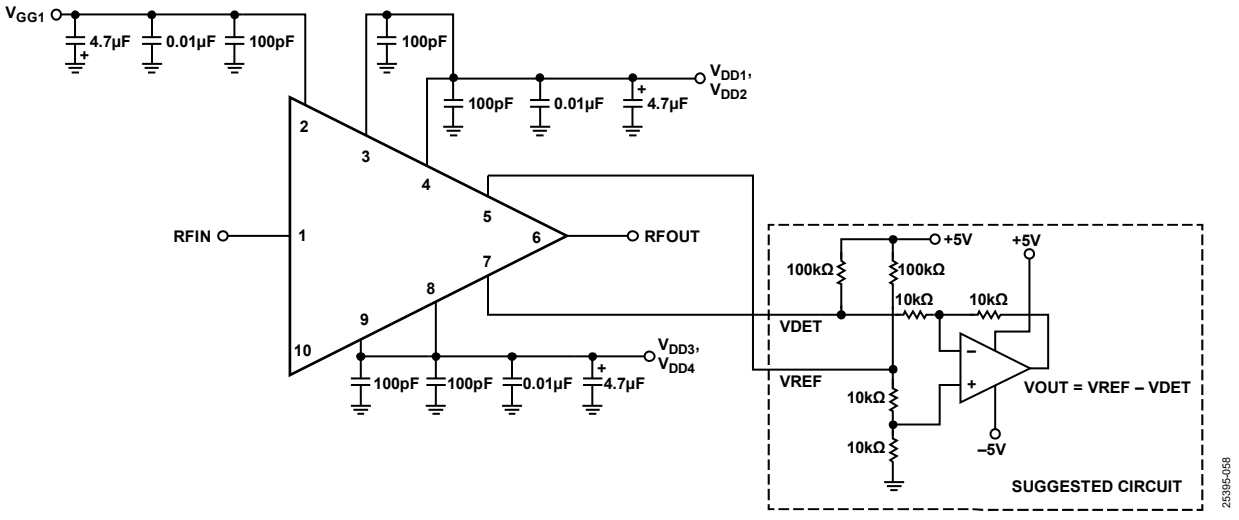

Figure 56. Primary Application Circuit

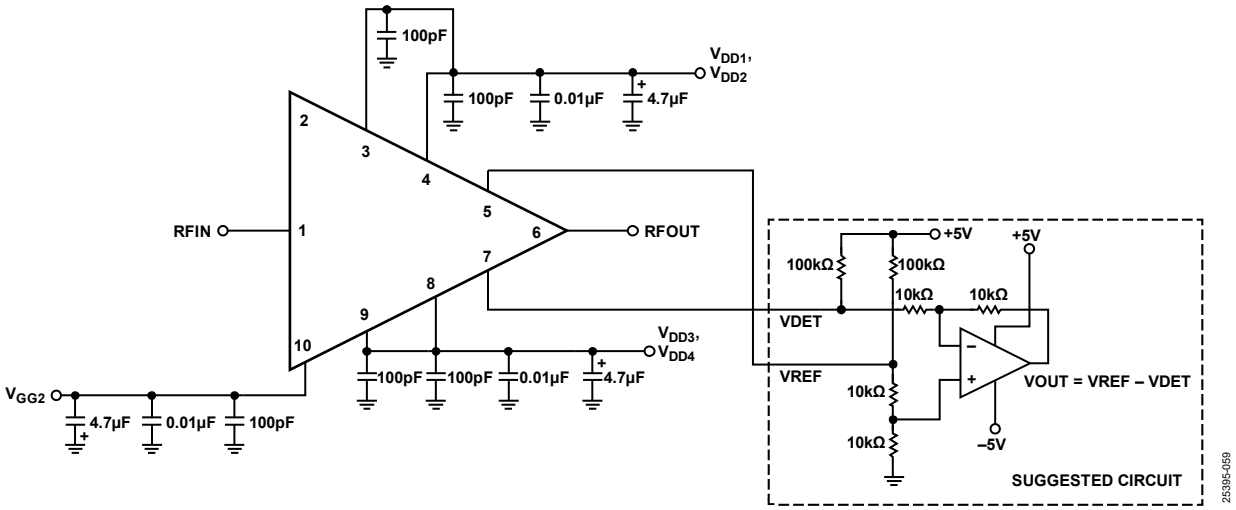

Figure 57. Alternate Application Circuit

BIASING ADPA7008CHIP WITH THE HMC980LP4E

The HMC980LP4E is an active bias controller that is designed to meet the bias requirements for enhancement mode and depletion mode amplifiers such as the ADPA7008CHIP. The controller provides constant drain current biasing over temperature and device to device variation, and properly sequences gate and drain voltages to ensure the safe operation of the amplifier. The HMC980LP4E also offers self protection in the event of a short circuit, an internal charge pump that generates the negative voltage needed on the gate of the ADPA7008CHIP, and the option to use an external negative voltage source. Because the HMC980LP4E can deliver a maximum current of 1.6 A and because the ADPA7008CHIP requires a peak current of I_{DD} = 1.7 A, two HMC980LP4E devices must be used in parallel in this instance.

The HMC980LP4E is also available in die form as the HMC980-Die.

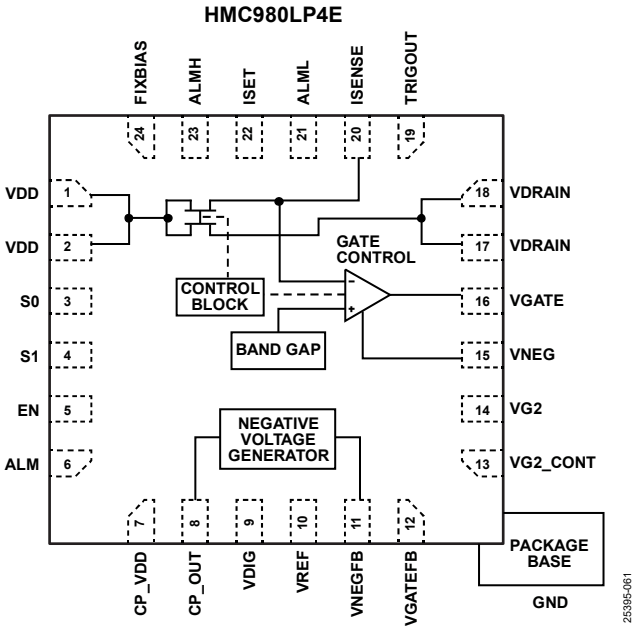

Figure 58. Functional Diagram of HMC980LP4E

APPLICATION CIRCUIT SETUP

Figure 59 shows an application circuit using the HMC980LP4E to control the ADPA7008CHIP. When using an external negative supply for VNEG, refer to the schematic in Figure 60.

In the application circuit shown in Figure 59, the ADPA7008CHIP drain voltage, V_{DRAIN}, and drain current, I_{DRAIN}, are set by the following equations:

$$V_{DD} = V_{DRAIN} + (I_{DRAIN} \times 0.85\ \Omega) \quad (1)$$

$$V_{DD} = 5\ V + (0.85\ A \times 0.85\ \Omega) = 5.72\ V$$

where:
V_{DD} and V_{DRAIN} are in volts.
I_{DRAIN} is in amperes.

$$R10 = (150\ \Omega \times A) \div (I_{DRAIN}) \quad (2)$$

$$R10 = (150\ \Omega \times A) \div (0.85\ A) = 176\ \Omega$$

where:
R10 is in ohms.
I_{DRAIN} is in amperes.

I_{DRAIN} is set to 850 mA in these equations because the current is split between two HMC980LP4E devices. Because both I_{SENSE} currents flow through the same resistor, the actual value used must be half of the above value (that is, 88 Ω).

LIMITING VGATE FOR THE ADPA7008CHIP V_{GGx} ABSOLUTE MAXIMUM RATING REQUIREMENT

When using the HMC980LP4E to control the ADPA7008CHIP, the minimum voltages for VNEG and VGATE must be −1.5 V to keep the voltages within the absolute maximum rating limit for the V_{GGx} pad of the ADPA7008CHIP. To set the minimum voltages, set R15 and R16 to the values shown in Figure 59 and set R16 to the value shown in Figure 60. Refer to the AN-1363 for more information and calculations for R15 and R16.

The HMC980LP4E application circuits for biasing figures in the AN-1363 are two examples of how the HMC980LP4E is used as an active bias controller. Both application circuits within the AN-1363 show the R5 and R7 resistors, which are analogous to the R15 and R16 resistor shown in Figure 59 and Figure 60.

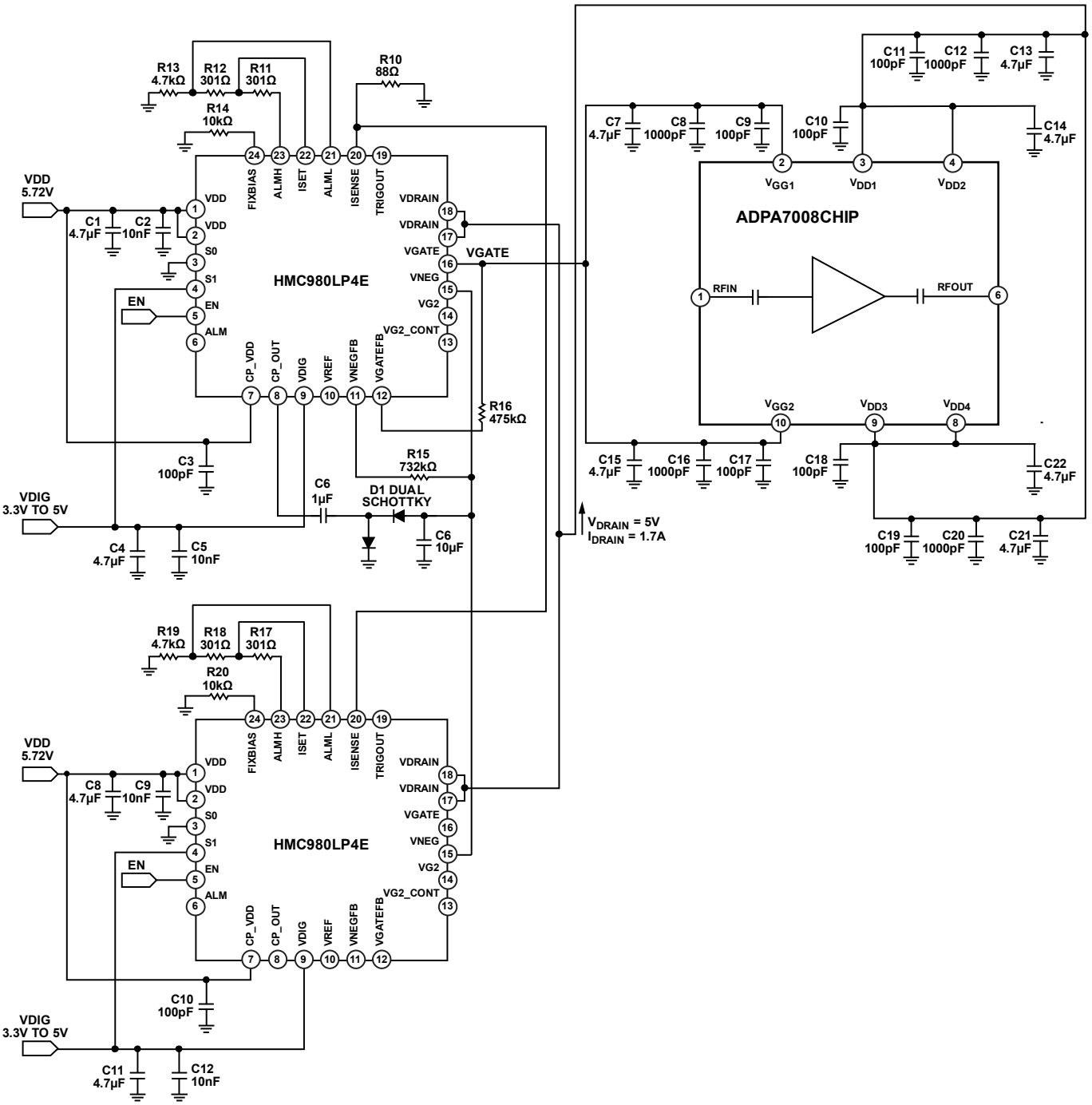

Figure 59. Application Circuit Using HMC980LP4E with ADPA7008CHIP (Internal Negative Voltage Source)

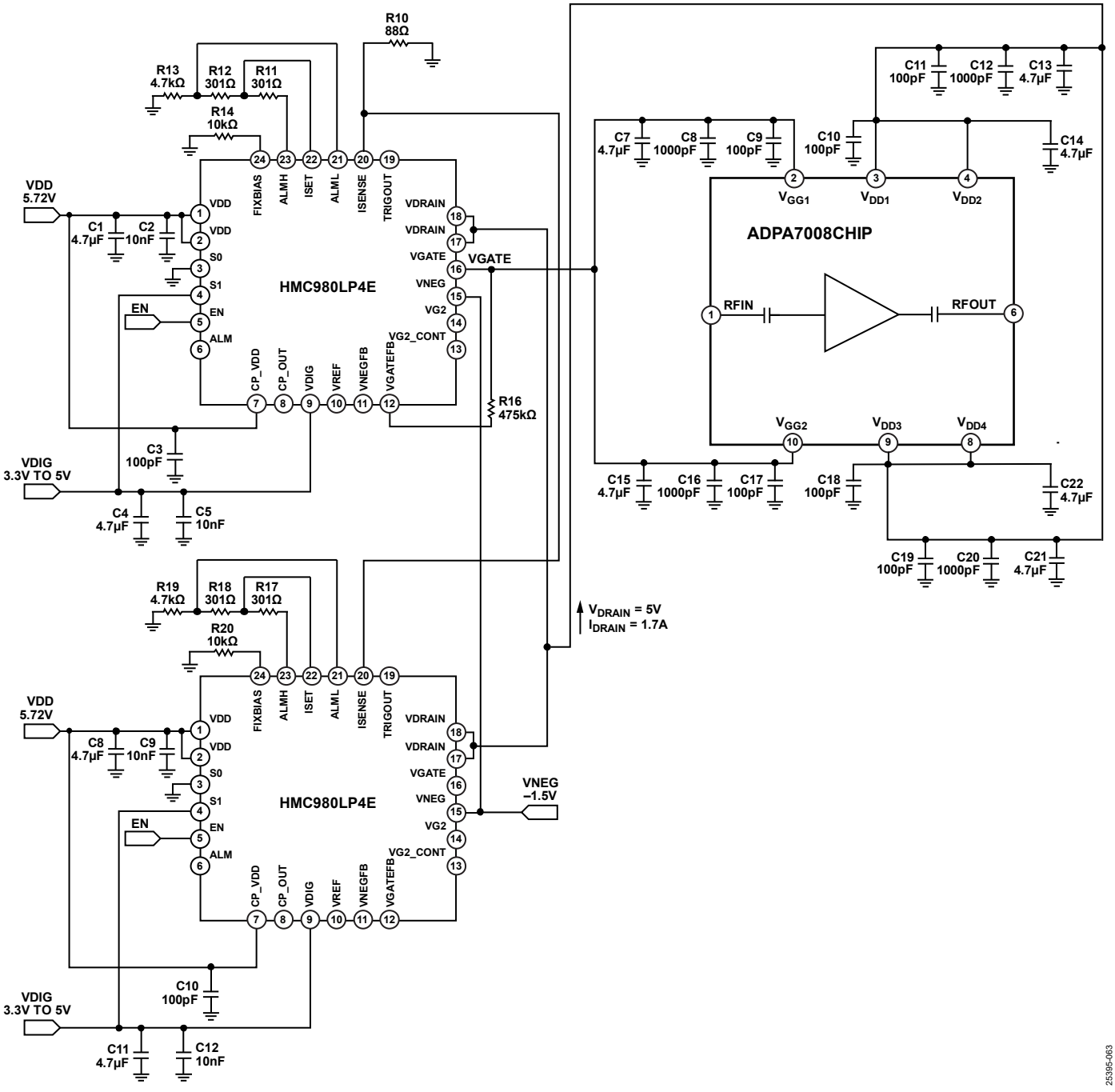

Figure 60. Application Circuit Using HMC980LP4E with ADPA7008CHIP (External Negative Voltage Source

HMC980LP4E BIAS SEQUENCE

The dc supply sequence described in this section is required to prevent damage to the HMC980LP4E when using the device to control the ADPA7008CHIP.

Power-Up Sequence

The power-up sequence for the HMC980LP4E is as follows:

1. Set VDIG = 3.3 V
2. Set S0 = 3.3 V
3. Set V_{DD} = 5.72 V.
4. Set VNEG = −1.5 V (this step is unnecessary if using internally generated voltage)
5. Set EN = 3.3 V (the transition from 0 V to 3.3 V turns on VGATE and VDRAIN).

Power-Down Sequence

The power-down sequence for the HMC980LP4E is as follows:

1. Set EN = 0 V (the transition from 3.3 V to 0 V turns off VDRAIN and VGATE).
2. Set VNEG = 0 V (this step is unnecessary if using internally generated voltage)
3. Set V_{DD} = 0 V.
4. Set S0 = 0 V
5. Set VDIG = 0 V

After the HMC980LP4E bias control circuit is set up, toggle the bias to the ADPA7008CHIP on or off by applying 3.3 V or 0 V, respectively, to the EN pad. At EN = +3.3 V, VGATE drops to −1.5 V, and VDRAIN turns on at +5 V. VGATE then rises until I_{DRAIN} = 1700 mA, and the closed control loop regulates I_{DRAIN} at 1600 mA. When EN = 0 V, VGATE is set to −1.5 V, and VDRAIN is set to 0 V.

CONSTANT DRAIN CURRENT BIASING vs. CONSTANT GATE VOLTAGE BIASING

The HMC980LP4E uses closed-loop feedback to continuously adjust VGATE to maintain a constant drain current bias over dc supply variation, temperature, and device to device variation. In addition, constant drain current bias is the optimum method for reducing time in calibration procedures and for maintaining consistent performance over time. By comparing the constant drain current bias with a constant gate voltage bias where the current is driven to increase when RF power is applied, a slightly lower output P1dB is seen with a constant drain current bias. This output P1dB is shown in Figure 61 and Figure 63, where the RF performance is slightly lower than the constant gate voltage bias operation due to a lower drain current at the high input powers as the device reaches 1 dB compression.

To increase the output P1dB performance for the constant drain current bias toward the constant gate voltage bias performance, increase the set current toward the I_{DD} value this performance reaches under the RF drive in the constant gate voltage bias condition, as shown in Figure 61 and Figure 63. The limit of increasing I_{DQ} under the constant drain current operation is set by the thermal limitations found in Table 5 with the maximum power dissipation specification. As I_{DD} increase continues, the actual output P1dB does not continue to increase indefinitely, and the power dissipation increases. Therefore, when using constant drain current biasing, take the trade-off between the power dissipation and the output P1dB performance.

CONSTANT I_{DD} OPERATION

T_A = 25°C, V_{DD} = 5 V, and I_{DQ} = 1700 mA for nominal operation, unless otherwise noted. Figure 61 to Figure 64 are biased with the HMC980LP4E active bias controller. See the Biasing ADPA7008CHIP with the HMC980LP4E section for biasing details.

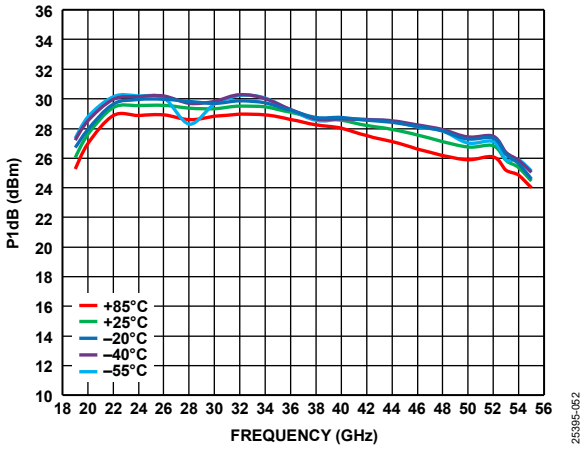

Figure 61. P1dB vs. Frequency for Various Temperatures, V_{DD} = 5 V, Data Measured with Constant I_{DD}

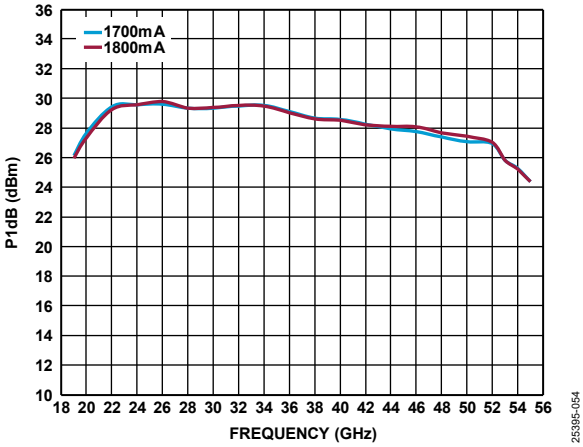

Figure 63. P1dB vs. Frequency for Various Drain Currents, V_{DD} = 5 V, Data Measured with Constant I_{DD}

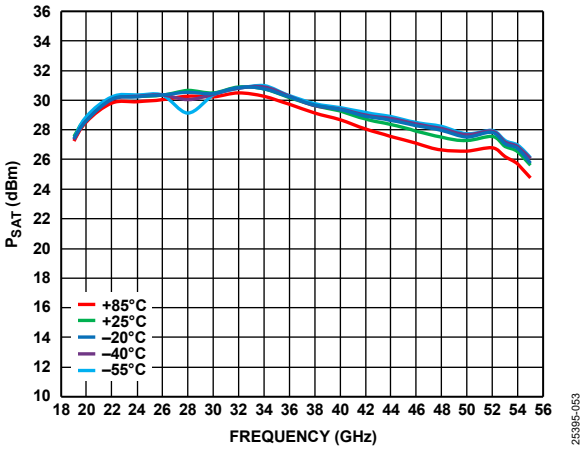

Figure 62. P_{SAT} vs. Frequency for Various Temperatures, V_{DD} = 5 V, Data Measured with Constant I_{DD}

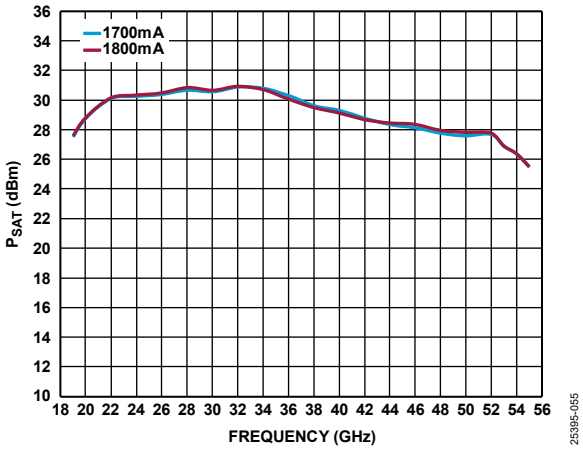

Figure 64. P_{SAT} vs. Frequency for Various Drain Currents, V_{DD} = 5 V, Data Measured with Constant I_{DD}

ASSEMBLY DIAGRAM

Figure 65 shows the assembly diagram for the ADPA7008CHIP.

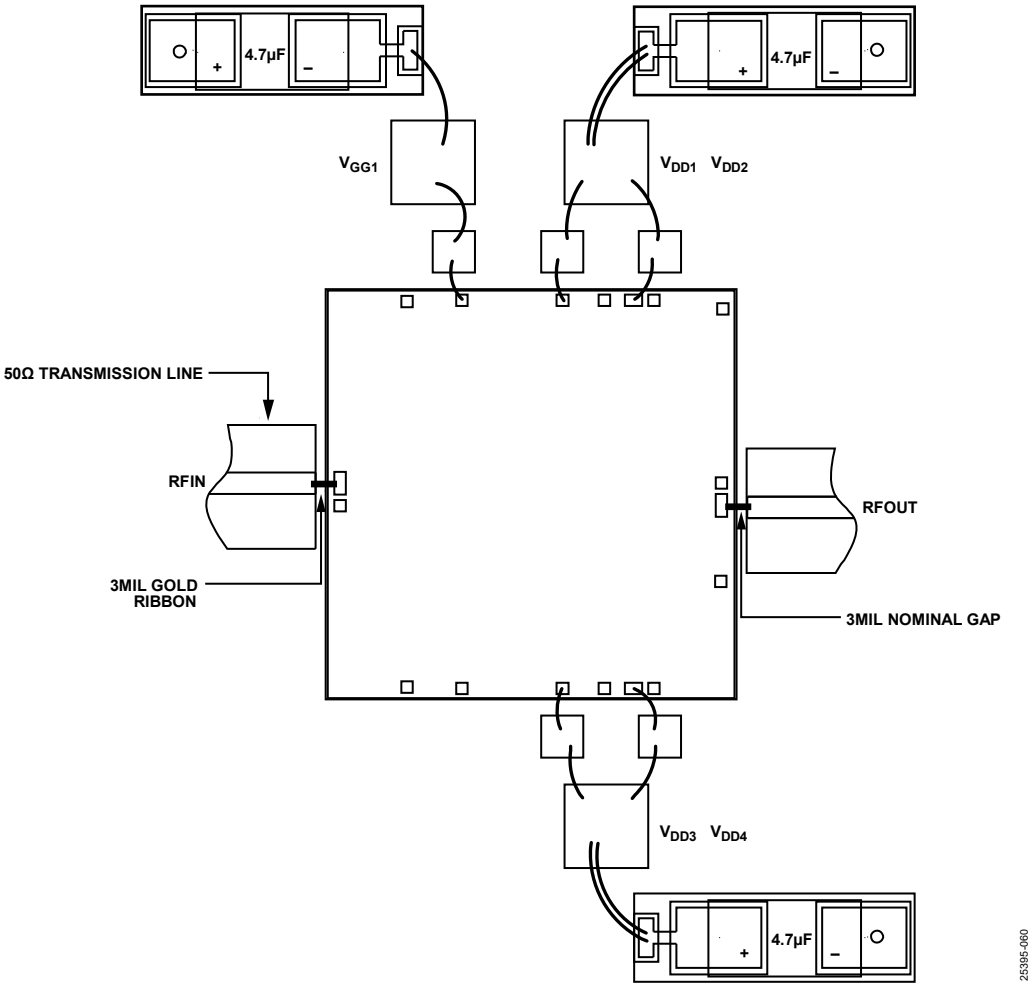

Figure 65. Assembly Diagram

MOUNTING AND BONDING TECHNIQUES FOR MILLIMETERWAVE GaAs MMICS

Attach the die directly to the ground plane with conductive epoxy (see the Handling Precautions section, the Mounting section, and the Wire Bonding section).

Place the microstrip substrates as close to the die as possible to minimize ribbon bond length. Typical die to substrate spacing is 0.076 mm to 0.152 mm (3 mil to 6 mil).

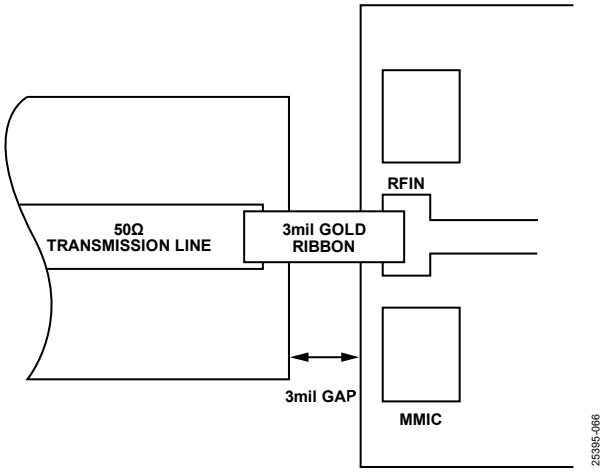

Figure 66. High Frequency Input Wideband Matching

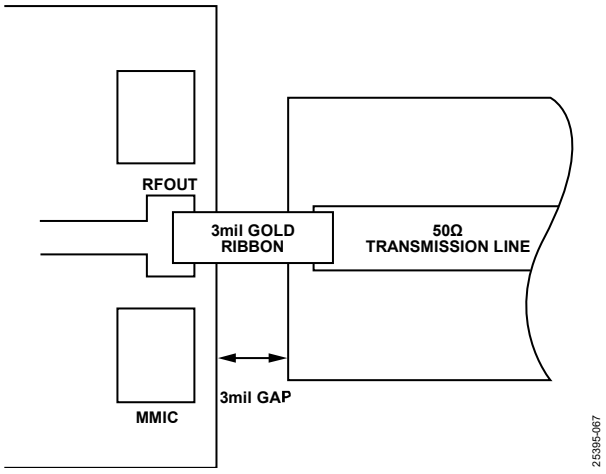

Figure 67. High Frequency Output Wideband Matching

HANDLING PRECAUTIONS

To avoid permanent damage, follow these storage, cleanliness, static sensitivity, transient, and general handling precautions:

- Place all bare die in either waffle- or gel-based ESD protective containers and then seal the die in an ESD protective bag for shipment. After the sealed ESD protective bag is opened, store all die in a dry nitrogen environment.
- Handle the chips in a clean environment. Do not attempt to clean the chips using liquid cleaning systems.
- Follow ESD precautions to protect against ESD strikes.
- While bias is applied, suppress instrument and bias supply transients. Use shielded signal and bias cables to minimize inductive pickup.
- Handle the chip along the edges with a vacuum collet or with a sharp pair of tweezers. The surface of the chip has fragile air bridges and must not be touched with a vacuum collet, tweezers, or fingers.

MOUNTING

Before the epoxy die is attached, apply a minimum amount of epoxy to the mounting surface so that a thin epoxy fillet is observed around the perimeter of the chip after it is placed into position. Cure the epoxy per the schedule of the manufacturer.

WIRE BONDING

RF bonds made with 0.076 mm × 0.0127 mm (3 mil × 0. 5 mil) gold ribbon are recommended for the RF ports. These bonds must be thermosonically bonded with a force of 40 g to 60 g. Thermosonically bonded dc bonds of 0.025 mm (1 mil) diameter are recommended. Create ball bonds with a force of 40 g to 50 g, and wedge bonds with a force of 18 g to 22 g. Create all bonds with a nominal stage temperature of 150°C. Apply the minimum amount of ultrasonic energy (depending on the process and package being used) to achieve reliable bonds. Keep all bonds as short as possible, less than 0.31 mm (12.2 mil).

Alternatively, use short RF bonds that are ≤3 mm and made with two 1 mm wires.