

FEATURES

Multifunction photometric front end Fully integrated AFE, ADC, LED drivers, and timing core Enables ambient light rejection capability without the need for photodiode optical filters Three 370 mA LED peak current drivers Flexible, multiple, short LED pulses per optical sample 20-bit burst accumulator enabling 20 bits per sample period On-board sample to sample accumulator, enabling up to 27 bits per data read Low power operation SPI, I 2C interface, and 1.8 V analog/digital core Flexible sampling frequency ranging from 0.122Hz to 2700Hz

FIFO data operation

Qualified for automotive applications

APPLICATIONS

Wearable health and fitness monitors Clinical measurements, for example, SpO2 Industrial monitoring Background light measurements

Photometric Front Ends

Data Sheet **[ADPD1080](https://www.analog.com/ADPD1080?doc=ADPD1080-1081.pdf)[/ADPD1081](https://www.analog.com/ADPD1081?doc=ADPD1080-1081.pdf)**

GENERAL DESCRIPTION

The ADPD1080/ADPD1081 are highly efficient, photometric front ends, each with an integrated 14-bit analog-to-digital converter (ADC) and a 20-bit burst accumulator that works with flexible light emitting diode (LED) drivers. The ADPD1080/ ADPD1081 stimulate an LED and measures the corresponding optical return signal. The data output and functional configuration occur over a 1.8 V I 2 C interface on the ADPD1080 or a serial port interface (SPI) on the ADPD1081. The control circuitry includes flexible LED signaling and synchronous detection.

The analog front end (AFE) features rejection of signal offset and corruption due to modulated interference commonly caused by ambient light without the need for optical filters or dc cancellation circuitry that requires external control.

Couple the ADPD1080/ADPD1081 with a low capacitance photodiode of <100 pF for optimal performance. The ADPD1080/ ADPD1081 can be used with any LED. The ADPD1080 is available in a 16-ball, 2.46 mm \times 1.4 mm WLCSP and a 28-lead, 4 mm \times 4 mm LFCSP. The SPI only version, ADPD1081, is available in a 17-ball, 2.46 mm \times 1.4 mm WLCSP.

Rev. C [Document Feedback](https://form.analog.com/Form_Pages/feedback/documentfeedback.aspx?doc=ADPD1080-1081.pdf&product=ADPD1080%20ADPD1081&rev=C)

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ADPD1080/ADPD1081

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REVISION HISTORY

10/2018—Rev. A to Rev. B

7/2018—Rev. 0 to Rev. A

1/2018—Revision 0: Initial Version

FUNCTIONAL BLOCK DIAGRAMS

Figure 1. Block Diagram for ADPD1080/ADPD1081 WLCSP (Chip Scale Package) Versions

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SPECIFICATIONS

TEMPERATURE AND POWER SPECIFICATIONS

Operating Conditions

Table 1.

Current Consumption

 $AVDD = DVD = 1.8 V$, ambient temperature $(T_A) = 25°C$, unless otherwise noted.

Table 2.

 1 V_{DD} is the voltage applied at the AVDD and DVDD pins.

² System power dissipation is the total average power dissipation, including the AFE V_{DD} supply plus the V_{LED} power supply to the LEDs.

PERFORMANCE SPECIFICATIONS

 $AVDD = DVDD = 1.8 V$, $T_A = 25°C$, unless otherwise noted.

¹ LED inductance is negligible for these values. The effective slew rate slows with increased inductance.

² Minimum LED period = $(2 \times$ AFE width) + 5 µs.

⁵ This setting is not recommended for photodiodes because it causes a 1.3 V forward-bias of the photodiode.

 3 The maximum values in this specification are the internal ADC sampling rates in normal mode using the internal 32 kHz state machine clock. The I²C read rates in some configurations may limit the output data rate.

⁴ This mode can induce additional noise and is not recommended unless necessary. The 1.8 V setting uses V_{DD}, which contains greater amounts of differential voltage noise with respect to the anode voltage.

ANALOG SPECIFICATIONS

AVDD = DVDD = 1.8 V, TA = 25°C, unless otherwise noted. Compensation of the AFE offset is explained in th[e AFE Operation](#page-25-0) section.

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¹ This saturation level applies to the ADC only and, therefore, includes only the pulsed signal. Any nonpulsatile signal is removed prior to the ADC stage.

² ADC resolution is listed per pulse when the AFE offset is correctly compensated per the AFE [Operation](#page-25-0) section. If using multiple pulses, divide by the number of pulses. ³ This saturation level applies to the full signal path and, therefore, includes both the ambient signal and the pulsed signal. The linear dynamic range of the TIA is 85% of the TIA saturation levels shown.

⁴ The noise term of the saturation SNR value refers to the receiver noise only and does not include photon shot noise or any noise on the LED signal itself.

DIGITAL SPECIFICATIONS

DVDD = 1.7 V to 1.9 V, TA = -40°C to 105°C, unless otherwise noted.

Table 5.

¹ This pin is only available as part of the I²C interface on the ADPD1080.
² This pin is only available as part of the SPI port on the ADPD1081.

TIMING SPECIFICATIONS

DVDD = 1.7 V to 1.9 V, T_A = -40° C to +105°C, unless otherwise noted.

I 2 C Timing Specifications

Table 6.

I 2 C Timing Diagram

Figure 3. I2 C Timing Diagram

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SPI Timing Specifications

DVDD = 1.7 V to 1.9 V, T_A = −40°C to +85°C, unless otherwise noted.

Table 7.

SPI Timing Diagram

Figure 4. SPI Timing Diagram

ABSOLUTE MAXIMUM RATINGS

Table 8. ADPD1080 Absolute Maximum Rating

Table 9. ADPD1081 Absolute Maximum Rating

Stresses at or above those listed under Absolute Maximum Ratings may cause permanent damage to the product. This is a stress rating only; functional operation of the product at these or any other conditions above those indicated in the operational section of this specification is not implied. Operation beyond the maximum operating conditions for extended periods may affect product reliability.

THERMAL RESISTANCE

Thermal performance is directly linked to printed circuit board (PCB) design and operating environment. Close attention to PCB thermal design is required.

θ_{JA} is the junction to ambient thermal resistance value, and θ_{JC} is the junction to case thermal resistance value.

Table 10. Thermal Resistance

¹ Thermal impedance simulated values are based on a JEDEC 2S2P board and 2 thermal vias. See JEDEC JESD-51.

RECOMMENDED SOLDERING PROFILE

[Figure 5](#page-12-4) and [Table](#page-12-5) 11 provide details about the recommended soldering profile.

Table 11. Recommended Soldering Profile

ESD CAUTION

ESD (electrostatic discharge) sensitive device. Charged devices and circuit boards can discharge without detection. Although this product features patented or proprietary protection circuitry, damage may occur on devices subjected to high energy ESD. Therefore, proper ESD precautions should be taken to avoid performance degradation or loss of functionality.

PIN CONFIGURATIONS AND FUNCTION DESCRIPTIONS

Figure 6. 28-Lead LFCSP Pin Configuration (ADPD1080)

Table 12. 28-Lead LFCSP Pin Function Descriptions (ADPD1080)

¹ DIO means digital input/output, S means supply, REF means voltage reference, AI means analog input, AO means analog output, R means reserved, and DI means digital input.

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Figure 7. 16-Ball WLCSP Pin Configuration (ADPD1080)

Table 13. 16-Ball WLCSP Pin Function Descriptions (ADPD1080)

¹ AO means analog output, S means supply, DIO means digital input/output, DI means digital input, REF means voltage reference, AI means analog input, and AO means analog output.

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Figure 8. 17-Ball WLCSP Pin Configuration (ADPD1081)

Table 14. 17-Ball WLCSP Pin Function Descriptions (ADPD1081)

¹ AO means analog output, S means supply, DIO means digital input/output, DO means digital output, DI means digital input, REF means voltage reference, and AI means analog input.

TYPICAL PERFORMANCE CHARACTERISTICS

Figure 10. 32 MHz Clock Frequency Distribution (Default Settings, Before User Calibration: Register 0x4D = 0x0098)

Figure 11. Referred to Input Noise vs. Transimpedance Amplifier Gain at CPD = 70 pF

Figure 12. LED Driver Current vs. LED Driver Voltage at 10% Drive Strength, Fine Setting at Default

Figure 13. LED Driver Current vs. LED Driver Voltage at 100% Drive Strength, Fine Setting at Default

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Figure 14. LED Driver Current vs. LED Fine Setting (Coarse Setting = 0x0)

Figure 15. LED Driver Current vs. LED Fine Setting (Coarse Setting = 0xF)

Figure 16. AC PSRR vs. Frequency for 75% Full-Scale Input Signal

THEORY OF OPERATION **INTRODUCTION**

The ADPD1080/ADPD1081 operate as a complete optical transceiver stimulating up to three LEDs and measuring the return signal on up to two separate current inputs. The core consists of a photometric front end coupled with an ADC, digital block, and three independent LED drivers. The core circuitry stimulates the LEDs and measures the return in the analog block through one to eight photodiode inputs, storing the results in discrete data locations. The two inputs can drive four simultaneous input channels. Data can be read directly by a register or through a first in, first out (FIFO) method. This highly integrated system includes an analog signal processing block, digital signal processing block, an I 2 C communication interface on the ADPD1080 or an SPI port on the ADPD1081, and programmable pulsed LED current sources.

The LED driver is a current sink and is agnostic to the LED supply voltage and the LED type. The photodiode (PDx) inputs can accommodate any photodiode with an input capacitance of less than 100 pF. The ADPD1080/ADPD1081 produces a high SNR for relatively low LED power while greatly reducing the effect of ambient light on the measured signal.

DUAL TIME SLOT OPERATION

The ADPD1080/ADPD1081 operate in two independent time slots, Time Slot A and Time Slot B, that operate sequentially. The entire signal path from LED stimulation to data capture and processing executes during each time slot. Each time slot has a separate datapath that uses independent settings for the LED driver, AFE setup, and the resulting data. Time Slot A and Time Slot B operate in sequence for every sampling period, as shown in [Figure 17.](#page-18-3)

The timing parameters for Time Slot A and Time Slot B are defined as follows:

 t_A (μ s) = *SLOTA_LED_OFFSET* + $n_A \times$ *SLOTA_PERIOD*

where n_A is the number of pulses for Time Slot A (Register 0x31, Bits[15:8]).

```
t_B (\mus) = SLOTB_LED_OFFSET + n_B \times SLOTB_PERIOD
```
where n_B is the number of pulses for Time Slot B (Register 0x36, Bits[15:8]).

Calculate the LED period using the following equation:

LED_PERIOD, minimum = 2 × *SLOTx_AFE_WIDTH* + 11

 t_1 and t_2 are fixed and based on the computation time for each slot. If a slot is not in use, these times do not add to the total active time. [Table 15](#page-18-4) defines the values for these LED and sampling time parameters.

Figure 17. Time Slot Timing Diagram (fSAMPLE is the sampling frequency (Register 0x12, Bits[15:0]).)

Table 15. LED Timing and Sample Timing Parameters

Parameter	Register	Bits	Test Conditions/Comments	Min	Typ	Max	Unit
SLOTA LED OFFSET ¹	0x30	[7:0]	Delay from power-up to LEDA rising edge	23		63	μs
SLOTB LED OFFSET ¹	0x35	$[7:0]$	Delay from power-up to LEDB rising edge	23		63	LIS
SLOTA PERIOD ²	0x31	[7:0]	Time between LED pulses in Time Slot A; SLOTx_AFE_WIDTH = $4 \mu s$	19		63	LIS
SLOTB PERIOD ²	0x36	[7:0]	Time between LED pulses in Time Slot B; SLOTx_AFE_WIDTH = $4 \mu s$	19		63	LIS
t_1	N/A	N/A	Compute time for Time Slot A		68		LIS
t ₂	N/A	N/A	Compute time for Time Slot B		20		LIS
tsleep	N/A	N/A	Sleep time between sample periods	222			μs

¹ Setting the SLOTx LED OFFSET less than the specified minimum value can cause failure of ambient light rejection for large photodiodes.

² Setting the SLOTx_LED_PERIOD less than the specified minimum value can cause invalid data captures.

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TIME SLOT SWITCH

ADPD1080 LFCSP Input Configurations

Up to eight photodiodes (PD1 to PD8) can be connected to the ADPD1080 for the LFCSP. The photodiode anodes are connected to the PD1 to PD8 input pins; the photodiode cathodes are connected to the cathode pin, PDC. The anodes are assigned in seven different configurations depending on the settings of Register 0x14 (see [Figure 18](#page-19-1) throug[h Figure 24\)](#page-20-0).

[Figure 18](#page-19-1) through [Figure 24](#page-20-0) show multiple configurations that can be used. The configuration selected depends on the requirements of the application. Depending on the dynamic range requirements of the application, 1-, 2-, or 4-channel modes can be selected. There are also several modes where input pins can be multiplexed together in cases where photodiode currents must be summed.

Se[e Table 16](#page-20-1) for the time slot switch settings. It is important to leave any unused inputs floating for proper operation of the devices. The photodiode inputs are current inputs and as such, these pins are considered voltage outputs. Tying these inputs to a voltage saturates the analog block.

Figure 20. PD1 to PD4 Connections with Register 0x14, Bits[11:8] and Bits[7:4] = 3 for the LFCSP

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INPUT CONFIGURATION FOR REGISTER 0x14[11:8] = 4 REGISTER 0x14[7:4] = 4 16110-021

Figure 21. PD5 to PD8 Connections with Register 0x14, Bits[11:8] and Bits[7:4] = 4 for the LFCSP

Figure 18. PD1 to PD4 Connections with Register 0x14, Bits[11:8] and Bits[7:4] = 1 for the LFCSP

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Figure 19. PD5 to PD8 Connections with Register 0x14, Bits[11:8] and Bits[7:4] = 2 for the LFCSP

Figure 23. PD3 to PD6 Connections with Register 0x14, Bits[11:8] and Bits[7:4] = 6 for the LFCSP

16110-024 **INPUT CONFIGURATION FOR REGISTER 0x14[11:8] = 7 REGISTER 0x14[7:4] = 7**

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Figure 24. PD5 to PD8 Connection with Register 0x14, Bits[11:8] and Bits[7:4] = 4 for the LFCSP

Table 16. Time Slot Switch (Register 0x14), ADPD1080 LFCSP											
		Channel									
Register, Bits, and Time Slot	Setting			3							
Register 0x14, Bits[11:8] for Time Slot B and Bits[7:4] for Time Slot A	0	No connect	No connect	No connect	No connect						
		PD3, PD4	PD1, PD2	No connect	No connect						
	$\overline{2}$	PD7, PD8	PD5, PD6	No connect	No connect						
		PD1 to PD4	No connect	No connect	No connect						
	4	PD ₅	PD ₆	PD7	PD ₈						
	5	P _D 1	P _D ₂	PD ₃	PD ₄						
	6	PD3, PD4	PD5, PD6	No connect	No connect						
		PD5 to PD8	No connect	No connect	No connect						

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WLCSP Input Configurations

Up to two photodiodes can be connected to the PD1 and PD5 input pins of the ADPD1080 and ADPD1081 WLCSP models. The photodiode anodes are connected to the PD1 and PD5 input pins; the photodiode cathodes are connected to the cathode pin, PDC. The anodes are assigned in the configurations shown in [Figure 25](#page-21-0) an[d Figure 26](#page-21-1) based on the bit settings of Register 0x14.

See [Table 17](#page-21-2) for the time slot switch settings. It is important to leave any unused inputs floating for proper operation of the devices. The photodiode inputs are current inputs and, as such, these pins are also considered voltage outputs. Tying these inputs to a voltage saturates the analog block.

Figure 25. PD5 Connection with Register 0x14, Bits[11:8] and Bits[7:4] = 4 for the WLCSP

026 16110-026 **REGISTER 0x14[11:8] = 5 REGISTER 0x14[7:4] = 5**

Figure 26. PD1 Connection with Register 0x14, Bits[11:8] and Bits[7:4] = 5 for the WLCSP

Table 17. Time Slot Switch (Register 0x14), ADPD1080/ADPD1081 WLCSP

ADJUSTABLE SAMPLING FREQUENCY

Register 0x12 controls the sampling frequency setting of the ADPD1080/ADPD1081 and Register 0x4B, Bits[5:0] further tunes this clock for greater accuracy. An internal 32 kHz sample rate clock that also drives the transition of the internal state machine governs the sampling frequency. The maximum sampling frequencies for some sample conditions are listed in [Table 3.](#page-6-3) The maximum sample frequency for all conditions is determined by the following equation:

 $f_{SAMPLE, MAX} = 1/(t_A + t_I + t_B + t_2 + t_{SLEEP, MIN})$

where *t_{SLEEP}*, MIN is the minimum sleep time required between samples. Se[e Table 15.](#page-18-4)

If a given time slot is not in use, elements from that time slot do not factor into the calculation. For example, if Time Slot A is not in use, t_A and t_1 do not add to the sampling period and the new maximum sampling frequency is calculated as follows:

 $f_{SAMPLE, MAX} = 1/(t_B + t_2 + t_{SLEEP, MIN})$

See the Dual [Time Slot Operation](#page-18-2) section for the definitions of t_A , t_B , and t_A . The maximum achievable sampling rate with a single pulse in Time Slot B is ~2.8 kSPS.

External Sync for Sampling

The ADPD1080/ADPD1081 provide an option to use an external sync signal to trigger the sampling periods. This external sample sync signal can be provided either on the GPIO0 pin or the GPIO1 pin. This functionality is controlled by Register 0x4F, Bits[3:2]. When enabled, a rising edge on the selected input specifies when the next sample cycle occurs. When triggered, there is a delay of one to two internal sampling clock (32 kHz) cycles, and then the normal start-up sequence occurs. This sequence is the same when the normal sample timer provides the trigger. To enable the external sync signal feature, use the following procedure:

- 1. Write 0x1 to Register 0x10 to enter program mode.
- 2. Write the appropriate value to Register 0x4F, Bits[3:2] to select whether the GPIO0 pin or the GPIO1 pin specifies when the next sample cycle occurs. Also, enable the appropriate input buffer using Register 0x4F, Bit 1, for the GPIO0 pin, or Register 0x4F, Bit 5, for the GPIO1 pin.
- 3. Write 0x4000 to Register 0x38.
- 4. Write 0x2 to Register 0x10 to start the sampling operations.
- 5. Apply the external sync signal on the selected pin at the desired rate; sampling occurs at that rate. As with normal sampling operations, read the data using the FIFO or the data registers.

The maximum frequency constraints also apply in this case.

Providing an External 32 kHz Clock

The ADPD1080/ADPD1081 have an option for the user to provide an external 32 kHz clock to the devices for system synchronization or for situations where a clock with better accuracy than the internal 32 kHz clock is required. The external 32 kHz clock is provided on the GPIO1 pin. To enable the 32 kHz external clock, use the following procedure at startup:

- 1. Drive the GPIO1 pin to a valid logic level or with the desired 32 kHz clock prior to enabling the GPIO1 pin as an input. Do not leave the pin floating prior to enabling it.
- 2. Write 01 to Register 0x4F, Bits[6:5] to enable the GPIO1 pin as an input.
- 3. Write 10 to Register 0x4B, Bits[8:7] to configure the devices to use an external 32 kHz clock. This setting disables the internal 32 kHz clock and enables the external 32 kHz clock.
- 4. Write 0x1 to Register 0x10 to enter program mode.
- 5. Write additional control registers in any order while the devices are in program mode to configure the devices as required.
- 6. Write 0x2 to Register 0x10 to start the normal sampling operation.

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STATE MACHINE OPERATION

During each time slot, the ADPD1080/ADPD1081 operate according to a state machine. The state machine operates in the sequence shown in [Figure 27.](#page-23-2)

Figure 27. State Machine Operation Flowchart

The ADPD1080/ADPD1081 operate in one of three modes: standby, program, and normal operation.

Standby mode is a power saving mode in which no data collection occurs. All register values are retained in this mode. To place the devices in standby mode, write 0x0 to Register 0x10, Bits[1:0]. The devices power up in standby mode.

Program mode is used for programming registers. Always cycle the ADPD1080/ADPD1081 through program mode when writing registers or changing modes. Because no power cycling occurs in

this mode, the devices may consume higher current in program mode than in normal operation. To place the devices in program mode, write 0x1 to Register 0x10, Bits[1:0].

In normal operation, the ADPD1080/ADPD1081 pulse light and collect data. Power consumption in this mode depends on the pulse count and data rate. To place the devices in normal sampling mode, write 0x2 to Register 0x10, Bits[1:0].

NORMAL MODE OPERATION AND DATA FLOW

In normal mode, the ADPD1080/ADPD1081 follow a specific pattern set up by the state machine. This pattern is shown in the corresponding datapath diagram shown in [Figure 28.](#page-23-3) The pattern is as follows:

- 1. LED pulse and sample. The ADPD1080/ADPD1081 pulse external LEDs. The response of a photodiode or photodiodes to the reflected light is measured by the ADPD1080/ ADPD1081. Each data sample is constructed from the sum of n individual pulses, where n is user configurable between 1 and 255.
- 2. Intersample averaging. If desired, the logic can average n samples, from 2 to 128 in powers of 2, to produce output data. New output data is saved to the output registers every N samples.
- 3. Data read. The host processor reads the converted results from the data register or the FIFO.
- 4. Repeat. The sequence has a few different loops that enable different types of averaging while keeping both time slots close in time relative to each other.

Figure 28. ADPD1080/ADPD1081 Datapath

LED Pulse and Sample

At each sampling period, the selected LED driver drives a series of LED pulses, as shown in [Figure 29.](#page-24-0) The magnitude, duration, and number of pulses are programmable over the I^2C interface. Each LED pulse coincides with a sensing period so that the sensed value represents the total charge acquired on the photodiode in response to only the corresponding LED pulse. Charge, such as ambient light, that does not correspond to the LED pulse is rejected.

After each LED pulse, the photodiode output relating the pulsed LED signal is sampled and converted to a digital value by the 14 bit ADC. Each subsequent conversion within a sampling period is summed with the previous result. Up to 255 pulse values from the ADC can be summed in an individual sampling period. There is a 20-bit maximum range for each sampling period.

Averaging

The ADPD1080/ADPD1081 offer sample accumulation and averaging functionality to increase signal resolution.

Within a sampling period, the AFE can sum up to 256 sequential pulses. As shown in [Figure 28,](#page-23-3) samples acquired by the AFE are clipped to 20 bits at the output of the AFE. Additional resolution, up to 27 bits, can be achieved by averaging between sampling periods. This accumulated data of N samples is stored as 27-bit values and can be read out directly by using the 32-bit output registers or the 32-bit FIFO configuration.

When using the averaging feature set up by Register 0x15, subsequent pulses can be averaged by powers of 2. The user can select from 2, 4, 8 … up to 128 samples to be averaged. Pulse data is still acquired by the AFE at the sampling frequency, f_{SAMPLE} (Register 0x12), but new data is written to the registers at the rate of $f_{\tt SAMPLE}/N$ every $N^{\rm th}$ sample. This new data consists of the sum of the previous N samples. The full 32-bit sum is stored in the 32-bit registers. However, before sending this data to the FIFO, a divide by N operation occurs. This divide operation maintains bit depth to prevent clipping on the FIFO.

Use this between sample averaging to lower the noise while maintaining 16-bit resolution. If the pulse count registers are kept to 8 or less, the 16-bit width is never exceeded. Therefore, when using Register 0x15 to average subsequent pulses, many pulses can be accumulated without exceeding the 16-bit word width. This averaging can reduce the number of FIFO reads required by the host processor.

Data Read

The host processor reads output data from the ADPD1080/ ADPD1081 via the I2 C protocol on the ADPD1080 or the SPI port on the ADPD1081. Data is read from the data registers or from the FIFO. New output data is made available every N samples, where N is the user configured averaging factor. The averaging factors for Time Slot A and Time Slot B are configurable independently of each other. If they are the same, both time slots can be configured to save data to the FIFO. If the two averaging factors are different, only one time slot can save data to the FIFO; data from the other time slot can be read from the output registers.

The data read operations are described in more detail in the [Reading Data](#page-33-2) section.

Figure 29. Example of a PPG Signal Sampled at a Data Rate of 10 Hz Using Five Pulses per Sample

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AFE OPERATION

The timing within each pulse burst is important for optimizing the operation of the ADPD1080/ADPD1081[. Figure 30](#page-25-2) shows the timing waveforms for a single time slot as an LED pulse response propagates through the analog block of the AFE. The first graph, shown in green, shows the ideal LED pulsed output. The filtered LED response, shown in blue, shows the output of the analog integrator. The third graph, shown in orange, shows an optimally placed integration window. When programmed to the optimized value, the full signal of the filtered LED response can be integrated. The AFE integration window is then applied to the output of the band-pass filter (BPF) and the result is sent to the ADC and summed for N pulses. If the AFE window is not correctly sized or located, all of the receive signal is not properly reported and system performance is not optimal; therefore, it is important to verify proper AFE position for every new hardware design or the LED width.

AFE INTEGRATION OFFSET ADJUSTMENT

The AFE integration width must be equal or larger than the LED width. As AFE width increases, the output noise increases and the ability to suppress high frequency content from the environment decreases. It is therefore desirable to keep the AFE integration width small. However, if the AFE width is too small, the LED signal is attenuated. With most hardware selections, the AFE width produces the optimal SNR at 1 μ s more than the LED width. After setting LED width, LED offset, and AFE width, the ADC offset can then be optimized. The AFE offset must be manually set such that the falling edge of the first segment of the integration window matches the zero crossing of the filtered LED response.

Figure 30. AFE Operation Diagram

AFE Integration Offset Starting Point

The starting point of the AFE integration offset, as expressed in microseconds, is set such that the falling edge of the integration window aligns with the falling edge of the LED.

LED_FALLING_EDGE = *SLOTx_LED_OFFSET* + *SLOTx_LED_WIDTH*

and,

AFE_INTEGRATION_FALLING_EDGE = 9 + *SLOTx_AFE_OFFSET + SLOTx_AFE_WIDTH*

If both falling edges are set equal to each other, solve for SLOTx_AFE_OFFSET to obtain the following equation:

AFE_OFFSET_STARTING_POINT = *SLOTx_LED_ OFFSET* + *SLOTx_LED_WIDTH* − 9 – *SLOTx_AFE_ WIDTH*

Setting the AFE offset to any point in time earlier than the starting point is equivalent to setting the integration in the future; the AFE cannot integrate the result from an LED pulse that has not yet occurred. As a result, a SLOTx_AFE_OFFSET value less than the AFE_OFFSET_STARTING_POINT value is an erroneous setting. Such a result may indicate that current in the TIA is operating in the reverse direction from intended, where the LED pulse is causing the current to leave the TIA rather than enter it.

Because, for most setups, the SLOTx_AFE_WIDTH is 1 µs wider than the SLOTx_LED_WIDTH, the AFE_OFFSET_ STARTING POINT value is typically 10 µs less than the SLOTx_LED_OFFSET value. Any value less than SLOTx_LED_

OFFSET − 10 is erroneous. The optimal AFE offset is some time after the AFE_OFFSET_STARTING_POINT value. The BPF response, LED response, and photodiode response each add some delay. In general, the component choice, board layout, SLOTx_LED_OFFSET, and SLOTx_LED_WIDTH are the variables that can change the SLOTx_AFE_OFFSET value. After a specific design is set, the SLOTx_AFE_OFFSET value can be locked down and does not need to be optimized further.

Sweeping the AFE Position

The AFE offsets for Time Slot A and Time Slot B are controlled by Bits[10:0] of Register 0x39 and Register 0x3B, respectively.

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Each LSB represents one cycle of the 32 MHz clock, or 31.25 ns. The register can be thought of as 2^{11-1} of these 31.25 ns steps, or it can be broken into an AFE coarse setting using Bits[10:5] to represent 1 µs steps and Bits[4:0] to represent 31.25 ns steps. Sweeping the AFE position from the starting point to find a local maximum is the recommended way to optimize the AFE offset. The setup for this test is to allow the LED light to fall on the photodiode in a static way. This test is typically done with a reflecting surface at a fixed distance. The AFE position can then be swept to look for changes in the output level. When adjusting the AFE position, it is important to sweep the position using the 31.25 ns steps. Typically, a local maximum is found within 2 µs of the starting point for most systems. [Figure](#page-26-0) [31](#page-26-0) shows an example of an AFE sweep, where 0 on the x-axis represents the AFE starting point defined previously. Each data point in [Figure 31](#page-26-0) corresponds to one 31.25 ns step of the SLOTx_AFE_OFFSET. The optimal location for SLOTx_AFE_OFFSET in this example is 0.687 µs from the AFE starting point.

[Table 18](#page-26-1) lists some typical LED and AFE values after optimization. In general, it is not recommended to use the SLOTx_AFE_OFFSET numbers i[n Table 18](#page-26-1) without first verifying them against the AFE sweep method. Repeat this method for every new LED width and with every new set of hardware made with the ADPD1080/ ADPD1081. For maximum accuracy, it is recommended that the 32 MHz clock be calibrated prior to sweeping the AFE.

I 2 C SERIAL INTERFACE

The ADPD1080 supports an I²C serial interface via the SDA (data) and SCL (clock) pins. All internal registers are accessed through the I^2C interface. The ADPD1080 is an I^2C only device and does not support an SPI.

The ADPD1080 conforms to the *UM10204 I2 C-Bus Specification and User Manual*, Rev. 05—9 October 2012, available from NXP Semiconductors. The I 2 C interface supports up to 1 Mbps data transfers. Register read and write are supported, as shown in [Figure 32.](#page-28-1) [Figure 3](#page-10-1) shows the timing diagram for the I²C interface.

Slave Address

The default 7-bit I^2C slave address for the device is 0x64, followed by the R/W bit. For a write, the default I 2 C slave address is 0xC8; for a read, the default I 2 C address is 0xC9. The slave address is configurable by writing to Register 0x09, Bits[7:1]. When multiple ADPD1080 devices are on the same bus lines, the GPIO0 and GPIO1 pins can be used to select specific devices for the address change. Register 0x0D can be used to select a key to enable address changes in specific devices. Use the following procedure to change the slave address when multiple ADPD1080 devices are connected to the same I²C bus lines:

- 1. Using Register 0x4F, enable the input buffer of the GPIO1 pin, the GPIO0 pin, or both, depending on the key being used.
- 2. For the device identified as requiring an address change, set the GPIO0 and/or GPIO1 pins high or low to match the key being used.
- 3. Write the SLAVE_ADDRESS_KEY bits using Register 0x0D, Bits[15:0] to match the desired function. The allowed keys are shown in [Table 42.](#page-65-1)
- 4. Write to the desired SLAVE_ADDRESS bits using Register 0x09, Bits[7:1]. While writing to Register 0x09, Bits[7:1], write 0xAD to Register 0x09, Bits[15:8] (ADDRESS_WRITE_KEY). Register 0x09 must be written to immediately after writing to Register 0x0D.
- 5. Repeat Step 1 to Step 4 for all the devices that need SLAVE_ADDRESS changed.
- 6. Set the GPIO0 and GPIO1 pins as desired for normal operation using the new SLAVE_ADDRESS for each device.

I 2 C Write and Read Operations

[Figure 32](#page-28-1) shows the ADPD1080 I 2 C write and read operations. Single-word and multiword read operations are supported. For a single register read, the host sends a no acknowledge (NACK) after the second data byte is read and a new register address is needed for each access.

For multiword operations, each pair of data bytes is followed by an acknowledge from the host until the last byte of the last word is read. The host indicates the last read word by sending a no acknowledge. When reading from the FIFO_ACCESS (Register 0x60), the data is automatically advanced to the next word in the FIFO, and the space is freed. When reading from other registers, the register address is automatically advanced to the next register, except at Register 0x5F (DATA_ACCESS_CTL) or Register 0x7F (B_PD4_HIGH), where the address does not increment. This auto-incrementing allows lower overhead reading of sequential registers.

All register writes are single word only and require 16 bits (one word) of data.

The software reset, SW_RESET (Register 0x0F, Bit 0), returns an acknowledge. The device then returns to standby mode with all registers in the default state.

Table 19. Definitions of I2 C Terminology

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NOTES 1. THE SHADED AREAS REPRESENT WHEN THE DEVICE IS LISTENING.

Figure 32. I2 C Write and Read Operations

SPI PORT

The ADPD1081 is a SPI only device. It does not support the I²C interface. The SPI port uses a 4-wire interface, consisting of the CS, MOSI, MISO, and SCLK signals, and it is always a slave port. The \overline{CS} signal goes low at the beginning of a transaction and high at the end of a transaction. The SCLK signal latches MOSI on a low to high transition. The MISO data is shifted out of the device on the falling edge of SCLK and must be clocked into a receiving device, such as a microcontroller, on the SCLK rising edge. The MOSI signal carries the serial input data, and the MISO signal carries the serial output data. The MISO signal remains three state until a read operation is requested, which allows other SPI-compatible peripherals to share the same MISO line. All SPI transactions have the same basic format shown in [Table 20.](#page-28-2) A timing diagram is shown in [Figure 4.](#page-11-0) Write all data MSB first.

Table 20. Generic Control Word Sequence

The first byte written in a SPI transaction is a 7-bit address, which is the location of the address being accessed, followed by the W/R bit. This bit determines whether the communication is a write (Logic Level 1) or a read (Logic Level 0). This format is shown in [Table 21.](#page-28-3)

Data on the MOSI pin is captured on the rising edge of the clock, and data is propagated on the MISO pin on the falling edge of the clock. The maximum read and write speed for the SPI slave port is 10 MHz. Se[e Figure 4](#page-11-0) for the SPI timing diagram, and se[e Table 7](#page-11-1) for the SPI timing specifications.

A sample timing diagram for a multiple word SPI write operation to a register is shown i[n Figure 33.](#page-29-0) A sample timing diagram of a single-word SPI read operation is shown i[n Figure 34.](#page-29-1) The MISO pin transitions from being three-state to being driven following the reception of a valid R bit. In this example, Byte 0 contains the address and the W/ \overline{R} bit and subsequent bytes carry the data. A sample timing diagram of a multiple word SPI read operation is shown i[n Figure 35.](#page-29-2) I[n Figure 33](#page-29-0) t[o Figure 35,](#page-29-2) rising edges on SCLK are indicated with an arrow, signifying that the data lines are sampled on the rising edge.

When performing multiple word reads or writes, the data address is automatically incremented to the next consecutive address for subsequent transactions except for Address 0x5F (DATA_ACCESS_CTL), Address 0x60 (FIFO_ACCESS), and Address 0x7F (B_PD4_HIGH).

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APPLICATIONS INFORMATION **TYPICAL CONNECTION DIAGRAM**

[Figure 36](#page-30-2) shows a typical circuit used for wrist-based heart rate measurement with the ADPD1080 WLCSP using a green LED. The 1.8 V I²C communication lines, SCL and SDA, along with the GPIO0 and GPIO1 lines, connect to a system microprocessor or sensor hub. The I²C signals can have pull-up resistors connected to a 1.8 V or a 3.3 V power supply. The GPIO0 and GPIO1 signals are only compatible with a 1.8 V supply and may need a level translator. The circuit shown i[n Figure 36](#page-30-2) is identical for the ADPD1081, except the I²C interface is replaced by an SPI. There are multiple ways to connect photodiodes to the 8-channel ADPD1080 LFCSP, as shown in [Table 22](#page-31-2) and [Figure 39.](#page-31-3) The photodiode anodes are connected to the PD1 to PD8 input pins and the photodiode cathodes are connected to the cathode pin, PDC.

Provide the 1.8 V supply, V_{DD}, to AVDD and DVDD. The LED supply uses a standard regulator circuit according to the peak current requirements specified in [Table 3](#page-6-3) and calculated in the [LED Driver Pins and LED Supply Voltage](#page-31-0) section.

For best noise performance, connect AGND, DGND, and LGND together at a large conductive surface, such as a ground plane, a ground pour, or a large ground trace.

The number of photodiodes or LEDs used varies depending on the application as well as the dynamic range and SNR required. For example, when using a single, large photodiode in an application, split the current between multiple inputs to increase the dynamic range. By connecting the anode of the photodiode to multiple channels, the current can split evenly among the number of channels connected, effectively increasing the dynamic range over a single channel configuration. Alternatively, in situations where the photodiode is small or the signal is greatly attenuated, SNR can be maximized by connecting the anode of the photodiode to a single channel. It is important to leave the unused input floating for proper device operation.

[Figure 37](#page-30-3) an[d Figure 38](#page-30-4) show the recommended connection diagram and printed circuit board (PCB) layout for the 16-ball WLCSP ADPD1080 and 17-ball WLCSP ADPD1081, respectively. The current input pins, PD1 and PD5, have a typical voltage of 1.3 V during the sampling period. During the sleep period, these pins are connected to the cathode pin. The cathode and anode voltages are listed i[n Table 3.](#page-6-3)

Figure 37. ADPD1080 Connection and PCB Layout Diagram (Top View), 16-Ball WLCSP

Figure 38. ADPD1081 Connection and PCB Layout Diagram, Dashed Line Traces from Blind Vias (Top View), 16-Ball WLCSP

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Table 22. Typical Photodiode Anode to Input Channel Connections for the ADPD1080 LFCSP1, 2

¹ Dx refers to the diode connected to the specified channel.

² NC means do not connect. Leave all unused inputs floating.

LED DRIVER PINS AND LED SUPPLY VOLTAGE

The LEDX1, LEDX2, and LEDX3 pins have an absolute maximum voltage rating of 3.6 V. Any voltage exposure over this rating affects the reliability of the device operation and, in certain circumstances, causes the device to cease proper operation. The voltage of the LEDx pins must not be confused with the supply voltages for the LED themselves. VLEDx is the voltage applied to the anode of the external LED, whereas the LEDXx pin is the input of the internal current driver, and the pins are connected to the cathode of the external LED.

LED DRIVER OPERATION

The LED driver for the ADPD1080/ADPD1081 is a current sink. The compliance voltage, measured at the driver pin with respect to ground, required to maintain the programmed LED current level is a function of the current required. [Figure 12](#page-16-1) shows the typical compliance voltages required at the various LED coarse settings. [Figure 40](#page-31-4) shows the basic schematic of how the ADPD1080/ADPD1081 connect to an LED through the LED driver. Th[e Determining the Average Current](#page-32-0) section and the Determining C_{VLED} section define the requirements for the bypass capacitor (CVLED) and the supply voltages of the LEDs (VLEDx).

Figure 40. VLEDx Supply Schematic

DETERMINING THE AVERAGE CURRENT

The ADPD1080/ADPD1081 drive an LED in a series of short pulses[. Figure 41](#page-32-2) shows the typical ADPD1080/ADPD1081 configuration of an LED pulse burst sequence.

Figure 41. Typical LED Pulse Burst Sequence Configuration

In this example, the LED pulse width, t_{LED_PULSE} , is 3 μs , and the LED pulse period, tLED_PERIOD, is 19 µs. The LED being driven is a pair of green LEDs driven to a 250 mA peak. The goal of CVLED is to buffer the LED between individual pulses. In the worst case scenario, where the pulse train shown i[n Figure 41](#page-32-2) is a continuous sequence of short pulses, the VLEDx supply must supply the average current. Therefore, calculate ILED_AVERAGE as follows:

$$
I_{LED_AVERAGE} = (t_{LED_PULSE}/t_{LED_PERIOD}) \times I_{LED_MAX}
$$
 (1)

where:

ILED_AVERAGE is the average current needed from the VLEDx supply during the pulse period, and it is also the VLEDx supply current rating.

ILED_MAX is the peak current setting of the LED.

For the values shown in Equation 1, $I_{LED_AVERAGE} = 3/19 \times$ ILED_MAX. For typical LED timing, the average VLEDx supply current is $3/19 \times 250$ mA = 39.4 mA, indicating that the V_{LEDx} supply must support a dc current of 40 mA.

DETERMINING C_{VLED}

To determine the C_{VLED} capacitor value, determine the maximum forward-biased voltage, V_{FB} LED MAX, of the LED in operation. The LED current, ILED_MAX, converts to VFB_LED_MAX as shown in [Figure 42.](#page-32-3) In this example, 250 mA of current through two green LEDs in parallel yields V_{FB} LED MAX = 3.95 V. Any series resistance in the LED path must also be included in this voltage. When designing the LED path, keep in mind that small resistances can add up to large voltage drops due to the LED peak current being large. In addition, these resistances can be unnecessary constraints on the VLEDx supply.

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Figure 42. Example of the Average LED Forward-Bias Voltage Drop as a Function of the LED Driver Current Setting

To correctly size the CVLED capacitor, do not deplete it during the pulse of the LED to the point where the voltage on the capacitor is less than the forward bias on the LED. Calculate the minimum value for the VLEDx bypass capacitor by

$$
C_{VLED} = \frac{t_{LED_PULSE} \times I_{LED_MAX}}{V_{LED_MIN} - (V_{FB_LED_MAX} + 0.6)}
$$
(2)

where:

tLED_PULSE is the LED pulse width.

ILED_MAX is the maximum forward-biased current on the LED used in operating the devices.

V_{LED} M_{IN} is the lowest voltage from the V_{LEDx} supply with no load. *VFB_LED_MAX* is the maximum forward-biased voltage required on the LED to achieve ILED MAX.

The numerator of the CVLED equation sets up the total discharge amount in coulombs from the bypass capacitor to satisfy a single programmed LED pulse of the maximum current. The denominator represents the difference between the lowest voltage from the VLEDx supply and the LED required voltage. The LED required voltage is the voltage of the anode of the LED such that the compliance of the LED driver and the forward-biased voltage of the LED operating at the maximum current is satisfied. At a 250 mA drive current, the compliance voltage of the driver is 0.6 V. For a typical ADPD1080 example, assume that the lowest value for the VLEDx supply is 4.75 V and that the peak current is 250 mA for two 528 nm LEDs in parallel. The minimum value for C_{VLED} is then equal to 3.75 μ F.

$$
C_{\text{VLED}} = (3 \times 10^{-6} \times 0.250) / (4.75 - (3.95 + 0.6)) = 3.75 \,\mu\text{F} \ (3)
$$

As shown in Equation 3, as the minimum supply voltage drops close to the maximum anode voltage, the demands on C_{VLED} become more stringent, forcing the capacitor value higher. It is important to insert the correct values into Equation 1, Equation 2, and Equation 3. For example, using an average value for VLED_MIN instead of the worst case value for VLED_MIN can cause a serious design deficiency, resulting in a CVLED value that is too small and that causes insufficient optical power in the application.

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Therefore, adding a sufficient margin on C_{VLED} is strongly recommended. Add additional margin to CVLED to account for derating of the capacitor value over voltage, bias, temperature, and other factors over the life of the component.

LED INDUCTANCE CONSIDERATIONS

The LED drivers (LEDXx) on the ADPD1080/ADPD1081 have configurable slew rate settings (Register 0x22, Bits[6:4], Register 0x23, Bits[6:4], and Register 0x24, Bits[6:4]). These slew rates are defined i[n Table 3.](#page-6-3) Even at the lowest setting, carefully consider board design and layout. If a large series inductor, such as a long PCB trace, is placed between the LED cathode and one of the LEDXx pins, voltage spikes from the switched inductor can cause violations of absolute maximum and minimum voltages on the LEDXx pins during the slew portion of the LED pulse.

To verify that there are no voltage spikes on the LEDXx pins due to parasitic inductance, use an oscilloscope on the LEDXx pins to monitor the voltage during normal operation. Any positive spike >3.6 V may damage the devices.

In addition, a negative spike less than −0.3 V may also damage the devices.

RECOMMENDED START-UP SEQUENCE

At power-up, the device is in standby mode (Register $0x10 =$ 0x0000), as shown in [Figure 27.](#page-23-2) The ADPD1080/ADPD1081 do not require a particular power-up sequence.

From standby mode, to begin measurement, initiate the ADPD1080/ADPD1081 as follows:

- 1. Set the CLK32K_EN bit (Register 0x4B, Bit 7) to start the sample clock (32 kHz clock). This clock controls the state machine. If this clock is off, the state machine is not able to transition as defined by Register 0x10.
- 2. Write 0x1 to Register 0x10 to force the device into program mode. Step 1 and Step 2 can be swapped, but the actual state transition does not occur until both steps occur.
- 3. Write additional control registers in any order while the device is in program mode to configure the devices as required.
- 4. Write 0x2 to Register 0x10 to start normal sampling operation.

To terminate normal operation, follow this sequence to place the ADPD1080/ADPD1081 in standby mode:

- 1. Write 0x1 to Register 0x10 to force the devices into program mode.
- 2. Write to the registers in any order while the devices are in program mode.
- 3. Write 0x00FF to Register 0x00 to clear all interrupts. If desired, clear the FIFO as well by writing 0x80FF to Register 0x00.

4. Write 0x0 to Register 0x10 to force the devices into standby mode.

Optionally, stop the 32 kHz clock by resetting the CLK32K_ EN bit (Register 0x4B, Bit 7). Register 0x4B, Bit 7 = 0 is the only write that must be written when the device is in standby mode (Register $0x10 = 0x0$). If 0 is written to this bit while in program mode or normal mode, the devices become unable to transition into any other mode, including standby mode, even if they are subsequently written to do so. As a result, the power consumption in what appears to be standby mode is greatly elevated. For this reason, and due to the low current draw of the 32 kHz clock while in operation, it is recommended from an ease of use perspective to keep the 32 kHz clock running after it is turned on.

READING DATA

The ADPD1080/ADPD1081 provide multiple methods for accessing the sample data. Each time slot can be independently configured to provide data access using the FIFO or the data registers. Interrupt signaling is also available to simplify timely data access. The FIFO is available to loosen the system timing requirements for data accesses.

Reading Data Using the FIFO

The ADPD1080/ADPD1081 include a 128-byte FIFO memory buffer that can store data from either or both time slots. Register 0x11 selects the kind of data from each time slot to be written to the FIFO. Note that both time slots can use the FIFO, but only if their output data rate is the same.

Output Data Rate = *fSAMPLE*/*NX*

where:

fSAMPLE is the sampling frequency.

NX is the averaging factor for each time slot (*NA* for Time Slot A and N_B for Time Slot B). In other words, $N_A = N_B$ must be true to store data from both time slots in the FIFO.

Data packets are written to the FIFO at the output data rate. A data packet for the FIFO consists of a complete sample for each enabled time slot. Data for each photodiode channel can be stored as either 16 or 32 bits. Each time slot can store 2, 4, 8, or 16 bytes of data per sample, depending on the mode and data format. To ensure that data packets are intact, new data is only written to the FIFO if there is sufficient space for a complete packet. Any new data that arrives when there is not enough space is lost. The FIFO continues to store data when sufficient space exists. Always read FIFO data in complete packets to ensure that data packets remain intact.

The number of bytes currently stored in the FIFO is available in Register 0x00, Bits[15:8]. A dedicated FIFO interrupt is also available and automatically generates when a specified amount of data is written to the FIFO.

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Interrupt-Based Method

To read data from the FIFO using an interrupt-based method, use the following procedure:

- 1. In program mode, set the configuration of the time slots as desired for operation.
- 2. Write to Register 0x11 with the desired data format for each time slot.
- 3. Set FIFO_THRESH in Register 0x06, Bits[13:8] to the interrupt threshold. A recommended value for this is the number of 16-bit words in a data packet minus 1, which causes an interrupt to generate when there is at least one complete packet in the FIFO.
- 4. Enable the FIFO interrupt by writing 0 to the FIFO_ INT_MASK in Register 0x01, Bit 8. Also, configure the interrupt pin (GPIO0 or GPIO1) by writing the appropriate value to the bits in Register 0x02.
- 5. Enter normal operation mode by setting Register 0x10 to 0x2.
- 6. When an interrupt occurs,
	- a. There is no requirement to read the FIFO_SAMPLES bits because the interrupt is generated only if there is one or more full packets. Optionally, the interrupt routine can check for the presence of more than one available packet by reading these bits.
	- b. Read a complete packet using one or more multiword accesses using Register 0x60. Reading the FIFO automatically frees the space for new samples.

The FIFO interrupt automatically clears immediately upon reading any data from the FIFO and is set again only when the FIFO is written and the number of words is more than the threshold.

Polling Method

To read data from the FIFO in a polling method, use the following procedure:

- 1. In program mode, set the configuration of the time slots as desired for operation.
- 2. Write to Register 0x11 with the desired data format for each time slot.
- 3. Enter normal operation mode by setting Register 0x10 to 2.

Next, begin the polling operations.

- 1. Wait for the polling interval to expire.
- 2. Read the FIFO_SAMPLES bits (Register 0x00, Bits[15:8]).
- 3. If FIFO_SAMPLES \geq the packet size, read a packet using the following steps:
	- a. Read a complete packet using one or more multiword accesses via Register 0x60. Reading the FIFO automatically frees the space for new samples. b. Repeat Step 1.

When a mode change is required, or any other disruption to normal sampling is necessary, clear the FIFO. Use the following procedure to clear the state and empty the FIFO:

2. Write 1 to Register 0x00, Bit 15.

Reading Data from Registers Using Interrupts

The latest sample data is always available in the data registers and is updated simultaneously at the end of each time slot. The data value for each photodiode channel is available as a 16-bit value in Register 0x64 through Register 0x67 for Time Slot A, and Register 0x68 through Register 0x6B for Time Slot B. If allowed to reach their maximum value, Register 0x64 through Register 0x6B clip. If Register 0x64 through Register 0x6B saturate, the unsaturated (up to 27 bits) values for each channel are available in Register 0x70 through Register 0x77 for Time Slot A and Register 0x78 through Register 0x7F for Time Slot B. Sample interrupts are available to indicate when the registers are updated and can be read. To use the interrupt for a given time slot, use the following procedure:

- 1. Enable the sample interrupt by writing a 0 to the appropriate bit in Register 0x01. To enable the interrupt for Time Slot A, write 0 to Bit 5. To enable the interrupt for Time Slot B, write 0 to Bit 6. Either or both interrupts can be set.
- 2. Configure the interrupt pin (GPIOx) by writing the appropriate value to the bits in Register 0x02.
- 3. An interrupt generates when the data registers are updated.
- The interrupt handler must perform the following: a. Read Register 0x00 and observe Bit 5 or Bit 6 to confirm which interrupt occurred. This step is not required if only one interrupt is in use.
	- b. Read the data registers before the next sample can be written. The system must have interrupt latency and service time short enough to respond before the next data update, based on the output data rate.
	- c. Write a 1 to Bit 5 or Bit 6 in Register 0x00 to clear the interrupt.

If both time slots are in use, it is possible to use only the Time Slot B interrupt to signal when all registers can be read. It is recommended to use the multiword read to transfer the data from the data registers.

Reading Data from Registers Without Interrupts

If the system interrupt response is not fast or predictable enough to use the interrupt method, or if the interrupt pin (GPIOx) is not used, it is possible to obtain reliable data access by using the data hold mechanism. To guarantee that the data read from the registers is from the same sample time, it is necessary to prevent the update of samples while reading the current values. The method for performing register reads without interrupt timing is as follows:

- 1. Write 1 to the SLOTA_DATA_HOLD or SLOTB_DATA_ HOLD bits (Register 0x5F, Bit 1 and Bit 2, respectively) for the time slot requiring access (both time slots can be accessed). This setting prevents sample updates.
- 2. Read the registers as desired.
- 1. Enter program mode by setting Register 0x10 to 0x1.

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3. Write 0 to the SLOTA_DATA_HOLD or SLOTB_DATA_ HOLD bits (Register 0x5F, Bit 1 and Bit 2, respectively) previously set. Sample updates are allowed again.

Because a new sample may arrive while the reads are occurring, this method prevents the new sample from partially overwriting the data being read.

CLOCKS AND TIMING CALIBRATION

The ADPD1080/ADPD1081 operate using two internal time bases: a 32 kHz clock sets the sample timing, and a 32 MHz clock controls the timing of the internal functions, such as LED pulsing and data capture. Both clocks are internally generated and exhibit device to device variation of approximately 10% (typical).

Heart rate monitoring applications require an accurate time base to achieve an accurate count of beats per minute. The ADPD1080/ADPD1081 provide a simple calibration procedure for both clocks.

Calibrating the 32 kHz Clock

Calibrating the 32 kHz clock also calibrates items associated with the output data rate. Calibration of this clock is important for applications where an accurate data rate is important, such as heart rate measurements.

To calibrate the 32 kHz clock,

- 1. Set the sampling frequency to the highest the system can handle, such as 2000 Hz. Because the 32 kHz clock controls sample timing, its frequency is readily accessible via the GPIO0 pin. Configure the interrupt by writing the appropriate value to the bits in Register 0x02 and set the interrupt to occur at the sampling frequency by writing 0 to Register 0x01, Bit 5 or Bit 6. Monitor the GPIO0 pin. The interrupt frequency must match the set sample frequency.
- 2. If the monitored interrupt frequency is less than the set sampling frequency, decrease the CLK32K_ADJUST bit (Register 0x4B, Bits[5:0]). If the monitored interrupt frequency is larger than the set sampling frequency, increase the CLK32K_ADJUST bits.
- 3. Repeat Step 1 and Step 2 until the monitored interrupt signal frequency is close enough to the set sampling frequency.

After the 32 kHz oscillator calibration completes, set the GPIO0 pin to the mode desired for normal operation.

Calibrating the 32 MHz Clock

Calibrating the 32 MHz clock also calibrates items associated with the fine timing within a sample period, such as LED pulse width and spacing, assuming that the 32 kHz clock is calibrated.

To calibrate the 32 MHz clock, the 32 kHz clock must first be calibrated as previously described. Always start this routine with Register 0x4D set to 0x98, which is the default value at power-up.

- 1. Write 0x1 to Register 0x5F, Bit 0 (DIGITAL_CLOCK_ENA) to enable the 32 MHz oscillator.
- 2. Enable the CLK_RATIO calculation by writing 0x1 to Register 0x50, Bit 5 (CLK32M_CAL_EN). This function counts the number of 32 MHz clock cycles in two cycles of the 32 kHz clock. With this function enabled, this cycle value is stored in Register 0x0A, Bits[11:0] and nominally this ratio is 2000 (0x7D0).
- 3. Calculate the 32 MHz clock error as follows: *Clock Error* = 32 MHz × (1 − *CLK_RATIO*/2000)
- 4. Adjust the frequency of the 32 MHz oscillator by adjusting the setting of Bits[7:0] in Register 0x4D by the amount calculated in the following equation:

CLK32M_ADJUST = *Clock Error*/112 kHz

5. Write 0x0 to Register 0x50, Bit 5 (CLK32M_CAL_EN) to reset the CLK_RATIO function.

Repeat Step 2 through Step 5 until the desired accuracy is achieved.

Write 0x0 to Register 0x5F, Bit 0 to disable the 32 MHz oscillator.

OPTIONAL TIMING SIGNALS AVAILABLE ON GPIO0 AND GPIO1

The ADPD1080/ADPD1081 provide a number of different timing signals, available via the GPIO0 and GPIO1 pins, to enable ease of system synchronization and flexible triggering options. Each GPIOx pin can be configured as an open-drain output if the pins are to share the bus with other drivers, or the pins can be configured to always drive the bus. Both outputs also have polarity control in situations where a timing signal must be inverted from the default.

Table 23. GPIOx Control Settings

The various available timing signals are controlled by the settings in Register 0x0B. Bits[12:8] of this register control the timing signals available on GPIO1, and Bits[4:0] control the timing signals available on GPIO0. All of the timing signals described in this data sheet are available on either (or both) of the GPIO0 and GPIO1 pins. Timing diagrams are shown in [Figure 43](#page-36-0) and [Figure 44.](#page-36-1) The time slot settings used to generate the timing diagrams are described in [Table 24.](#page-36-2)
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Table 24. ADPD1080/ADPD1081 Settings Used for Timing Diagrams Shown i[n Figure 43](#page-36-0) and [Figure 44](#page-36-1)

Figure 44. Optional Timing Signals Available on GPIOx—Register 0x0B, Bits[12:8] or Bits[4:0] = 0x02, 0x0C, 0x0D, and 0x0E

ADPD103 Backward Compatibility

Setting Register 0x0B = 0 provides backward compatibility to the [ADPD103.](http://www.analog.com/ADPD103?doc=ADPD1080-1081.pdf) The GPIO0 pin mirrors the functionality of the [ADPD103](http://www.analog.com/ADPD103?doc=ADPD1080-1081.pdf) INT pin. The GPIO1 pin mirrors the functionality of the [ADPD103](http://www.analog.com/ADPD103?doc=ADPD1080-1081.pdf) PDSO pin.

Interrupt Function

Setting Register 0x0B, Bits[12:8] or Bits[4:0] = 0x01 configures the respective pin to perform the interrupt function as defined by the settings in Register 0x01.

Sample Timing

Setting Register 0x0B, Bits[12:8] or Bits[4:0] = 0x02 configures the respective pin to provide a signal that asserts at the beginning of the first time slot of the current sample and deasserts at the end of the last time slot of the current sample. For example, if both time slots are enabled, this signal asserts at the beginning of Time Slot A and deasserts at the end of Time Slot B. If only a single time slot is enabled, the signal asserts at the beginning of the enabled time slot and deasserts at the end of this same time slot.

Pulse Outputs

Three options are available to provide a copy of the LED pulse outputs. Setting Register 0x0B, Bits[12:8] or Bits[4:0] = $0x05$ provides a copy of the Time Slot A LED pulses on the respective pin. A setting of 0x06 provides the Time Slot B pulses, and a setting of 0x07 provides the pulse outputs of both time slots.

Output Data Cycle Signal

Three options are available to provide a signal that indicates when the output data is written to the output data registers or to the FIFO. Setting Register 0x0B, Bits[12:8] or Bits[4:0] = 0x0C provides a signal that indicates that a data value is written for Time Slot A. A setting of 0x0D provides a signal that indicates that a data value is written for Time Slot B, and a setting of 0x0E provides a signal to indicate that a value is written for either time slot. The signal asserts at the end of the time slot, when the output data is already written, and deasserts at the start of the subsequent sample. This timing signal is especially useful in situations where the FIFO is used. For example, one of the GPIOx pins can provide an interrupt after the FIFO reaches the FIFO threshold set in Register 0x06, Bits[13:8], while the other GPIOx pin can provide the output data cycle signal. This signal can trigger a peripheral device, such as an accelerometer, so that time aligned signals are provided to the processor.

fS/2 Output

Setting Register 0x0B, Bits[12:8] or Bits[4:0] = $0x0F$ configures the respective pin to provide a signal that toggles at half the sampling rate. This timing signal is useful in, for example, situations where more than two LEDs per sample are required. This signal can be used as a select signal to a multiplexer being used to mux two LEDs into a single LED driver, providing the

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ability to drive up to four separate LEDs per sample period. In such a case, the ADPD1080/ADPD1081 operate at 2× the sampling rate, and the LED settings can be reconfigured during the sleep period between samples. If identical LED settings (current and timing) are used for the LEDs being muxed, up to four LEDs can be sampled per sampling period without host intervention. An example of this configuration is shown in [Figure 45.](#page-37-0)

The fs/2 timing signal always starts in an active low state when the device switches from standby mode to normal operating mode and transitions to a high state at the completion of the first sample.

Figure 45. Example Using the fs/2 Timing Signal

Logic 0 Output

Setting Register 0x0B, Bits[12:8] or Bits[4:0] = $0x10$ configures the respective pin to provide a Logic 0 output.

Logic 1 Output

Setting Register 0x0B, Bits[12:8] or Bits[4:0] = 0x11 configures the respective pin to provide a Logic 1 output.

32 kHz Oscillator Output

Setting Register 0x0B, Bits[12:8] or Bits[4:0] = 0x13 configures the respective pin to provide a copy of the on-board 32 kHz oscillator.

CALCULATING CURRENT CONSUMPTION

The current consumption of the ADPD1080/ADPD1081 depends on the user selected operating configuration, as determined by the following equations.

Total Power Consumption

To calculate the total power consumption, use Equation 4.

Average V_{DD} Supply Current

To calculate the average V_{DD} supply current, use Equation 5.

$$
I_{VDD_AVG} = DR \times ((I_{AFE_A} \times t_{SLOTA}) + (I_{AFE_B} \times t_{SLOTB}) +
$$

\n
$$
Q_{PROC_X} + I_{VDD_STANDBY}
$$
\n(5)

where:

DR is the data rate in Hz.

 $I_{VDD_STANDBY} = 0.2 \mu A$.

QPROC_X is an average charge associated with a processing time.

When only Time Slot A is enabled,

$$
Q_{PROC_A} (C) = 0.35 \times 10^{-6}
$$

When only Time Slot B is enabled,

 $Q_{PROC,B}$ (C) = 0.24 × 10⁻⁶

When Time Slot A and Time Slot B are enabled,

 Q_{PROC_AB} (C) = 0.40 \times 10⁻⁶

$$
I_{AFE_x}(A) = 3.0 \times 10^{-3} + (1.5 \times 10^{-3} \times NUM_CHANNELS) +(4.6 \times 10^{-3} \times I_{LEDX_PK}/SCALE_X)
$$
(6)

$$
t_{\text{SLOTx}}\left(\text{sec}\right) = LEDx_OFFSET + LEDx_PERIOD \times\nPULSE_COUNT
$$
\n(7)

where:

NUM_CHANNELS is the number of active channels. *ILEDX_PK* is the peak LED current, expressed in amps, for whichever LED is enabled in that particular time slot.

SCALE_X is the scale factor for the LED current drive determined by Bit 13 of the ILEDx_COARSE registers, Register 0x22,

Register 0x23, and Register 0x24.

LEDx_OFFSET is the pulse start time offset expressed in seconds.

LEDx_PERIOD is the pulse period expressed in seconds. *PULSE* COUNT is the number of pulses.

If either Time Slot A or Time Slot B are disabled, $I_{\text{AFE_x}} = 0$ for that respective time slot. Additionally, if operating in TIA ADC mode, set Register 0x3C, Bits[8:3] = 010010 to achieve power savings. This setting disables the BPFs that are bypassed in TIA ADC mode, changing the AFE power contribution calculation to

$$
I_{AFE_x}(mA) = 3.0 \times 10^{-3} + (1.0 \times 10^{-3} \times NUM_CHANNELS) + (4.6 \times 10^{-3} \times I_{LEDX_PK} / SCALE_X)
$$
 (8)

Average VLEDA Supply Current

To calculate the average VLEDA supply current, use Equation 9.

$$
I_{LED_AVG_A} = SLOTA_LED_WIDTH \times I_{LEDA_PK} \times DR \times
$$

$$
PULSE_COUNT
$$
 (9)

where:

SLOTA_LED_WIDTH is the LED pulse width expressed in seconds.

ILEDA_PK is the peak current, expressed in amps, for whichever LED is selected for Time Slot A.

Average VLEDB Supply Current

To calculate the average VLEDB supply current, use Equation 10.

$$
I_{LED_AVG_B} = SLOTB_LED_WIDTH \times I_{LEDB_PK} \times DR \times
$$

$$
PULSE_COUNT
$$
 (10)

where:

SLOTB_LED_WIDTH is the LED pulse width expressed in seconds.

ILEDB_PK is the peak current, expressed in amps, for whichever LED is selected for Time Slot B.

OPTIMIZING SNR PER WATT

The ADPD1080/ADPD1081 offer a variety of adjustable parameters to achieve the best signal. One of the key goals of system performance is to obtain the best system SNR for the lowest total power. This goal is often referred to as optimizing SNR per Watt. Even in systems where only the SNR matters and power is a secondary concern, there may be a lower power or a high power means of achieving the same SNR.

Optimizing for Peak SNR

The first step in optimizing for peak SNR is to find a TIA gain and LED level that gives the best performance where the number of LED pulses remains constant. If peak SNR is the goal, use the noise section o[f Table 4](#page-7-0) as a guide. It is important to note that the SNR improves as a square root of the number of pulses averaged together, whereas the increase in the LED power consumed is directly proportional to the number of LED pulses. In other words, for every doubling of the LED pulse count, there is a doubling of the LED power consumed and a 3 dB SNR improvement. As a result, avoid any change in the gain configuration that provides less than 3 dB of improvement for a 2× power penalty; any TIA gain configuration that provides more than 3 dB of improvement for a $2\times$ power penalty is a suitable choice. If peak SNR is the goal and there is no issue saturating the photodiode with LED current at any gain, the 50 kΩ TIA gain setting is an optimal choice. After the SNR per pulse per channel is optimized, the user can then increase the number of pulses to achieve the desired system SNR.

Optimizing SNR per Watt in a Signal Limited System

In practice, optimizing for peak SNR is not always practical. One scenario in which the PPG signal has a poor SNR is the signal limited regime. In this scenario, the LED current reaches an upper limit before the desired dc return level is achieved.

Tuning in this case starts where the peak SNR tuning stops. The starting point is nominally a 50 k Ω gain, as long as the lowest LED current setting of 8 mA does not saturate the photodiode and the 50 kΩ gain provides enough protection against intense background light. In these cases, use a 25 k Ω gain as the starting point.

The goal of the tuning process is to bring the dc return signal to a specific ADC range, such as 50% or 60%. The ADC range choice is a function of the margin of headroom needed to prevent saturation as the dc level fluctuates over time. The SNR of the PPG waveform is always some percentage of the dc level. If the target level cannot be achieved at the base gain, increase the gain and repeat the procedure. The tuning system may need to place an upper limit on the gain to prevent saturation from ambient signals.

Tuning the Pulse Count

After the LED peak current and TIA gain are optimized, increasing the number of pulses per sample increases the SNR by the square root of the number of pulses. There are two ways to increase the pulse count. The pulse count registers (Register 0x31, Bits[15:8], and Register 0x36, Bits[15:8]) change the number of pulses per internal sample. Register 0x15, Bits[6:4] and Bits[10:8], controls the number of internal samples that are averaged together before the data is sent to the output. Therefore, the number of pulses per sample is the pulse count register multiplied by the number of subsequent samples being averaged. In general, the internal sampling rate increases as the number of internal sample averages increase to maintain the desired output data rate. The SNR/Watt is most optimal with pulse count values of 16 or less. Above pulse count values of 16, the square root relationship does not hold in the pulse count register. However, this relationship continues to hold when averaged between samples using Register 0x15.

Note that increasing LED peak current increases SNR almost directly proportional to LED power, whereas increasing the number of pulses by a factor of n results in only a nominal $\sqrt{(n)}$ increase in SNR.

When using the sample sum or average function (Register 0x15), the output data rate decreases by the number of summed samples. To maintain a static output data rate, increase the sample frequency (Register 0x12) by the same factor as that selected in Register 0x15. For example, for a 100 Hz output data rate and a sample sum or average of four samples, set the sample frequency to 400 Hz.

Applying a Reverse Bias to the Photodiode

The photodiode capacitance contributes to higher noise in the signal path. Applying a reverse bias to the photodiode reduces the capacitance of the photodiode, resulting in better noise performance. To apply a reverse bias to the photodiode, set Register 0x54, Bit 7 to 1. The actual reverse bias is then determined by the settings in Register 0x54, Bits[11:10] for Time Slot B and in Register 0x54, Bits[9:8] for Time Slot A. Set these bits equal to $0x2$ applies \sim 250 mV of reverse bias across the photodiode. There is also an option of setting the cathode of the PD equal to the positive supply voltage, which can result in up to 0.9 V of reverse bias; however, any noise on the supply is introduced directly into the signal so this may actually result in higher noise levels. The recommended setting is to set Register 0x54, Bits[11:10] and/or Register 0x54, Bits[9:8] equal to 0x2 for an \sim 250 mV reverse bias.

Improving SNR Using Integrator Chopping

The last stage in the analog front end that is integrated into the ADPD1080/ADPD1081 data path is a charge integrator. The integrator uses an on and off integration sequence, synchronized to the emitted light pulse, which acts as an additional high-pass filter to remove offsets, drifts, and low frequency noise from the previous stages. However, the integrating amplifier can itself introduce low frequency signal content at a low level. The ADPD1080/ADPD1081 have an integrator chop mode that enables additional chopping in the digital domain to remove this signal. This chopping is achieved by using even numbers of pulses per sample and inverting the integration sequence for half of those sequences. In the calculation to combine the digitized result of each of the pulses of the sample, the sequences with an inverted integrator sequence are subtracted and the sequences with a normal integrator sequence are added. An example diagram of the integrator chopping sequence is shown in [Figure 46.](#page-39-0)

The result is that any low frequency signal contribution from the integrator is eliminated, leaving only the integrated signal, which results in higher SNR, especially at higher numbers of pulses and at lower TIA gains where the noise contribution of the integrator becomes more pronounced.

Digital chopping is enabled using the registers and bits detailed in [Table 25.](#page-39-1) The bit fields define the chopping operation for the first four pulses. This 4-bit sequence is then repeated for all subsequent pulses. I[n Figure 46,](#page-39-0) a sequence is shown where the second and fourth pulses are inverted, whereas the first and third pulses remain in the default polarity (noninverted). This configuration is achieved by setting Register $0x17$, Bits[3:0] = $0xA$ and Register 0x1D, Bits $[3:0] = 0$ xA for Time Slot A and Time Slot B, respectively. To complete the operation, the math must be adjusted using Register 0x58. In this example, set Register 0x58, Bits[9:8] and Register 0x58, Bits[11:10] to b01 to add the third pulse and subtract the fourth pulse for Time Slot A and Time Slot B, respectively. Set Register 0x58, Bits[2:1] and Register 0x58, Bits[6:5] to b01 to add the first pulse and subtract the second pulse for Time Slot A and Time Slot B, respectively. This sequence then repeats for every subsequent sequence of four pulses. An even number of pulses must be used with integrator chop mode.

When using integrator chop mode, the ADC offset registers (Register 0x18 through Register 0x1B for Time Slot A, and Register 0x1E through Register 0x21 for Time Slot B) must be set to 0. These settings are required because any digital offsets at the output of the ADC are automatically eliminated when the math is adjusted to subtract the inverted integration sequences while the default integration sequences are added. Integrator chop mode also eliminates the need to manually null the ADC offsets at startup in a typical application. Note that the elimination of the offset using chop mode may clip at least half of the noise signal when no input signal is present, which makes measuring the noise floor during characterization of the system difficult. For this reason, perform noise floor characterization of the system either with chop mode disabled or with chop mode enabled but with a minimal signal present at the input that increases the noise floor enough such that it is no longer clipped.

Figure 46. Diagram of Integrator Chopping Sequence

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OPTIMIZING POWER BY DISABLING UNUSED CHANNELS AND AMPLIFIERS

Single-Channel AFE Mode

When using a single photodiode in an application, with that photodiode connected to a single AFE channel (either Channel 1 or Channel 2), the ADPD1080/ADPD1081 have an option to power down the unused channels, placing the device in single AFE channel mode. Because three of the four AFE channels are off in this mode, the power consumption is reduced considerably.

When only Channel 1 is used, disable Channel 2, Channel 3, and Channel 4 by writing 0x7 to Register 0x3C, Bits[8:6]. If only Channel 2 is used, disable Channel 1 by writing 0x7 to Register 0x3C, Bits[5:3], and disable Channel 3 and Channel 4 by writing 0x7 to Register 0x37, Bits[15:13].

Dual-Channel AFE Mode

In situations where two of the four channels are in use, the other two channels can be disabled. Enable Channel 1 and Channel 2 (with Channel 3 and Channel 4 disabled) by writing 0x7 to Register 0x37, Bits[15:13]. Operate Channel 3 and Channel 4 in dual channel mode (with Channel 1 and Channel 2 disabled) by writing 0x7 to both Register 0x3C, Bits[5:3] and Register 0x37, Bits[12:10].

Three-channel mode can also be achieved with the appropriate settings. See Table 26 for the settings required to power down different co[mbination](#page-41-0)s of channels. Refer to the Time Slot Switch section to determine the different combi[nations of the](#page-19-0) [PDx inp](#page-19-0)uts and enabled channels required to optimize the system configuration for maximum SNR and lowest power.

Powering Down Individual Amplifiers for Additional Power Savings

Each channel includes a TIA, a BPF, and an integrator which can also be configured as a buffer (see Figure 47).Options are built into the devices to power down in[dividual am](#page-40-0)plifiers in the signal path. For example, in TIA ADC mode, the BPF is bypassed but left powered up by default. The BPF can be disabled completely, which saves 1/3 of the power dissipated by the AFE during the sampling phase. See the descriptions for Register 0x3C and Register 0x37 in Table 38 for information on how to disable the individual ampli[fiers.](#page-59-0)

Figure 47. TIA/BPF/Integrator Block Diagram

It is important to leave any unused input channels floating for proper device operation.

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Table 26. Channel Power-Down Settings

OPTIMIZING DYNAMIC RANGE FOR HIGH AMBIENT LIGHT CONDITIONS

Large amounts of ambient light use large amounts of the available dynamic range of the TIA. The band-pass filter rejects the ambient light prior to the charge being integrated by the integrator; therefore, the ambient light is not a primary concern for the integrator. However, to accommodate increased levels of ambient light, it may be necessary to use lower TIA gain to avoid saturation of the TIA. When the TIA gain is reduced, the referred to input (RTI) noise of the desired signal increases. The impact of this increase can be reversed by increasing the gain of the integrator so that the LED signal gain in mA per LSB remains the same.

For example, start with an amount of pulsed signal (desired) where the TIA gain has been optimized such that the pulsed signal is using the desired amount of ADC dynamic range available, typically ~70% full scale. If the ambient light level increases and the gain of the TIA must be decreased to accommodate for the increase in ambient light without saturating the TIA, then the amount of pulsed signal presented to the ADC is attenuated by the factor that the TIA gain is reduced, which results in the SNR of the desired signal reducing.

To increase the SNR of the desired signal in this situation, use one of the following two methods. The first method simply increases the LED current by the amount required to bring the level of the pulsed signal at the ADC back to the desired amount of full scale. However, this is at the expense of increasing the overall power of the system. The second method is to increase

the gain of the integrator to achieve a similar result. [Figure 48](#page-41-1) shows a block diagram of the receive path. The gain of the signal path is determined by the TIA feedback resistor (R_F) and the input resistor to the integrator (R_{INT}). When R_F is reduced to provide additional dynamic range at the input to the TIA to accommodate additional ambient light, R_{INT} can be reduced to provide more gain through the integrator such that the same amount of pulsed signal at the input to the TIA utilizes the same amount of dynamic range of the ADC before the TIA gain is reduced. Use Bits[9:8] of Register 0x42 (Time Slot A) and Register 0x44 (Time Slot B) to choose the resistor setting of RINT as shown in [Table 27.](#page-41-2)

[Table 28](#page-41-3) shows an example of how the SNR can be optimized as a function of the R_F and R_{INT} vs. the amount of ambient light that must be accommodated. The values shown i[n Table 28](#page-41-3) are for a 2 µs LED pulse and a photodiode capacitance of 30 pF.

TIA ADC MODE

[Figure 49](#page-42-0) shows a way to put the devices into a mode that effectively runs the TIA directly into the ADC without using the analog BPF and integrator. This mode is referred to as TIA ADC mode. There are two basic applications of TIA ADC mode. In normal operation, all background light is blocked from the signal chain and, therefore, cannot be measured. TIA ADC mode can measure the amount of background and ambient light. This mode can also measure other dc input currents, such as leakage resistance.

When the devices are in TIA ADC mode, the BPF and the integrator stage are bypassed. This bypass effectively wires the TIA directly into the ADC. At the set sampling frequency, the ADC samples Channel 1 through Channel 4 in sequential

order, and each sample is taken at 1 µs intervals.

There are two modes of operation in TIA ADC mode. One mode is an inverting configuration where TIA ADC mode directly drives the ADC. This mode is enabled by setting Register 0x43 (Time Slot A) and/or Register 0x45 (Time Slot B) to 0xB065, which bypasses the BPF and the integrator. With the ADC offset register(s) for the desired channel set to 0, and the bias voltage for the TIA (TIA_VREF) set to 1.265 V, the output of the ADC is at ~13,000 codes for a single pulse and a zero input current condition. As the input current from the photodiode increases, the ADC output decreases toward 0. This configuration is a legacy TIA ADC mode from the [ADPD103](http://www.analog.com/ADPD103?doc=ADPD1080-1081.pdf) that is kept in the ADPD1080/ADPD1081 for backward compatibility.

The recommended TIA ADC mode is one in which the BPF is bypassed and the integrator is configured as an inverting buffer. This mode is enabled by writing 0xAE65 to Register 0x43 (Time Slot A) and/or Register 0x45 (Time Slot B) to bypass the BPF. Additionally, to configure the integrator as a buffer, set Bit 7 of Register 0x42 (Time Slot A) and/or Register 0x44 (Time Slot B) to 1, and set Bit 7 of Register 0x58 to 1. With the ADC offset register(s) for the desired channel set to 0 and the TIA_VREF set to 1.265 V, the output of the ADC is at ~13,000 codes for a single pulse and a zero input current condition. As the input current from the photodiode increases, the ADC output decreases toward 0.

When configuring the integrator as a buffer, there is the option of either using a gain of 1 or a gain of 0.7. Using the gain of 0.7 increases the usable dynamic range at the input to the TIA; however, it is possible to overrange the ADC in this configuration and care must be taken to not saturate the ADC. To set the buffer gain use Register 0x42, Bit 9 for Time Slot A and Register 0x44, Bit 9 for Time Slot B. Setting this bit to 0 (default) sets a gain of 1. Setting this bit to 1 configures the buffer with a gain of 0.7.

Calculate the ADC output (ADC_{OUT}) as follows:

$$
ADC_{OUT} = 8192 \pm \left(\left(\left(2 \times TIA_VREF - 2 \times i \times R_F - 1.8 \text{ V} \right) \right) \right. \\ \left. 146 \, \mu\text{V}/LSB \right) \times SLOTx_BUF_GAIN \right) \tag{11}
$$

where:

TIA_VREF is the bias voltage for the TIA (the default value is 1.265 V).

i is the input current to the TIA.

RF is the TIA feedback resistor.

SLOTx_BUF_GAIN is either 0.7 or 1 based on the setting of Register 0x42, Bit 9 and Register 0x44, Bit 9.

Equation 11 is an approximation and does not account for internal offsets and gain errors. The calculation also assumes that the ADC offset registers are set to 0

One time slot can be used in TIA ADC mode at the same time the other time slot is being used in normal pulsed mode. This capability is useful for monitoring ambient and pulsed signals at the same time. The ambient signal is monitored during the time slot configured for TIA ADC mode, while the pulsed signal, with the ambient signal rejected, is monitored in the time slot configured for normal mode.

Protecting Against TIA Saturation in Normal Operation

One of the reasons to monitor TIA ADC mode is to protect against environments that may cause saturation. One concern when operating in high light conditions, especially with larger photodiodes, is that the TIA stage may become saturated while the ADPD1080/ADPD1081 continue to communicate data. The resulting saturation is not typical. The TIA, based on its settings, can only handle a certain level of photodiode current. Based on the way the ADPD1080/ADPD1081 are configured, if there is a current level from the photodiode that is larger than the TIA can handle, the TIA output during the LED pulse effectively extends the current pulse, making it wider. The AFE timing is then violated because the positive portion of the BPF output extends into the negative section of the integration window. Thus, the photo signal is subtracted from itself, causing the output signal to decrease when the effective light signal increases.

To measure the response from the TIA and verify that this stage is not saturating, place the device in TIA ADC mode and slightly modify the timing. Specifically, sweep SLOTx_AFE_OFFSET until two or three of the four channels reach a minimum value (note that TIA is in an inverting configuration). The four channels do not reach this minimum value because, typically, 3 µs LED pulse widths are used, and the ADC samples the four channels sequentially at 1 µs intervals. This procedure aligns the ADC sampling time with the LED pulse to measure the total amount of light falling on the photodetector (for example, background light + LED pulse).

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If this minimum value is above 0 LSB, the TIA is not saturated. However, take care, because even if the result is not 0 LSB, operating the device near saturation can quickly result in saturation if light conditions change. A safe operating region is typically at ¾ full scale and lower. Use [Table 29](#page-43-0) to determine how the input codes map to ADC levels on a per channel per pulse basis. These codes are not the same as in normal mode because the BPF and integrator are not unity-gain elements.

Measuring PCB Parasitic Input Resistance

During the process of mounting the ADPD1080/ADPD1081, undesired resistance can develop on the inputs through assembly errors or debris on the PCB. These resistances can form between the anode and cathode, or between the anode and some other supply or ground. In normal operation, the ambient rejection feature of the ADPD1080/ADPD1081 masks the primary effects of these resistances, making it difficult to detect them. However, even at 1 M Ω to 10 M Ω , such resistance can affect performance significantly through added noise or decreased dynamic range. TIA ADC mode can screen for these assembly issues.

Measuring Shunt Resistance on the Photodiode

A shunt resistor across the photodiode does not generally affect the output level of the device in operation because the effective impedance of the TIA is low, especially if the photodiode is held to 0 V in operation. However, such resistance can add noise to the system, degrading performance. The best way to detect photodiode leakage, also called photodiode shunt resistance, is to place the device in TIA ADC mode in the dark and vary the operation mode cathode voltage. Setting the cathode to 1.3 V places 0 V across the photodiode because the anode is always at 1.3 V

while in operation. Setting the cathode to 1.8 V places 0.5 V across the photodiode. Using the register settings i[n Table 3](#page-6-0) to control the cathode voltage, measure the TIA ADC value at both voltages. Next, divide the voltage difference of 0.5 V by the difference of the ADC result after converting it to a current. This result is the approximate shunt resistance. Values greater than 10 MΩ may be difficult to measure, but this method is useful in identifying gross failures.

Measuring TIA Input Shunt Resistance

A resistance to develop between the TIA input and another supply or ground on the PCB is an example of another problem that can occur. These resistances can force the TIA into saturation prematurely. This premature saturation, in turn, takes away dynamic range from the device in operation and adds a Johnson noise component to the input. To measure these resistances, place the device in TIA ADC mode in the dark and start by measuring the TIA ADC offset level with the photodiode inputs disconnected (Register 0x14, Bits[11:8] = 0 or Register 0x14, Bits[7:4] = 0). From this, subtract the value of TIA ADC mode with the darkened photodiode connected and convert the difference into a current. If the value is positive, and the ADC signal decreased, the resistance is to a voltage higher than 1.3 V, such as V_{DD} . Current entering the TIA causes the output to drop. If the output difference is negative due to an increase of codes at the ADC, current is being pulled out of the TIA, and there is a shunt resistance to a lower potential than 1.3 V, such as ground.

Hex Addr. Data Bit(s) Bit Name Normal Mode Value TIA ADC Mode Value Description 42 [15:10] SLOTA_AFE_MODE 0x07 Not applicable In normal mode, this setting configures the integrator block for optimal operation. This setting is not important for TIA ADC mode. [9:8] SLOTA_INT_GAIN \vert 0x0 \vert 0x0 \vert 00: buffer gain = 1.0. 01: buffer gain $= 1.0$. 10: buffer gain $= 0.7$. 7 SLOTA_INT_AS_BUF 0x0 0x1 0: normal integrator configuration. 1: convert integrator to buffer amplifier 43 [15:0] SLOTA_AFE_CFG 0xADA5 0xAE65 Time Slot A AFE connection. 0xAE65 bypasses the band-pass filter. 0xB065 can also be used in TIA ADC mode. This setting bypasses the BPF and the integrator. 44 [15:10] SLOTB_AFE_MODE 0x07 Not applicable In normal mode, this setting configures the integrator block for optimal operation. This setting is not important for TIA ADC mode. [9:8] SLOTB_INT_GAIN \vert 0x0 \vert 0x0 \vert 00: buffer gain = 1.0. 01: buffer gain $= 1.0$. 10: buffer gain $= 0.7$. 7 SLOTB_INT_AS_BUF 0x0 0x1 0: normal integrator configuration. 1: convert integrator to buffer amplifier 45 $\left[$ [15:0] SLOTB_AFE_CFG $\left[$ 0xADA5 $\left[$ 0xAE65 $\left[$ Time Slot B AFE connection. 0xAE65 bypasses the BPF. 0xB065 can also be used in TIA ADC mode. This setting bypasses the BPF and the integrator. 58 7 ENA_INT_AS_BUF 0x0 0x1 Enables the ability to configure the integrator as a buffer in TIA ADC mode.

Table 30. Configuration Registers to Switch Between the Normal Sample Mode and TIA ADC Mode

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PULSE CONNECT MODE

In pulse connect mode, the photodiode input connections are pulsed according to the timing set up in the LED pulse timing registers. In this mode, if the LED pulse timing is set up to provide a 2 µs LED pulse, the device pulses the connection to the photodiode input for 2 µs instead of providing a 2 µs LED pulse. This mode is an alternate to TIA ADC mode, allowing the entire signal path, including the BPF and integrator, to measure ambient light as well as other types of measurements with different types of sensors (for example, electrocardiogram (ECG)).

To enable pulse connect mode, the device is configured identically to normal mode, except that Register 0x14, Bits $[3:2] = 0$ for Time Slot B, and Register 0x14, Bits[1:0] = 0 for Time Slot A.

SYNCHRONOUS ECG AND PPG MEASUREMENT USING TIA ADC MODE

In wearable devices developed for monitoring the health care of patients, it is often necessary to have synchronized measurements of biomedical signals. For example, a synchronous measurement of patient ECG and PPG can determine the pulse wave transit time (PWTT), which can then estimate blood pressure.

The circuit shown in [Figure 51](#page-45-0) shows a synchronous ECG and PPG measurement using the [AD8233](http://www.analog.com/AD8233?doc=ADPD1080-1081.pdf) and the ADPD1080. The [AD8233](http://www.analog.com/AD8233?doc=ADPD1080-1081.pdf) implements a two-pole high-pass filter (HPF) with a cutoff frequency at 0.3 Hz, and a two-pole low-pass filter (LPF) with a cutoff frequency of 37 Hz. The output of the [AD8233](http://www.analog.com/AD8233?doc=ADPD1080-1081.pdf) is fed to one of the current inputs of the ADPD1080 through a 200 k Ω resistor to convert the voltage output of th[e AD8233](http://www.analog.com/AD8233?doc=ADPD1080-1081.pdf) into a current.

The ADPD1080 is configured to alternately measure the photodiode signal and the ECG signal from th[e AD8233](http://www.analog.com/AD8233?doc=ADPD1080-1081.pdf) on consecutive time slots to provide fully synchronized PPG and ECG measurements. Data can be read out of the on-chip FIFO or straight from data registers. The ADPD1080 channel used to process the ECG signal is set up in TIA ADC mode, and the input bias voltage must be set to the 0.90 V setting using Bits[5:4] of Register 0x42 if the ECG signal is on Time Slot A, or Register 0x44 on Time Slot B. The TIA gain setting can be set to optimize the dynamic range of the signal path. The channel used to process the PPG signal is configured in its normal operating mode. [Figure 50](#page-45-1) shows a plot of a synchronized ECG and PPG measurement using th[e AD8233](http://www.analog.com/AD8233?doc=ADPD1080-1081.pdf) with the ADPD1080.

Figure 51. Synchronized PPG and ECG Measurement Using the ADPD1080 with the [AD8233](http://www.analog.com/AD8233?doc=ADPD1080-1081.pdf)

FLOAT MODE

The ADPD1080/ADPD1081 has a unique operating mode, float mode, that allows excellent SNR at low power in low light situations. In float mode, the photodiode is first preconditioned to a known state and then the photodiode anode is disconnected from the receive path of the ADPD1080/ ADPD1081 for a preset amount of float time. During the float time, light falls on the photodiode, either from ambient light, pulsed LED light, or a combination of the two depending on the operating mode. Charge from the sensor is stored directly on the capacitance of the sensor. At the end of the float time, the photodiode switches back into the receive path of the ADPD1080/ADPD1081 and an inrush of the accumulated charge occurs, which is subsequently integrated by the integrator of the ADPD1080/ADPD1081, allowing the maximum amount of charge to be processed per pulse with the minimum amount of noise added by the signal path. The charge is integrated externally on the capacitance of the photodiode for as long as it takes to acquire maximum charge, independent of the amplifiers of the signal path, which adds noise to the signal.

Amplifier and ADC noise values are constant for a given measurement. For optimal SNR, it is desirable to have a greater amount of signal (charge) per measurement. In normal mode, because the pulse time is fixed, the charge per measurement can be increased only by increasing the LED drive current. For high light conditions, this is sufficient. In low light conditions, however, there is a limit to the available current. In addition, high current pulses can cause ground noise in some systems. Green LEDs have lower efficiency at high currents, and many battery designs do not deliver high current pulses as efficiently. Float mode allows the user the flexibility to increase the amount of charge per measurement by either increasing the LED drive current or by increasing the float time. This flexibility is especially useful in low current transfer ratio (CTR) conditions, for example, 10 nA/mA, where normal mode requires multiple pulses to achieve an acceptable level of SNR.

In float mode, the signal path bypasses the BPF and uses only the TIA and integrator. In normal mode, the shape of the pulse is known (typically either 2 µs or 3 µs) and is consistent across devices and conditions. The shape of the signal coming through the BPF is also predictable, which allows a user to align the integrator timing with the zero-crossing of the filtered signal. In float mode, the shape of the signal produced by the charge dump can differ across devices and conditions. A filtered signal cannot be reliably aligned; therefore, the BPF cannot be used. In float mode, the entire charge dump is integrated in the negative cycle of the integrator and the positive cycle cancels any offsets.

Float Mode Measurement Cycle

[Figure 52](#page-47-0) shows the float mode measurement cycle timing diagram, and the following details the points shown:

- The precondition period is shown prior to Point A. The photodiode is connected to the TIA, and the photocurrent flows into the TIA. The photodiode anode is held at 0.9 V (Register 0x42 and Register 0x44, Bits $[5:4] = 0x2$ sets TIA_VREF = 0.9 V). The photodiode is reverse biased to a maximum reverse bias of \sim 250 mV by setting Register 0x54, Bit $7 = 1$ and Register 0x54, Bits $[9:8] =$ 0x2 (for Time Slot A). At this point, the output of the TIA $(TIA_OUT) = TIA_VREF - (I_{PD} \times R_F)$, where I_{PD} is the current flowing from the PD into the ADPD1080/ ADPD1081 input, and the integrator is off.
- At Point A, the photodiode is disconnected from the receive path. Light continues to fall on the photodiode, producing a charge that accumulates directly on the photodiode capacitance. As the charge accumulates, the voltage at the floating photodiode anode rises. The TIA is disconnected from the input to the ADPD1080/ADPD1081 so that no current flows through the TIA, and the TIA output is at TIA_VREF. Just prior to Point B, the integrator resets to 0. In the Float Mode for Synchronous LED [Measurements](#page-49-0) section*,* the LED pulses during the time period between Point A and Point D. Float times of <4 µs are not allowed.
- At Point B, the integrator begins its positive integration phase. Small dc offsets between the TIA output and the integrator reference causes the integrator output to ramp up for positive offsets or ramp down for negative offsets. The photodiode continues to accumulate charge during this period.
- At Point C, the integrator begins its negative integration phase. This reversal in polarity begins to cancel any signal caused by offsets. This offset cancellation continues through Point F, where all offsets are cancelled completely.
- At Point D, the photodiode switches into the receive path where all the charge that has accumulated on the photodiode capacitance during the float time is dumped into the TIA. The typical charge dump time is less than 2 µs. As the current flows through the TIA, the output of the TIA responds with a large negative signal. Because the integrator is in the negative integration phase at this point, the output of the integrator rises as the input current to the device integrates back to total charge. Between Point D and Point E, any light incident on the photodiode produces additional photocurrent, which is immediately integrated by the integrator as charge.
- At Point E, the TIA disconnects from the receive path and the TIA output returns to TIA_VREF. Between Point E and Point F, the integrator completes the negative integration phase and cancellation of the offsets.
- At Point F, the integrator output is held until sampled by the ADC.

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Figure 52. Float Mode Measurement Cycle Timing Diagram

Float Mode Limitations

When using float mode, the limitations of the mode must be well understood. For example, a finite amount of charge can accumulate on the capacitance of the photodiode, and a maximum amount of charge that can be integrated by the integrator. Based on an initial reverse bias of 250 mV on the photodiode and assuming that the photodiode begins to become nonlinear at ~200 mV of forward bias, there is ~450 mV of headroom for the anode voltage to increase from its starting point at the beginning of the float time before the charge ceases to accumulate in a linear fashion. It is desirable to operate only in the linear region of the photodiode (se[e Figure 53\)](#page-47-1). To verify that float mode is operating in the linear region of the diode, the user can perform a simple check. Record data at a desired float time and then record data at half the float time. The ratio of the two received signals should be 2:1. If this ratio does not hold true, the diode is likely beginning to forward bias at the longer float time and becomes nonlinear.

Float Time

The maximum amount of charge that can be stored on the photodiode capacitance and remain in the linear operating region of the sensor can be estimated by

$$
Q = CV
$$

where:

Q is the integrated charge.

C is the capacitance of the photodiode.

V is the amount of voltage change across the photodiode before the photodiode becomes nonlinear.

For a typical discrete optical design using a 7 mm2 photodiode with 70 pF capacitance and 450 mV of headroom, the maximum amount of charge that can be stored on the photodiode capacitance is 31.5 pC.

In addition, consider the maximum amount of charge the integrator of the ADPD1080/ADPD1081 can integrate. The integrator can integrate up to 7.6 pC. When this charge is referred back to the input, consider the TIA gain. When the TIA gain is at 200 kΩ, the input referred charge is at a 1:1 ratio to the integrated charge on the integrator. For 100 k Ω gain, it is 2:1; for 50 k Ω gain, it is 4:1; and for 25 k Ω gain, it is 8:1. For the previous example using a photodiode with 70 pF capacitance, use 50 k Ω TIA gain and set the float timing such that, for a single pulse, the output of the ADC is at 70% of full scale, which is a typical operating condition. Under these operating conditions, 5.3 pC integrates per pulse by the integrator for 21.2 pC of charge accumulated on the photodiode capacitance. For small CTR, however, it can take a long time to accumulate 21.2 pC of charge on the photodiode capacitance, in which case, use higher TIA gains according to how much charge can be accumulated in a

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given amount of time. Ultimately, the type of measurement being made (ambient or pulsed LED), the photodiode capacitance, and the CTR of the system determine the float times.

Float Mode for Ambient Light Measurements

Float mode is used for ambient light measurements where the background light is sufficiently small. Use TIA ADC mode for ambient light measurements of higher intensities. Small amounts of light can be measured with adequate float times, allowing the incoming charge to accumulate to levels large enough to be measured above the noise floor of the system. The source of this light can be any combination of synchronous light (for example, from a pulsed LED) and asynchronous light (that is, background). If there is no system generated light source, the measurement is simply a measure of the background light.

Use a two pulse differential measurement technique to cancel out electrical drifts and offsets. Take two measurements, each of a different float time. The first float time is considerably

shorter than the second pulse. After the two measurements are taken, Measurement 1 is subtracted from Measurement 2, which effectively cancels out any offset and drift common to both measurements. What is left is an ambient light measurement based on an amount of charge that is integrated over a time that is the difference of the first and second float times. For example, if Float Time 1 is 6 µs and Float Time 2 is 26 µs, the ambient light measurement is based on 20 µs of charge integrated on the photodiode capacitance with any offset and drift removed. In float mode for ambient light, the number of pulses must be set to two to cancel drifts and offsets because only the first pulse can be short. More than two pulses can be used; however, pulses two through n are always the same length. If drift cancellation is not required, any number of pulses can be used and added together. [Figure 54](#page-48-0) shows an example of float ambient mode timing, and [Table 31](#page-48-1) details the relevant registers that must be configured.

Figure 54. Example of Float Ambient Mode Timing

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Float Mode for Synchronous LED Measurements

In float LED mode, photocurrent is generated from ambient light and pulsed LED light during the float time. Float LED mode is desirable in low signal conditions where the CTR is <10 nA/mA. In addition, float mode is a good option in situations where the user wants to limit the LED drive current of the green LEDs in a heart rate measurement to keep the forward voltage drop of the green LED to a level that allows the elimination of a boost converter for the LED supply. For example, the LED current can be limited to 10 mA to ensure that the LED voltage drop is \sim 3 V so that it can operate directly from the battery without the need of a boost converter. Float mode accumulates the received charge during longer LED pulses without adding noise from the signal path, effectively yielding the highest SNR and/or photon attainable.

As with float ambient mode, multiple pulses cancel electrical offsets and drifts; however, in float LED mode, the ambient light must also be cancelled because only the reflected return from the LED pulses is desired. To achieve this ambient light rejection, use an even number of equal length pulses. For every pair of pulses, the LED flashes in one of the pulses and does not flash in the other. The return from the LED + ambient + offset

is present in one of the pulses. In the other, only the ambient light and offset is present. A subtraction of the two pulses is made that eliminates ambient light as well as any offset and drift. It is recommended to use groups of four pulses for measurement where the LED is flashed on Pulse 2 and Pulse 3. The accumulator adds Pulse 2 and Pulse 3 and then subtract Pulse 1 and Pulse 4. To gain additional SNR, use multiple groups of four pulses.

The settings of FLT_LED_FIRE_x, Register 0x5A, Bits[15:8] determine if the LED fires in which pulse position. Which pulse positions are added or subtracted is configured in the FLT_MATH12x and FLT_MATH34x bits of Register 0x58. These sequences are repeated in groups of four pulses. The value written to the FIFO or data registers is dependent on the total number of pulses per sample period. For example, if the device is setup for 32 pulses, the 4 pulse sequence, as defined in FLT_LED_FIRE_x and FLT_MATHxxx, repeats eight times and a single register or FIFO write of the final value based on 32 pulses executes. [Table 32](#page-50-0) details the relevant registers for float LED mode.

Table 32. Float LED Mode Registers

A timing diagram for a four pulse float LED sequence for Time Slot B is shown i[n Figure 55.](#page-51-0) In this example, the device is set up for LED pulses of 12 µs that fall within a float period of 16 µs, 2 µs of which are used for dumping of the accumulated charge on the photodiode. The integration time is set to $3 \mu s$, which is 1 µs more than the charge dump time to allow timing margin when integrating the incoming charge. Note, there is a 9 µs offset built into the integration start time. Consider this offset when setting the SLOTx_AFE_OFFSET value. As shown i[n Figure 55,](#page-51-0) the time of the first charge dump is set to 30 µs.

SLOTx_AFE_OFFSET is set to 0x238 (17.75 µs), taking into account the 3 µs integration time, the 9 µs offset, and an additional 250 ns for edge placement margin.

To calculate SLOTx_AFE_OFFSET, use the following equation:

SLOTx_AFE_OFFSET = *SLOTx_LED_OFFSET* – *SLOTx_AFE_WIDTH* − 9.25 µs

Placement of the integration period is such that the negative phase of the integration is centered on the charge dump phase. The TIA is an inverting stage; therefore, placing the negative

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phase of the integration during the dumping of the charge from the photodiode causes the integrator to increase with the negative going output signal from the TIA.

The LED flashes in the second and third pulses of the four pulse sequence. Setting Register 0x58, Bits[6:5] = 2 and Register 0x58,

Bits $[11:10] = 1$ forces the device to add the second and third pulses while subtracting the first and fourth pulses, effectively cancelling out the ambient light and electrical offsets and drift.

A comparison of float ambient mode vs. float LED mode is shown in [Table 33](#page-51-1) an[d Table 34.](#page-51-2)

Figure 55. Example Timing Diagram of Four Pulse Float LED Mode Sequence

Table 33. Float Ambient Mode—Measure Ambient Light Level

Pulse	Float Time	Integrated Charge	Calculation	Result
	Shorter	Offset, Ambient 1 (shorter time)	Subtract	Ambient Measurement = Ambient 2 – Ambient 1 (Offset Cancels)
	Longer	Offset, Ambient 1 (shorter time)	Add	
	Not applicable	Not applicable	Not applicable	
\overline{a}	Not applicable	Not applicable	Not applicable	

Table 34. Float LED Mode—Measurement Synchronous Reflected Light from LED

Monitoring Ambient Light Levels in Float LED Mode

In real-world applications, it is common for the ambient light levels to change constantly. When using float LED mode, increasing the amount of ambient light can approach levels where the ambient light uses an unacceptable amount of dynamic range of the charge that can be stored on the photodiode capacitance. For this reason, it is required that the ambient light level is monitored so that configuration changes can be made when necessary, for example, float time, TIA gain, and operating mode. There are two ways to monitor ambient light levels. One way is to use TIA ADC mode in the alternate time slot and continuously monitor the ambient light level. The other way is to use a feature of the ADPD1080/ADPD1081 where the ambient light level is automatically monitored in the background during float mode operation and is compared against a user-defined threshold. If the ambient light level exceeds this threshold by some user-defined number of times, the device sets a flag that can be read by the user or can be output to a GPIO. [Table 35](#page-52-0) lists all the registers used to monitor the ambient light level while in float LED mode.

The user sets an ambient level threshold in the BG_THRESH register, which is the threshold by which the ADC result of the subtract cycles in float LED mode are compared against. The subtract cycles in float LED mode are the positions in the pulse sequence in which the LED pulse is masked; therefore, it is the background level measurement. The ADC result is equal to the raw ADC output minus the contents of the ADC offset register (Register 0x18 to Register 0x1B and Register 0x1E to Register 0x21). In the BG_COUNT register, the user sets a limit on the number of cycles that BG_THRESH is exceeded by the ADC result before the BG_STATUS bit is set for any particular channel. Every time the BG_THRESH value is exceeded by the ADC result during a subtract cycle, an internal counter increments. Each channel has its own counter. When this count exceeds the limit set in the BG_COUNT register, the BG_STATUS bit is set for the channel. The user can periodically monitor the BG_STATUS register to check for asserted bits. Alternatively, a GPIOx pin can be asserted if a BG_STATUS flag is set. See [Table 35](#page-52-0) for the various logical combinations of BG_STATUS flags and interrupts that can be brought out on a GPIOx.

REGISTER LISTING

The recommended values are not shown. Only power-on reset values are shown i[n Table 36.](#page-53-0) The recommended values are largely dependent on use case.

Table 36. Numeric Register Listing

LED CONTROL REGISTERS

Table 37. LED Control Registers

AFE CONFIGURATION REGISTERS

Table 38. AFE Global Configuration Registers

Table 39. AFE Configuration Registers, Time Slot A

Table 40. AFE Configuration Registers, Time Slot B

FLOAT MODE REGISTERS

Table 41. Float Mode Registers

SYSTEM REGISTERS

Table 42. System Registers

ADC REGISTERS

Table 43. ADC Registers

DATA REGISTERS

Table 44. Data Registers

REQUIRED START-UP LOAD PROCEDURE

The required start-up load procedure is as follows:

- 1. Write to 0x1 to Register 0x4B, Bit 7 to enable the clock that drives the state machine.
- 2. Write 0x0001 to Register 0x10 to enter program mode.
- 3. Write to the other registers; the register order is not important while the device is in program mode.
- 4. Write 0x0002 to Register 0x10 to start normal sampling operation.
OUTLINE DIMENSIONS

