

Highly Efficient, Regulated Dual-Output, Ambient Energy Manager for TEG with Optional Primary Battery

Features

Ultra-low power start-up

- Cold start from 60 mV input voltage and $150 \mu W$ input power (typical) with optional external module.
- Cold start from 380 mV input voltage and 100 μ W input power (typical) without optional external module.

Ultra-low power boost regulator

- Open-circuit voltage sensing for MPPT every 21 s.
- Configurable MPPT with 2-pin programming.
- Selectable Voc ratios of 50%, 55% or 75%.
- Harvesting input voltage range from 50 mV to 3.5 V.
- MPPT voltage operation range from 50 mV to 3.5 V.
- Constant impedance matching (ZMPPT).

Integrated 1.2 V/1.8 V LDO regulator

- Up to 20 mA load current.
- Dynamically power-gated by external control.
- Selectable output voltage.

Integrated 1.8 V - 4.1 V LDO regulator

- Up to 80 mA load current with 300 mV drop-out.
- Dynamically power-gated by external control.
- Selectable or adjustable output voltage.

Flexible energy storage management

- Selectable or adjustable overcharge and overdischarge protection for any type of rechargeable battery or (super)capacitor.
- Fast supercapacitor charging.
- Indication when battery is running low.
- Indication when output voltage regulators are available.

Optional primary battery

- Automatic switching to primary battery when the secondary battery is exhausted.

Integrated storage element balancing circuit for dual-cell supercapacitor

Applications

Description

The AEM20940 is an integrated energy management circuit that extracts DC power from a TEG to simultaneously store energy in a rechargeable element and supply the system with two independent regulated voltages. The AEM20940 allows to extend battery lifetime and ultimately eliminate the primary energy storage element in a large range of wireless applications such as industrial monitoring, home automation and smart agriculture.

The AEM20940 harvests the available input current up to 110 mA while regulating the source to a voltage configured by the user. It integrates an ultra-low power boost converter to charge a storage element, such as a Li-ion battery, a thin film battery, a supercapacitor or a conventional capacitor. The boost converter operates with input voltages ranging from 50 mV to 3.5 V.

With its unique cold-start circuit, it can start operating with empty storage elements at an input voltage as low as 380 mV and an input power of only $100 \mu W$. Thanks to an external optional module, the cold start input voltage lowers to 60 mV with an input power of just 150 μ W.

The low-voltage supply typically drives a microcontroller at 1.2 V or 1.8 V. The high-voltage supply typically drives a radio transceiver at 1.8 V, 2.5 V or 3.3 V. Both are driven by highlyefficient LDO (Low Drop-Out) linear regulators for low noise and high stability.

Configuration pins determine various operating modes by setting predefined conditions for the energy storage element (overcharge or overdischarge voltages), and by selecting the voltage of the high-voltage supply and the low-voltage supply.

The chip integrates all active elements for powering a typical wireless sensor. Five capacitors and two inductors are required, all available in small packages. With only seven external components (external cold-start module not included), integration is maximized, footprint and BOM are minimized, optimizing the time-to-market and the costs of designs.

Device Information

Evaluation Board

AEM20940 evaluation boards are available at *[e-peas.com](https://e-peas.com/product/aem20940/)*.

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1. Introduction

The AEM20940 is a full-featured energy efficient power management circuit capable of charging a storage element (battery or supercapacitor, connected to BATT) from an energy source (connected to SRC) as well as supplying loads at different operating voltages through two power supplying LDO regulators (LVOUT and HVOUT).

The heart of the AEM20940 is a cascade of two regulated switching converters, namely the boost converter and the buck converter, both with high power conversion efficiencies (See [Section 12\)](#page-26-0).

At first start-up, as soon as a required cold-start voltage of 380 mV and a scant amount of power of only 100 µW are available from the harvested energy source, the AEM coldstarts. With an optional external module, the cold start voltage can be reduced to 60 mV for a scant amount of power of just 150 μW. After the cold start, the AEM can extract the power available from the source as long as the input voltage is within 50 mV to 3.5 V range. Note that the STONBATT pin makes it possible to bypass the cold start procedure using the pre-charged storage element to start the AEM20940 (see [Section 9.5](#page-17-0)).

Through three configuration pins (CFG[2:0]), the user can select a specific operating mode from a range of seven modes that covers most application requirements without any dedicated external component. These operating modes define the LDO output voltages and the protection levels of the storage element.

The Maximum Power Point (MPP) ratio can be configured using two configuration pins (SELMPP[1:0]) (See [Section 9.2](#page-16-2)).

Two logic control pins (ENLV and ENHV) allow to dynamically activate or deactivate the LDO regulators that supply the low and high voltage load. The status pin STATUS[0] alerts the user that the LDOs are operational and can be enabled. This signal can also be used to enable an optional external regulator.

If the battery voltage gets depleted, LVOUT and HVOUT are power-gated and the controller is no longer supplied by the storage element to protect it from further discharge. Around 600 ms before the shutdown of the AEM, the status pin STATUS[1] alerts the user for a clean shutdown of the system.

However, if the storage element gets depleted and an optional primary battery is connected on PRIM, the AEM20940 automatically uses it as a source to recharge the storage element before switching back to the ambient source. This guarantees continuous operation even under the most adverse conditions (See [Section 8.2.4](#page-14-2)). STATUS[1] is asserted when the primary battery is providing power.

The status of the MPPT controller is reported with one dedicated status pin (STATUS[2]). The status pin is asserted when an MPP calculation is being performed.

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Table 5: Electrical characteristics (Part 2)

1. Minimum V_{SRC} value for harvesting capabilities after coldstart.

2. Maximum V_{MPP} value only when the MPPT is configured on ZMPP (see Section [9.2\)](#page-16-2).

3. To stay in NORMAL MODE, V_{BAT} minimum voltage must stay above V_{OVDIS} .

4. The variability of V_{LV} at 1 mA is 1% (typical and preliminary result from simulations).

5. The variability of V_{HV} at 1 mA is 1.3% (typical and preliminary result from simulations).

6. Recommended Operation Conditions

Table 6: Recommended operating conditions

7. Functional Block Diagram

Figure 3: Functional block diagram

Figure 4: Simplified schematic view of the AEM20940

8. Theory of Operation

8.1. Power Converters

8.1.1. Boost Converter

The boost (or step-up) converter raises the voltage available at BUFSRC to a level suitable for charging the storage element, in the range of 2.2 V to 4.5 V, according to the system configuration. This voltage (V_{BOOST}) is available at the BOOST pin.

The switching transistors of the boost converter are M3 and M4, with the switching node available externally at SWBOOST. The reactive power components of this converter are the external inductor L_{BOOST} and the external capacitor C_{BOMST}

The MPPT control circuit (see [Section 8.3](#page-14-5)) periodically disconnects the source on SRC pin from the BUFSRC pin with the transistor M1 in order to measure the open-circuit voltage of the harvester on SRC and define the optimal SRC regulation voltage.

BUFSRC is decoupled by the capacitor C_{SRC} , which smooths the voltage against the current pulses induced by the boost converter.

The storage element is connected to the BATT pin. Its voltage is named V_{BAT} . This node is linked to BOOST through the transistor M2. In NORMAL MODE (see [Section 8.2.2\)](#page-14-4), this transistor effectively shorts the battery to the BOOST node $(V_{BAT} = V_{BOOST})$. When energy harvesting is occurring, the boost converter delivers a current that is shared between the battery and the LDOs. M2 is opened to disconnect the storage element when V_{BAT} reaches V_{OVDIS} . However, in such a scenario, the AEM20940 offers the possibility of connecting a primary battery to recharge V_{BATT} up to V_{CHRDY} . The transistor M9 connects PRIM to BUFSRC and the transistor M1 is opened to disconnect the SRC input pin as explained in the PRIMARY BATTERY MODE section.

More explanations about the different modes can be found in [Section 8.2](#page-13-4).

8.1.2. Buck Converter

The buck (or step-down) converter lowers the voltage from V_{BOOST} to a constant V_{BUCK} value of 2.2 V. This voltage is available at the BUCK pin. The switching transistors of the buck converter are M5 and M6, with the switching node available externally at SWBUCK. The reactive power components of the buck converter are the external inductor L_{BUCK} and the external capacitor C_{BUCK} .

8.1.3. LDO Outputs

Two Low Drop-Out linear regulators are available to supply loads at different operating voltages:

- Through M7, BOOST supplies the high-voltage LDO that powers its load through HVOUT. This regulator delivers a clean voltage named V_{HV} . When using the built-in configuration modes, an output voltage of 1.8 V, 2.5 V or 3.3 V can be selected. The output is decoupled by the external capacitor C_{HVI} .
- Through M8, V_{BUCK} supplies the low-voltage LDO that powers its load through LVOUT. This regulator delivers a clean voltage named V_{UV} of 1.2 V or 1.8 V. The output is decoupled by the external capacitor C_{LV}

See [Table 5](#page-8-2) for HVOUT and LVOUT maximum current values (respectively I_{HV} and I_{LV}).

Both the high-voltage and the low-voltage outputs can be dynamically enabled or disabled respectively with the logic control pins ENHV and ENLV (see Table below).

ENLV		ENHV	
	Disabled		Disabled
	Enabled		Enabled

Table 7: LDOs configurations

8.2. Operating Modes

Figure 5: Diagram of the AEM20940 modes

8.2.1. Deep Sleep & Wake Up Modes

The DEEP SLEEP MODE is a state where all nodes are deeply discharged and there is no available energy to be harvested. As soon as the required cold-start voltage of 380 mV and the required power of 100 μ W becomes available on SRC, the WAKE-UP MODE is activated. V_{ROOST} and V_{BICK} rise up to a voltage of 2.2 V. V_{BOOST} then rises up to V_{OVCH} .

At this stage, both LDOs are internally disabled. Therefore, STATUS^[0] is low as shown in [Figure 10](#page-21-2) and [Figure 11.](#page-22-0)

When V_{ROOST} reaches V_{OVCH} , two scenarios are possible:

- In the first scenario, a supercapacitor or a capacitor having a voltage lower than V_{CHRDY} is connected to the BATT node (see [Section 8.2.1.2\)](#page-13-5).
- In the second scenario, a charged battery is connected to the BATT node (see [Section 8.2.1.3\)](#page-13-6).

8.2.1.1. Wake Up Mode with the External Cold Start Module

The external cold-start module is an optional auto-oscillating circuit which allows to reduce the minimum input voltage required to coldstart the AEM.

During the cold start, the external module input (connected to CSIN) is internally connected with the energy source (connected to SRC). Once 60 mV and 150 μ W are available on SRC, the external cold-start module generates at least 400 mV on CSOUT. This pin is connected to the AEM20940 internal cold-start module and allows waking up the AEM.

Once V_{BOOST} and V_{BUCK} rise up to a voltage of 2.2 V, the AEM disconnects the link between CSIN and SRC, and extract power directly from the input energy source through SRC.

If the external module is not used on the application, CSOUT and SRC must be shorted and CSIN left floating. In this condition, 380 mV and a power of just 100 µW are required to cold start the AEM.

8.2.1.2. Supercapacitor as a Storage Element

If the storage element is a supercapacitor, the storage element may need to be charged from 0 V. The boost converter charges BATT from the input source and by modulating the conductance of M1 and M2. During the charge of the BATT node, both LDOs are disabled and STATUS[0] is set to low. When V_{BAT} reaches V_{CHRDY} , the circuit enters NORMAL MODE, STATUS[0] is asserted and the LDOs can be enabled by the user using ENLV and ENHV control pins as shown in [Figure 10](#page-21-2).

8.2.1.3. Battery as a Storage Element

If the storage element is a battery but its voltage is lower than V_{CHRW} , the storage element first needs to be charged until it reaches V_{CHBN} . This allows a safety margin to ensure that the storage element is able to provide the required power before enabling the outputs (LDOs).

Once V_{BAT} exceeds V_{CHRDY} , or if the battery was initially charged above V_{CHRDY} , the circuit enters NORMAL MODE. STATUS^[0] is asserted and the LDOs can be dynamically enabled or disabled through ENLV and ENHV as shown in [Figure 11](#page-22-0).

8.2.2. Normal Mode

Once the AEM enters NORMAL MODE, it stays in this mode as long as the following condition is met:

 $V_{\text{OVDIS}} < V_{\text{BATT}} < V_{\text{OVCH}}$

The AEM20940 will switch to another mode in the following cases:

- V_{BAT} increases above V_{OVCH} because the source provides more power than the load consumes. The circuit enters OVERCHARGE MODE, as explained in [Section 8.2.3.](#page-14-6)
- V_{BAT} falls below V_{OVDIS} due to a lack of power from the source. In this case, either the circuit enters SHUTDOWN MODE as explained in [Section 8.2.5](#page-14-7), or, if a charged primary battery is connected on PRIM, the circuit enters PRIMARY BATTERY MODE as explained in [Section 8.2.4](#page-14-8).

8.2.3. Overcharge Mode

When V_{BAT} reaches V_{OVCH} , the battery charge is complete. The AEM maintains V_{BATT} around V_{OVCH} , with a hysteresis of a few mV as shown in [Figure 12,](#page-23-1) to prevent damage to the storage element and to the internal circuitry. In this configuration, the boost converter is periodically activated to maintain V_{BATT} and the LDOs are available. Moreover, when the boost converter is not activated, the transistor M1 in [Figure 4](#page-12-3) is opened to prevent current from the source to the storage element when V_{SRC} is higher than V_{OVCH} .

8.2.4. Primary Battery Mode

When V_{BAT} drops below V_{OVDIS} , the circuit compares the voltage on PRIM with the voltage on FB_PRIM_U to determine whether a charged primary battery is connected on PRIM. The voltage on FB_PRIM_U is set thanks to two optional resistors as explained in [Section 9.3.](#page-16-9)

If the following formula is true, the circuit considers the primary battery as available and the circuit enters PRIMARY BATTERY MODE.

$$
\frac{V_{PRIM}}{4} > V_{FB_PRIM_U}
$$

In that mode, transistor M1 is opened and the primary battery is connected to BUFSRC through transistor M9 to become the source of energy of the AEM20940. STATUS[1] is asserted as long as the chip is in PRIMARY BATTERY MODE.

The AEM remains in this mode until V_{BAT} reaches V_{CHRDY} . At that point, the circuit enters NORMAL MODE.

If no primary battery is used in the application, PRIM, FB_PRIM_U and FB_PRIM_D must be tied to GND.

8.2.5. Shutdown Mode

When V_{BAT} drops below V_{OVDIS} and no power is available from a primary battery, the circuit enters SHUTDOWN MODE, as shown in [Figure 13,](#page-24-1) to prevent deep discharge that could damage the storage element and make the LDOs unstable. The circuit asserts $STATUS[1]$ to warn the application that a shutdown may occur. Both LDO regulators remain enabled during the next 600 ms (T_{CRIT}) .

If no primary battery is used, this mechanism allows the application circuit, whether it is powered on LVOUT or HVOUT, to trigger an interrupt by the low to-high transition of STATUS[1], and to take all appropriate actions before LVOUT and HVOUT are disabled.

If V_{BAT} recovers to V_{OVDIS} within T_{CRIT} (about 600 ms), the AEM switches back to NORMAL MODE. But if, after T_{CRIT} , V_{BATT} does not reach V_{OVDIS} , the circuit enters DEEP SLEEP MODE. Both LDOs are disabled and BATT is disconnected from BOOST to avoid damaging the battery due to the overdischarge. From now on, the AEM must go through the wake-up procedure described in the [Section 8.2.1](#page-13-7).

8.3. Maximum Power Point Tracking

During NORMAL MODE, SHUTDOWN MODE and a part of WAKE-UP MODE, the boost converter is regulated thanks to an internal MPPT (Maximum Power Point Tracking) module. V_{MPP} is the voltage level of the MPP, and depends on the input power available at the source.

The MPPT module evaluates V_{MPP} as a constant fraction of the open-circuit voltage of the source V_{OC} . The ratio between V_{MPP} and V_{OC} can be configured with the SELMPP[1:0] pins.

The AEM20940 periodically measures V_{OC} by stopping to pull current from the source (SRC pin) during $T_{MPPT,VOC}$ (328 ms) every $T_{MPPT PFRION}$ (21 s), thus letting the source rise to its open-circuit voltage. The source target voltage V_{MPP} is then redefined as a fraction of the previously measured V_{OC} . This way, the MPPT module adapts to the harvester variations due to varying ambient conditions. The behavior of the MPPT module is shown in [Figure 6.](#page-14-9)

Figure 6: MPP evaluation behavior

With the exception of this sampling process, the source voltage V_{SRC} is continuously compared to V_{MPP} :

- When V_{SRC} exceeds V_{MPP} by a small hysteresis, the boost converter is switched on, extracting electric charges from the source, thus lowering its voltage.
- When V_{SRC} falls below V_{MPP} by a small hysteresis, the boost converter is switched off, allowing the harvester to accumulate new electric charges into C_{SRC} , which voltage rises.

This way, the boost converter regulates its input voltage so that the electric current (or flow of electric charges) that enters the boost converter yields the best power transfer from the harvester under any ambient conditions. The AEM20940 supports any V_{MPP} level in the range from 50 mV to 3.5 V. It offers a choice of three values for the $V_{\text{MPP}}/V_{\text{OC}}$ ratio through the configuration pins SELMPP[1:0] as shown in [Table 9.](#page-16-10) It is also possible to regulate the source voltage by matching the input impedance of the BOOST converter with an impedance connected to the ZMPP terminal thanks to the ZMPPT feature, by setting SELMPP[1:0] to HH (see [Section](#page-16-11) [9.4](#page-16-11)). The status of the MPPT controller is reported through one dedicated status pins (STATUS[2]). This status pin is asserted when a MPPT module periodic V_{OC} evaluation is being performed.

8.4. Storage Element Balancing Circuit for Dual-cell Supercapacitor

When using a dual-cell supercapacitor, it is necessary to keep both cells at similar voltages to avoid damage due to a potential over-voltage on one cell. This is ensured by the AEM20940 storage element balancing circuit.

If a battery, a capacitor or a single-cell supercapacitor is connected on BATT, BAL is connected to GND and the storage element balancing circuit is disabled.

If a dual-cell supercapacitor is connected on BATT, BAL is connected to the node between the two cells of the supercapacitor. The storage element balancing circuit compensates for any mismatch of the two cells that could overcharge one of both cells. It ensures that BAL remains close to $V_{\text{BAT}}/2$.

9. System Configuration

9.1. Battery and LDOs Configuration

Table 8: Usage of CFG[2:0]

Through three configuration pins (CFG[2:0]), the user can set a particular operating mode from a range that covers most application requirements, without any dedicated external component as shown in [Table 8.](#page-16-12) The three threshold levels are defined as:

- V_{OVCH} : maximum voltage accepted on the storage element before disabling the boost converter.
- V_{CHRDY} : minimum voltage required on the storage element after a cold start before enabling the LDOs.
- V_{OVDIS} : minimum voltage accepted on the storage element before considering the storage element as depleted.

See [Section 8](#page-12-4) for more information about the purposes of these thresholds.

The two LDOs output voltages are called V_{HV} and V_{UV} for the high and low output voltages respectively. Seven combinations of these voltage levels are hard-wired and selectable through the CFG[2:0] configuration pins, covering most application cases.

9.2. MPPT Configuration

Two dedicated configuration pins, SELMPP[1:0], allow selecting the MPP tracking ratio based on the characteristic of the input power source.

SELMPP[1]	SELMPP[0]	V_{MPP} / V_{OC}
		50%
	н	55%
		75%
	н	ZMPP

Table 9: Usage of SELMPP[1:0]

9.3. Primary Battery Configuration

To use the primary battery, it is mandatory to determine $V_{PRIM,MIN}$, the voltage at which the primary battery is considered as fully depleted. The circuit uses a resistive divider between BUCK and FB_PRIM_D to define the voltage on FB_PRIM_U as $V_{PRIM,MIN}$ divided by 4. During $V_{PRIM,MIN}$ evaluation, the circuit connects FB_PRIM_D to GND.

When $V_{PRIM,MIN}$ is not evaluated, FB_PRIM_D is left floating to avoid quiescent current on the resistive divider. The resistors are calculated as follows:

- $-R_P = R7 + R8$
- $100 \text{k}\Omega \leq R_\text{p} \leq 500 \text{k}\Omega$

$$
- \quad R7 = \frac{V_{PRIM_MIN}}{4} \cdot R_p \cdot \frac{1}{2.2V}
$$

$$
- \quad R8 = R_p - R7
$$

NOTE: FB_PRIM_U, FB_PRIM_D and PRIM must be tied to GND if no primary battery is used.

9.4. ZMPPT Configuration

Instead of working at a ratio of the open-circuit voltage, the AEM20940 can regulate the input impedance of the BOOST converter so that it matches a constant impedance connected to the $ZMPP$ pin (R_{ZMPP}) . In this case, the AEM20940 regulates V_{SRC} at a voltage equal to the product of the ZMPP impedance and the current available at the SRC input.

 $-10\Omega \leq R_{\text{ZMPP}} \leq 1\text{M}\Omega$

9.5. Start-on-battery Configuration

Alternatively to the cold start procedure described in [Section](#page-13-7) [8.2.1,](#page-13-7) by connecting STONBATT to BATT, the circuit can also start with the energy provided by the storage element connected on BATT if its voltage is higher than V_{CHRDY} .

NOTE: The AEM20940 will not start if the voltage on BATT is lower than V_{CHRDY}

9.6. No-battery Configuration

If the application doesn't use a storage element, the PCB must include a capacitor on the BATT pin. See [Section 9.8](#page-17-5) for C_{BATT} value.

The storage element may not be necessary in the following cases:

- If the harvested energy source is permanently available and covers the application purposes.
- - If the application does not need to store energy when the harvested energy source is not available.

9.7. Supplying an Application Circuit with BUCK

It is possible to supply an application circuit directly from BUCK, with the benefit of high BATT to BUCK efficiency, provided that the following conditions are met:

- The application circuit can be supplied from a voltage in the 2.0 V - 2.5 V range (V_{BUCK} is typically 2.2 V with ripple, see [Table 5](#page-8-2)).
- The sum of the following currents must be below the maximum I_{BUCK} value (see [Table 5\)](#page-8-2):
	- Current of the load connected to BUCK.
	- Current of the load connected to LVOUT.
- The application circuit on BUCK does not pull current during the AEM20940 cold start.

To satisfy the last condition, the following circuit may be implemented:

Q1 is a N-MOSFET, whose gate is driven by STATUS[0] with R1 as a pull-down resistor. When the AEM20940 is in DEEP SLEEP MODE or in WAKE-UP MODE, STATUS[0] is LOW (see [Section](#page-13-4) [8.2](#page-13-4)), ensuring that Q1 is non-conducting, and thus that the application circuit is not supplied.

When the AEM20940 switches from WAKE-UP MODE to NORMAL MODE, STATUS[0] is HIGH, making Q1 conducting. The application circuit is then supplied by BUCK, and remains so when the AEM20940 is in NORMAL MODE, OVERCHARGE MODE, PRIMARY BATTERY MODE and SHUTDOWN MODE.

Q1 must be chosen as follows:

- Low Gate-Source Leakage I_{GSS}.
- Low Zero Gate Voltage Drain Current I_{DSS}.
- Drain-Source On-State Resistance R_{DS(on)} low enough to supply application circuit with an acceptable voltage drop.
- V_{GS} maximum voltage must be above V_{OVCH} (STATUS[0] HIGH voltage is V_{BONST}).
- Maximum gate-source threshold voltage $V_{GS(th),MAX}$ matches the following, with $V_{\text{BUEK,MAX}}$ being V_{BUEK} maximum value stated in [Table 5:](#page-8-2)

 $V_{GS(th)}$ MAX $V_{OVDIS} - V_{BIICK$ MAX

9.8. Storage Element Information

The energy storage element of the AEM20940 can be a rechargeable battery, a supercapacitor or a large capacitor. It should be chosen so that its voltage does not fall below V_{OVDIS} even during occasional peaks of the load current. If the internal resistance of the storage element cannot sustain this voltage limit, it is advisable to buffer the battery by decoupling it with a capacitor.

The BATT pin, connecting the storage element, must never be left floating. If the application expects a disconnection of the battery (e.g., because of a user removable connector), the PCB must include a capacitor:

- If the LDOs are used, the minimum needed capacitor value is 150 µF.
- If the LDOs are not used, the minimum needed capacitor value is 22 µF.

The leakage current of the storage element should be small as leakage currents directly impact the quiescent current of the subsystem.

Figure 7: Schematic for supplying an application circuit with BUCK

9.9. External Inductors Information

The AEM20940 operates with two standard miniature inductors. Switching frequency must be at least 10 MHz for both. Low equivalent series resistance (ESR) favors the power conversion efficiency of the boost and buck converters.

L_{BOOST}

The AEM20940 circuit is typically implemented with one of the following values on L_{ROOST} :

- 10 µH (peak current min. 250 mA) allows higher current from SRC to BATT.
- 22 µH (peak current min. 115 mA) allows better efficiencies, especially at low SRC voltages.

L_{BUCK}

The buck inductor L_{BUCK} must sustain a peak current of at least 50 mA. The recommended value is 10 µH.

9.10. External Capacitors Information

The AEM20940 operates with:

- Four identical standard miniature ceramic capacitors of 10 µF.
- One miniature ceramic capacitor of 22 µF.

The leakage current of the capacitors should be small as leakage currents directly impact the quiescent current of the subsystem.

C_{SRC}

This capacitor acts as an energy buffer at the input of the boost converter. It prevents large voltage fluctuations of V_{SRC} when the boost converter is switching. The recommended value is 10 µF +/- 20%.

C_{BUCK}

This capacitor acts as an energy buffer for the buck converter. It also reduces the voltage ripple induced by the current pulses inherent to the switching mode of the converter. The recommended value is 10 µF +/- 20%.

C_{BOOST}

This capacitor acts as an energy buffer for the boost converter. It also reduces the voltage ripple induced by the current pulses inherent to the switching mode of the converter. The recommended value is 22 μ F +/- 20%.

C_{HV} / C_{LV}

These capacitors ensure a high-efficiency load regulation of the high-voltage and low-voltage LDO regulators. Closed-loop stability requires the value to be in the range of 8 μ F to 14 μ F.

10. Typical Application Circuits

10.1. Example Circuit 1

Figure 8: Typical application circuit 1

The energy source is a thermoelectric generator and the storage element is a standard Li-ion battery cell. The radio communication is supplied by HVOUT set at 3.3 V. The micro-controller that controls the application is supplied by LVOUT set at 1.8 V.

STONBATT is tied to BATT, bypassing the cold-start procedure, to start thanks to the energy stored in the precharged Li-ion battery cell.

Once the start-on-battery configuration is enabled, the external cold-start module is not useful for this application and by consequence, CSOUT and SRC are shorted.

This circuit uses a pre-defined AEM configuration, typical of systems that use standard components for radio and energy storage.

The operating mode pins are set as follows:

- $CFG[2:0] = HHH$ (all to V_{BUCK})

Referring to Table [8](#page-16-7), in this mode, the threshold voltages are:

- $V_{\text{OVCH}} = 4.12 \text{ V}$
- V_{CHRDY} = 3.67 V
- $-V_{OVDIS} = 3.60 V$

Moreover, the LDOs output voltages are:

- $-V_{\text{HV}}$ = 3.3 V
- $-V_{\text{UV}}$ = 1.8 V

A primary battery is also connected as a back-up solution. The minimal level allowed on this battery is set at 3.5 V. Following equations from [Section 9.3](#page-16-3):

- R_p = 0.5MΩ
\n- R7 =
$$
\frac{3.5V}{4}
$$
 · 0.5MΩ · $\frac{1}{2.2V}$ = 200kΩ
\n- R8 = 0.5MΩ – 200kΩ = 300kΩ

The MPP configuration pins SELMPP[1:0] are tied to GND (logic LOW), thus, selecting an MPP ratio of 50%.

The LVOUT LDO output is enabled by tying ENLV to BUCK.

The micro-controller is supplied by LVOUT, that is enabled when V_{BAT} and V_{BOOST} voltage rise above V_{CHRDY} .

The application software can enable or disable the radio transceiver supply with a GPIO connected to ENHV.

10.2. Example Circuit 2

Figure 9: Typical application circuit 2

The energy source is a thermoelectric generator and the storage element is a dual-cell supercapacitor. Please note that the supercapacitor might be completely depleted during the cold start. Consequently, STONBATT is tied to GND to use the input energy source only.

To decrease the minimum voltage required for the cold start, the external cold-start module has been connected to CSIN and CSOUT.

Moreover, BAL is connected to the dual-cell supercapacitor to compensate for any mismatch between the two cells and, in that way, protect the supercapacitor.

A micro-controller acts as the application master. The operating mode pins are set as follows:

 $CFG[2:0] = LHL$

The storage element voltages are set as follows with a custom configuration:

- V_{OVCH} = 4.5 V
- $-V_{CHRDY}$ = 3.92 V
- $-V_{\text{OVDIS}}$ = 3.6 V

The LDO voltages are set as follows:

- $-V_{\text{HV}}$ = 3.3 V
- $-V_{\text{LV}} = 1.8 \text{ V}$

Enabling and disabling LVOUT is controlled by the application circuit with a micro-controller GPIO connected to ENLV.

ENHV is tied to BUCK so that HVOUT is always on.

The micro-controller is supplied by HVOUT, which is enabled when V_{BATT} and V_{BOOST} voltages rise above V_{CHRDY} .

The MPP configuration pins SELMPP[1:0] are tied to BUCK (logic HIGH), thus, selecting the ZMPPT configuration to match a 1-kΩ impedance.

No primary battery is connected: PRIM, FB_PRIM_U and FB_PRIM_D pins are tied to GND.

11. Circuit Behavior

11.1. Cold-start Behavior

11.1.1. (Super)capacitor as a Storage Element

The following figure shows the AEM20940 behavior with a capacitor connected to BATT and the following settings:

- $-CFG[2:0] = LHH$
- $-$ SELMPP $[1:0]$ = HL (75%)
- $-C_{\text{BAT}} = 4.85 \text{ mF}$
- SRC: 1 mA current source with 3 V voltage compliance
- $-$ ENHV = ENLV = H
- 22 kΩ resistive load on LVOUT
- 2 kΩ resistive load on HVOUT

Figure 10: Cold start with a capacitor connected to BATT

11.1.2. Battery as a Storage Element

The following figure shows the AEM20940 behavior with a pre-charged capacitor (acting as a battery) connected to BATT and the following settings:

- $-CFG[2:0] = LHH$
- $-$ SELMPP $[1:0]$ = HL (75%)
- $-C_{\text{BAT}} = 4.85 \text{ mF}$
- SRC: 1 mA current source with 3 V voltage compliance
- $-$ ENHV = ENLV = H
- 22 kΩ resistive load on LVOUT
- 2 kΩ resistive load on HVOUT

Figure 11: Cold start with a battery connected to BATT

11.2. Overcharge Mode Behavior

The following figure shows the AEM20940 behavior in OVERCHARGE MODE with the following settings:

- $-CFG[2:0] = HHH$
- $-$ SELMPP $[1:0]$ = HL (75%)
- $-C_{\text{BATT}}$ = 4.85 mF
- SRC: 1 mA current source with 3 V voltage compliance
- $-$ ENHV = ENLV = H
- 22 kΩ resistive load on LVOUT
- 2 kΩ resistive load on HVOUT

Figure 12: Overcharge mode

11.3. Shutdown Mode Behavior

11.3.1. Without Primary Battery

The following figure shows the AEM20940 behavior in SHUTDOWN MODE with the following settings:

- $-CFG[2:0] = LHL$
- $-$ SELMPP $[1:0]$ = HL (75%)
- $-C_{\text{BAT}} = 4.85 \text{ mF}$
- SRC: left floating to let the storage element on BATT discharge
- $-$ ENHV = ENLV = H
- 22 kΩ resistive load on LVOUT
- 22 kΩ resistive load on HVOUT
- PRIM, FB_PRIM_U and FB_PRIM_D connected to GND

Figure 13: Shutdown mode (without primary battery)

11.3.2. With Primary Battery

The following figure shows the AEM20940 behavior in SHUTDOWN MODE with the following settings:

- $-CFG[2:0] = HHH$
- $-$ SELMPP $[1:0]$ = HL (75%)
- $-C_{\text{BATT}}$ = 4.85 mF
- SRC: left floating to let the storage element on BATT discharge
- $E N H V = E N L V = H$
- 22 kΩ resistive load on LVOUT
- 22 kΩ resistive load on HVOUT
- PRIM: 3 V voltage source with 1 mA current compliance
- R7 = 68 kΩ
- $-R8 = 330 kΩ$

e.pea

12.1. BOOST Conversion Efficiency for LBOOST = 10 µH

Figure 15: Boost efficiency for Isrc at 100µA, 1mA, 10mA and 100mA (LBOOST = 10 µH)

12.2. BOOST Conversion Efficiency for LBOOST = 22 µH

 0 $^{+}$

Figure 16: Boost efficiency for Isrc at 100µA, 1mA and 10mA (LBOOST = 22 µH)

.0 0.5 1.0 1.5 2.0 2.5 3.0 3.5 4.0 4.5 V_{SRC} [V] (I_{SRC} = 10 mA)

 $V_{BOOST} = 3.6 V$ $V_{BOOST} = 4.1 V$

12.3. BUCK Conversion Efficiency

The following graph shows the buck converter efficiency from BATT to BUCK with the AEM20940 quiescent current I_Q subtracted.

Figure 17: Buck Efficiency (L_{BUCK} = 10 µH)

12.4. Quiescent Current

12.5. High-voltage LDO Regulation

12.7. High-voltage LDO Efficiency

The theoretical efficiency of an LDO can be calculated as Vout / Vin if quiescent current can be neglected with regards to the output current. For the high-voltage LDO, the theoretical efficiency is equal to V_{HV}/V_{BAT}

12.8. Low-voltage LDO Efficiency

The theoretical efficiency of an LDO can be calculated as V_{LV}/V_{BUCK} . Starting from the battery, the efficiency of the buck converter (ηbuck) has to be taken into account (see [Figure 4\)](#page-12-2).

The efficiency between V_{BAT} and V_{LV} is therefore equal to:

$$
\eta_{\text{BUCK}}\cdot\frac{V_{\text{LV}}}{V_{\text{BUCK}}}
$$

13. Schematic

Figure 23: Schematic example

Table 10: BOM example for AEM20940 and its required passive components

14. Layout

14.1. Guidelines

Good layout practices are mandatory in order to obtain good AEM20940 stability, best efficiency and avoid EMI problems.

The following list, while not exhaustive, shows the main attention points when routing a PCB with the AEM20940:

- The switching nodes (BUFSRC, SWBOOST, SWBUCK and BUCK) must be kept as short as possible, with minimal track resistance and minimal track capacitance. Low resistance is obtained by keeping track length as short as possible and track width as large as possible between these switching nodes and the AEM20940 pins. Minimal capacitance is obtained by maintaining a large distance between the switching nodes and other signals. We recommend removing the ground plane, the power plane and the bottom layer ground pour under L_{BOOST} and L_{BUGK} footprints, as well as adding distance between BUFSRC/SWBOOST and the top ground pour, as shown in [Figure 24](#page-34-2).
- The decoupling capacitors (C_{BOOST} C_{BUCK} C_{SRC} C_{HV} $-C_{LV}$ - C_{BAT}) must be placed as close as possible to the AEM20940, with direct connection and minimum track resistance for the corresponding power nodes (BOOST, BUCK, BUFSRC, HVOUT, LVOUT and BATT).
- The GND return path between the decoupling capacitors and the AEM20940 thermal pad, which is the AEM20940 main GND connection, must be as direct and short as possible. This is preferably done on the top layer when possible, otherwise by internal/bottom plane, using low resistance vias to decrease layer-to-layer connection resistance. In [Figure 24](#page-34-2), this GND return path is done on an internal plane.
- The external DC power connections (SRC, HVOUT, LVOUT and BATT) must be connected to the AEM20940 with low resistance tracks.
- If used, ZMPP must be connected to the AEM20940 with a low resistance track, according to the expected SRC power.
- The BAL pin connection track must be able to handle at least 40 mA.
- The custom mode setting pins SET OVDIS, SET CHRDY and SET OVCH are high impedance analog inputs typically connected to a resistive divider with high resistor values, making those three nodes prone to pickup noise. Thus, it is recommended to keep those as short as possible and as far as possible to noise sources such as DCDC switching nodes.
- The configuration pins and the status pins have minimal layout restrictions.

14.2. Layout Example

Figure 24: Layout example for the AEM20940 and its passive components

15. Package Information

15.1. Plastic Quad Flatpack No-lead (QFN 28-pin 5x5mm)

Figure 25: QFN 28-pin 5x5mm drawing (all dimension in mm)

15.2. Board Layout (QFN 28-pin 5x5mm)

16. Glossary

AEM

Ambient Energy Manager.

BOM

Bill Of Materials.

C_{BATT}

Capacitor connected on the BATT pin (if no storage element connected).

CBOOST

Output capacitor of the BOOST converter.

CBUCK

Output capacitor of the BUCK converter.

C_{HV}

High-voltage LDO regulator decoupling capacitor.

CLV

Low-voltage LDO regulator decoupling capacitor.

CSRC

BUFSRC pin decoupling capacitor.

GPIO

General Purpose Input / Output.

IBUCK

Total load current supplied by the BUCK converter (including the LVOUT current I_{UV}).

IHV

Load current supplied by the high-voltage LDO regulator.

ILV

Load current supplied by the low-voltage LDO regulator.

IPRIM

Current from the primary battery.

IQ

Quiescent current on BATT when no energy is available on SRC.

ISRC

Harvested current from the energy source.

LBOOST

BOOST converter inductor.

LBUCK

BUCK converter inductor.

LDO

Low Drop-Out.

MPPT

Maximum Power Point Tracking.

PCB

Printed Circuit Board.

PSRC_CS

Minimum power available on SRC for the AEM20940 to coldstart.

R_p

Sum of resistors for setting the primary battery minimum voltage. $R_p = R7 + R8$.

RZMPP

Resistor that defines the AEM20940 BOOST converter input resistance when used in ZMPP mode.

TCRIT

Time before shutdown once STATUS[1] has been asserted.

TEG

Thermoelectric Generator.

TMPPT,VOC

Open-circuit duration for the MPP evaluations.

TMPPT,PERIOD

Time between two MPP evaluations.

V_{BATT}

Voltage on the BATT pin.

VBOOST

Output voltage of the BOOST converter.

VBUCK

Output voltage of the BUCK converter.

V_{CHRDY}

Charge ready voltage on the BATT pin.

VFB_PRIM_U

Feedback for the minimal voltage level on the primary battery.

VHV

Output voltage of the high-voltage LDO regulator.

V_{IV}

Output voltage of the low-voltage LDO regulator.

V_{MPP}

Target regulation voltage on SRC when extracting power.

V_{oc}

Open-circuit voltage of the harvester connected to the SRC pin.

VOVCH

Over-charge voltage on the BATT pin.

V_{OVDIS}

Over-discharge voltage on the BATT pin.

V_{PRIM}

Voltage on the primary battery.

VPRIM,MIN

Voltage at which the primary battery is considered fully depleted.

V_{SRC}

Voltage on the SRC pin.

ZMPPT

Maximum Power Point Tracking with constant impedance.