

AP3981C

Description

The AP3981C is a high performance power switchers integrated with a primary side regulation controller and an N-channel power MOSFET. It can be used for battery charger and adaptor applications, accurate Constant Voltage (CV) and Constant Current (CC) can be achieved without an opto-coupler and secondary control circuitry.

The AP3981C operates in Pulse Frequency Modulation (PFM) mode and peak current Amplitude Modulation (AM) mode to form a fine tune frequency curve within the whole power range. Therefore, the AP3981C can achieve high average efficiency and improve audible noise.

The AP3981C provides comprehensive protections without additional circuitry. It contains V_{CC} over voltage protection, output over voltage protection, output under voltage protection, output short circuit protection, cycle-by-cycle current limit, open loop protection, and internal over temperature protection, etc.

The AP3981C is available in SO-8 package.

Features

- Primary Side Control for Eliminating Opto-Coupler
- Built-In 650V Power MOSFET
- 75mW No-Load Input Power
- Flyback Topology in DCM Operation
- External Adjustable Line Compensation for CC
- Fixed Internal Cable Compensation
- Multiple Segment AM/PFM Control Mode to Improve Audio Noise and Efficiency
- Frequency Jitter to Improve System EMI
- Capacitive Load Start-Up Capability
- Valley-On for the Higher Efficiency and Better EMI Behavior
- Multiple Protections:
	- Secondary-Side Over Voltage Protection (SOVP)
	- Secondary-Side Under Voltage Protection (SUVP)
	- Output Short Circuit Protection (SCP)
	- Transformer Saturation Protection (TSP) via Primary Peak Current Limitation
	- Internal Over Temperature Protection (OTP)
- SO-8 Package
- **Totally Lead-Free & Fully RoHS Compliant (Notes 1 & 2)**
- **Halogen and Antimony Free. "Green" Device (Note 3)**
- Notes: 1. No purposely added lead. Fully EU Directive 2002/95/EC (RoHS), 2011/65/EU (RoHS 2) & 2015/863/EU (RoHS 3) compliant.
	- 2. See [https://www.diodes.com/quality/lead-free/ fo](https://www.diodes.com/quality/lead-free/)r more information about Diodes Incorporated's definitions of Halogen- and Antimony-free, "Green" and Lead-free.
	- 3. Halogen- and Antimony-free "Green" products are defined as those which contain <900ppm bromine, <900ppm chlorine (<1500ppm total Br + Cl) and <1000ppm antimony compounds.

PRIMARY SIDE REGULATED POWER SWITCHER

Pin Assignments

Applications

- Routers
- Set-Top Box (STB) Power Supply
- Network Adaptors

Typical Applications Circuit

Pin Descriptions

NEW PRODUCT

NEW PRODUCT

Absolute Maximum Ratings (Note 4)

Notes: 4. Stresses greater than those listed under "*Absolute Maximum Ratings*" can cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "*Recommended Operating Conditions*" is not implied. Exposure to "Absolute Maximum Ratings" for extended periods can affect device reliability.
5. Test condition: Device mounted on FR-4 substrate PC board, 2oz copper, with 1inch² cooling area.

Recommended Operating Conditions

Electrical Characteristics (@T_A =+25°C, V_{CC} = 15V, unless otherwise specified.)

Electrical Characteristics (@T_A =+25°C, V_{CC} = 15V, unless otherwise specified.) (continued)

Note: $6.$ The aging condition of drain-source voltage is 80% of BV_{DSS.}

Performance Characteristics

Minimal Operating Voltage vs. Ambient Temperature Operating Current vs. Ambient Temperature

Ambient Temperature (°C)

V_{CS_H} vs. Ambient Temperature to be to by to by to the sum of th

Performance Characteristics (continued)

Feedback Voltage vs. Ambient Temperature V_{CC} OVP Voltage vs. Ambient Temperature

Ambient Temperature (°C)

Ambient Temperature (°C)

AP3981C Document number: DS41619 Rev. 2 - 2

Operation Description

1. The Conventional PSR Operating Waveforms

Figure 1. The Operation Waveform of Flyback PSR System

Figure 1 shows the typical waveforms which demonstrate the basic operating principle of AP3981C application. And the parameters are defined as following.

IP---The primary side current

I^S ---The secondary side current

IPK---Peak value of primary side current

IPKS---Peak value of secondary side current

VSEC---The transient voltage at secondary winding

VO---The output voltage

VAUX---The transient voltage at auxiliary winding

V_A--- The stable voltage at auxiliary winding when rectification diode is in conducting status, which equals the sum of voltage VCC and the forward voltage drop of auxiliary diode

tSW ---The period of switching frequency

tONP ---The conduction time when primary side switch is "ON"

tONS ---The conduction time when secondary side diode is "ON"

tOFF ---The dead time when neither primary side switch nor secondary side diode is "ON"

tOFFS --- The time when secondary side diode is "OFF"

For primary-side regulation, the primary current ip(t) is sensed by a current sense resistor R_{CS} connected to pin SOURCE. The current rises up linearly at a rate of:

$$
\frac{dip(t)}{dt} = \frac{V_{\text{IN}}(t)}{L_M} \tag{1}
$$

As illustrated in Figure 1, when the current ip(t) rises up to I_{PK}, the primary MOSFET would turn off. The constant peak current is given by:

$$
I_{PK} = \frac{V_{CS}}{R_{CS}}\tag{2}
$$

The energy stored in the magnetizing inductance L_M each cycle is therefore:

$$
E_g = \frac{1}{2} \times L_M \cdot I_{p_K}^2 \tag{3}
$$

So the power transferring from the input to the output is given by:

$$
P = \frac{1}{2} \times L_M \times I_{PK}^2 \times f_{SW}
$$
 (4)

Where, the fsw is the switching frequency. When the peak current I_{PK} is constant, the output power would depend on the switching frequency fsw.

2. Constant Voltage Operation

The output voltage is proportional to the auxiliary winding voltage during t_{ONS} period indicated by Formula 5, this auxiliary winding voltage is divided by resistors R_{FB1} and R_{FB2} (refer to Figure 5) before inputting to the FB pin. As Figure 2 illustrated, the AP3981C detects the FB voltage at the end of t_{SAMPLE} during t_{ONS} period, the detected voltage which reflects the output voltage is regulated to V_{FB} of 2.4V with the help of the constant voltage control block in the AP3981C. For system design, adjusting the ratio of RFB1 and RFB2 can get the target output voltage value.

Vo Vd N N V AUX S AUX (5) 0V ^tONS ^tSAMPLE tSW Figure 2. Auxiliary Voltage Waveform

3. Constant Current Control

In the AP3981C, Formula 6 shows the related parameters that determine the output current. To get a constant output current, the V_{CS} and t_{ONS}/t_{SW} is fixed in AP3981C during CC mode. Meanwhile, the reliable control logic is integrated within AP3981C to ensure the system swift smoothly between CC mode and CV mode.

$$
I_{\text{OUT}} = \frac{1}{2} * \frac{Np}{Ns} * Ipk * \frac{t_{\text{ONS}}}{t_{\text{SW}}} = \frac{1}{2} * \frac{Np}{Ns} * \frac{Vcs}{Rcs} * \frac{t_{\text{ONS}}}{t_{\text{SW}}} \tag{6}
$$

4. Multiple Segment Peak Current

In the original PFM PSR system, the switching frequency decreases with the decreasing output current, which will encounter audible noise issue when switching frequency decreases below 20kHz.

In order to avoid audible noise issue and a big drop in efficiency at light load, the AP3981C uses a 3-segment primary peak current control method at CV mode, the current sense threshold voltage is piecewise defined. As shown in Figure 3, the low threshold V_{CS_L} is set under 2% CC load, the high threshold V_{CS_H} is set above 40% CC load. Within the range from 2% to 40%, the threshold V_{CS_M} increases basing on the load condition, the V_{CSM} is carefully calculated inside the AP3981C to make the system operate at a reasonable switching frequency which rises above 20kHz at a varying slope.

Figure 3. Segment Peak Current and Operating Frequency at CV Mode

5. Sample Time

As shown in Equation 5 and Figure 2, the detected auxiliary voltage reflects the output voltage. To be compatible with different system designs and avoid the turn-off ringing voltage influence on CV sampling, the t_{SAMPLE} is designed to be proportional of t_{ONS}. On the other hand, to alleviate the Vd effect on the accuracy of V_{OUT}, the sample ratio of t_{SAMPLE} to t_{ONS} varies according to load condition. The t_{SAMPLE} is usually 50% of t_{ONS} for the below 2% CC load conditions and 80% of $t_{\rm ONS}$ for the above 40% CC load conditions, within the range from 2% to 40% loading, the sample ratio rises linearly from 50% to 80%.

6. Capacitive Load Start-Up Capability

In order to achieve fast start-up for capacitive load startup applications, the AP3981C induces a two level CC point design during start up time. The output voltage rises after power on, when the detected output voltage is lower than SUVP point, the t_{ONS}/t_{SW} is set to be 0.75, which means output constant current is 1.5 times of normal output constant current. When the output voltage rises above SUVP point, the t_{ONS}/t_{SW} is switched to the normal value of 0.5.

7. Leading Edge Blanking

When the power switch is turned on, a turn-on spike voltage will occur on the V_{CS} sense resistance. To avoid false-termination of the switching pulse, a fixed 470ns leading-edge blanking time is built in. During this blanking period, the current sense comparator is disabled and the primary MOSFET cannot be turned off.

8. Valley Turn-On

When the off time (t_{OFF}) is shorter than t_{VAL-ON}, the AP3981C power system can work with valley turn-on. It can reduce the switching-on power losses and achieve high overall efficiency. At the same time, because of valley turn-on the switching frequency has the random jitter feature, which will be of benefit to conductive EMI performance. The valley turn-on can also reduce the power switch turn-on spike current and then achieve the better radiative EMI performance.

9. VCS Jitter

Even though the valley turn on function produces the random frequency jitter feature, an active frequency jitter function is added in the AP3981C. The active frequency dithering is realized by applying variation on V_{CS} reference (V_{CS_REF}). The V_{CS_REF} is changed every 2 cycles and the period of variation is 12 cycles, which is shown as Figure 4. The variation between V_{CS4} and V_{CS1} is +/-2% using the mean level as a reference.

Figure 4. V_{CS} Jitter

10. Adjustable Line Compensation

In real system, there exists a delay time, from the V_{SOLRCE} reach the inner V_{CS} threshold to the actual switch turn-off point. The delay time contains the propagation time of the inner comparator and the driver delay, and it does not change with line voltage. The delay time leads to different primary peak current under different line voltage, which results in different output current in CC mode.

Figure 5. Line Compensation Control Circuit

In order to alleviate the difference under the universal input voltage, the AP3981C integrates the line compensation control circuit shown as Figure 5. During the primary on stage, an inner switcher R_S switches on, the R_{LC} is much smaller compared with R_{FB2}, so the R_{FB2}'s effect on line compensation can be neglected, the proportional line voltage is detected through RFB1 and RLC and is added to the VCs threshold (VCS_REF). The V_{LC} can be derived from the Formula 7:

$$
V_{LC} = \frac{\frac{R_{FBI}}{3 \times R2} \times V_{PP} - V_{AUX}}{1 + \frac{R_{FBI}}{3 \times R2} + \frac{R_{FBI}}{R_{LC}}}
$$
(7)

The final compensated V_{CS} is:

$$
V_{CS_{REF}} = \frac{1}{3} * V_{PP} + \frac{2}{3} * V_{LC}
$$
 (8)

In the above formulas, V_{PP} is 1.8V at CC mode, R_{LC} is 55 Ω , R2 is 60k Ω , R1 is two times of R2, V_{AUX} is the auxiliary winding voltage during primary-on period, which is proportional to bus voltage. Based on the formula, we can make a conclusion that a smaller RFB1 results in deeper line compensation. If we know the delay time t_{DELAY}, typically 150ns in AP3981C, we can calculate the R_{FB1} as a reference for the system design.

11. Protection

The AP3981C provides versatile protections to prevent the system from damage under various fault conditions. Most protections will trigger autorecovery mode in which the system will restart as soon as the V_{CC} drops to V_{OPR(MIN)}, when the fault conditions are removed, the system will recover to normal operation automatically.

VCC OVP

A V_{CC} OVP threshold is set to protect the IC from damage. When the V_{CC} OVP protection is triggered, the IC will stop outputting drive signal immediately and the system will enter auto-recovery mode.

Output Over Voltage Protection (SOVP)

As it is described above that the FB pin voltage during t_{ONS} reflects the output voltage proportionally, this voltage can be used to realize SOVP. The AP3981C set a higher threshold, $V_{FB(OVP)}$ to shut down the system if the sampled voltage reached the threshold continuously for 3 switching cycles, the SOVP will be triggered and the system will enter auto-recovery mode.

Output Under Voltage Protection (SUVP)

Like SOVP, the AP3981C also integrates the SUVP protection. If the detected voltage on FB pin is lower than V_{FB(SUVP)} for 128ms, the SOVP will be triggered and the system will enter auto-recovery mode.

Output Short Protection (SCP)

A much lower threshold is set on FB pin to protect the system when output short condition occurs. If the detected FB voltage is lower than 0.78V for 64ms, the SCP will be triggered and the system will enter auto-recovery mode.

Transformer Anti-Saturation Protection

Under some fault conditions or bad system design, the transformer may approach saturation and the current increases dramatically. To avoid power device damage since of transformer saturation, the AP3981C integrates a maximum V_{CS} threshold V_{CS(MAX)} to protect the system. If there are 3 consecutive pulses where V_{CS} exceeds the threshold, the controller will shut down and enter auto-recovery mode.

Over Temperature Protection (OTP)

If the IC junction temperature exceeds the threshold of T_{OTP} , AP3981C will shut down immediately and enter auto-recovery mode. Note that even when the V_{CC} reaches V_{TH_ST}, the IC will not output any drive pulse until the junction temperature falls of a hysteresis temperature of +30°C.

Brown In/ Brown Out Protection

The AP3981C detects the bus voltage at each switching cycle through FB pin during t_{ONP} period. When the V_{CC} reaches V_{TH ST} after power on, the AP3981C will output one switching pulse to check if the detected bus voltage on FB pin is higher than V_{FB_NEG_H}. If so, the system will start up normally, otherwise the AP3981C will stop outputting following pulses, then the V_{CC} will drop below V_{OPR(MIN)} and the system will repeat the process described above until the detected FB voltage is higher than V_{FB_NEG_H}. When the power is off or there is a ditch in bus voltage, if the detected voltage is lower than V_{FB-NEG} for 3 consecutive switching cycles, the IC will shut down and enter auto-recovery mode. This function is very useful when the bulk capacitor is open, or when the heavy load suddenly released after power off.

Ordering Information

Marking Information

SO-8

Package Outline Dimensions

Please see <http://www.diodes.com/package-outlines.html> for the latest version.

(1) Package Type: SO-8

Suggested Pad Layout

Please see <http://www.diodes.com/package-outlines.html> for the latest version.

(1) Package Type: SO-8

Note: The suggested land pattern dimensions have been provided for reference only, as actual pad layouts may vary depending on application. These dimensions may be modified based on user equipment capability or fabrication criteria. A more robust pattern may be desired for wave soldering and is calculated by adding 0.2 mm to the 'Z' dimension. For further information, please reference document IPC-7351A, Naming Convention for Standard SMT Land Patterns, and for International grid details, please see document IEC, Publication 97.

Note: For high voltage applications, the appropriate industry sector guidelines should be considered with regards to creepage and clearance distances between device Terminals and PCB tracking.