

LT1189

Low Power Video Difference Amplifier

- Differential or Single-Ended Gain Block (Adjustable)
- -3 dB Bandwidth, A_V = ± 10 35MHz
■ Slew Rate 220V/µs
- \blacksquare Slew Rate
- Low Supply Current 13mA
- Output Current $±20mA$
- CMRR at 10MHz 48dB
- LT1193 Pin Out
- Low Cost
- Single 5V Operation
- Drives Cables Directly
- Output Shutdown

U A S O PPLICATI

- Line Receivers
- Video Signal Processing
- Cable Drivers
- Tape and Disc Drive Systems

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The LT1189 is a difference amplifier optimized for operation on $\pm 5V$, or a single 5V supply, and gain ≥ 10 . This versatile amplifier features uncommitted high input impedance (+) and (–) inputs, and can be used in differential or single-ended configurations. Additionally, a second set of inputs give gain adjustment and DC control to the difference amplifier.

The LT1189's high slew rate, $220V/\mu s$, wide bandwidth, 35MHz, and ± 20 mA output current require only 13mA of supply current. The shutdown feature reduces the power dissipation to a mere 15mW, and allows multiple amplifiers to drive the same cable.

The LT1189 is a low power, gain of 10 stable version of the popular LT1193, and is available in 8-pin miniDIPs and SO packages. For lower gain applications see the LT1187 data sheet.

TYPICAL APPLICATION

Cable Sense Amplifier for Loop Through Connections Closed-Loop Gain vs Frequency with DC Adjust

ABSOLUTE MAXIMUM RATING

PACKAGE/ORDER INFORMATION

\pm **5V ELECTRICAL CHARACTERISTICS T_A** = 25°C, (Note 3)

+–5V ELECTRICAL C C HARA TERISTICS TA = 25°**C, (Note 3)**

VS = ±**5V, VREF = 0V, RFB1 = 900**Ω **from pins 6 to 8, RFB2 = 100**Ω **from pin 8 to ground, RL = RFB1 + RFB2 = 1k, CL** ≤ **10pF, pin 5 open.**

5V ELECTRICAL CHARACTERISTICS TA = 25°C, (Note 3)

VS + = 5V, VS – = 0V, VREF = 2.5V, RFB1 = 900Ω **from pins 6 to 8, RFB2 = 100**Ω **from pin 8 to VREF, RL = RFB1 + RFB2 = 1k, CL** ≤ **10pF, pin 5**

±5V €LECTRICAL CHARACTERISTICS -55° C ≤ TA ≤ 125°C, (Note 3)

VS = ±**5V, VREF = 0V, RFB1 = 900**Ω **from pins 6 to 8, RFB2 = 100**Ω **from pin 8 to ground, RL = RFB1 + RFB2 = 1k, CL** ≤ **10pF, pin 5 open.**

± 5 V ELECTRICAL CHARACTERISTICS 0° C \leq T_A \leq 70°C, (Note 3)
V_S = ±5V, V_{REF} = 0V, R_{FB1} = 900Ω from pins 6 to 8, R_{FB2} = 100Ω from pin 8 to ground, R_L = R_{FB1} + R_{FB2} = 1k, C_L \leq 10pF, pin 5 op

5V ELECTRICAL CHARACTERISTICS 0°C ≤ TA ≤ 70°C, (Note 3)

VS + = +5V, VS – = 0V, VREF = 2.5V, RFB1 = 900Ω **from pins 6 to 8, RFB2 = 100**Ω **from pin 8 to VREF, RL = RFB1 + RFB2 = 1k, CL** ≤ **10pF, pin 5**

Note 1: A heat sink may be required to keep the junction temperature below absolute maximum when the output is shorted continuously.

Note 2: T_J is calculated from the ambient temperature T_A and power dissipation P_D according to the following formulas:

Note 3: When R_L = 1k is specified, the load resistor is R_{FB1} + R_{FB2} , but when $R_l = 300\Omega$ is specified, then an additional 430 Ω is added to the output such that (R_{FB1} + R_{FB2}) in parallel with 430 Ω is R_L = 300 Ω .

Note 4: V_{OS} measured at the output (pin 6) is the contribution from both input pair, and is input referred.

Note 5: $V_{IN \text{LIM}}$ is the maximum voltage between $-V_{IN}$ and $+V_{IN}$ (pin 2 and pin 3) for which the output can respond.

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Note 6: Slew rate is measured between \pm 1V on the output, with a V_{IN} step of $\pm 0.5V$, A_V = 10 and R_L = 1k.

Note 7: Full power bandwidth is calculated from the slew rate measurement: $FPBW = SR/2\pi Vp$.

Note 8: Settling time measurement techniques are shown in "Take the Guesswork Out of Settling Time Measurements," EDN, September 19, 1985. **Note 9**: NTSC (3.58MHz).

Note 10: AC parameters are 100% tested on the ceramic and plastic DIP packaged parts (J8 and N8 suffix) and are sample tested on every lot of the SO packaged parts (S8 suffix).

Note 11: See Application section for shutdown at elevated temperatures. Do not operate shutdown above $T_J > 125$ °C.

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Shutdown Supply Current vs

Equivalent Input Noise Voltage vs

Frequency **Example 20**

Frequency **Example 20**

Frequency

Supply Current vs Supply Voltage

Temperature Gain Error vs Temperature Open-Loop Gain vs Temperature

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TEMPERATURE (°C)

–25 0 25 50 75 100 125

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 V^- 0

–50

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±SUPPLY VOLTAGE (V)

0 2 4 6 10 8

FREQUENCY (Hz)

100k

1k 100k 10M 100M

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Output Voltage Step vs Settling Time, $A_V = 10$

Large-Signal Transient Reponse

Harmonic Distortion vs Output Level

Small-Signal Transient Reponse

 $A_V = 10$, $R_L = 1k$, $t_r = 9.40$ ns

 Δ \mathcal{T} LINEAR

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The primary use of the LT1189 is in converting high speed differential signals to a single-ended output. The LT1189 video difference amplifier has two uncommitted high input impedance $(+)$ and $(-)$ inputs. The amplifier has another set of inputs which can be used for reference and feedback. Additionally, this set of inputs give gain adjust, and DC control to the differential amplifier. The voltage gain of the LT1189 is set like a conventional operational amplifier. Feedback is applied to pin 8, and it is optimized for gains of 10 or greater. The amplifier can be operated singleended by connecting either the $(+)$ or $(-)$ inputs to the +/REF (pin 1). The voltage gain is set by the resistors: $(R_{FB} + R_G)/R_G$.

Like the single-ended case, the differential voltage gain is set by the external resistors: $(R_{FB} + R_G)/R_G$. The maximum input differential signal for which the output will respond is approximately ±170mV.

Power Supply Bypassing

The LT1189 is quite tolerant of power supply bypassing. In some applications a 0.1µF ceramic disc capacitor placed 1/2 inch from the amplifier is all that is required. In applications requiring good settling time, it is important to use multiple bypass capacitors. A 0.1µF ceramic disc in parallel with a 4.7µF tantalum is recommended.

Calculating the Output Offset Voltage

Both input stages contribute to the output offset voltage at pin 6. The feedback correction forces balance in the input stages by introducing an Input V_{OS} at pin 8. The complete expression for the output offset voltage is:

$$
V_{\text{OUT}} = (V_{\text{OS}} + I_{\text{OS}}(R_{\text{S}}) + I_{\text{B}}(R_{\text{REF}})) \times (R_{\text{FB}} + R_{\text{G}})/R_{\text{G}} + I_{\text{B}}(R_{\text{FB}})
$$

 R_S represents the input source resistance, typically 75 Ω , and R_{REF} represents finite source impedance from the DC reference voltage, for V_{RFF} grounded, R_{RFF} = 0Ω the I_{OS} is normally a small contributor and the expression simplifies to:

$$
\mathrm{V_{OUT}} = \mathrm{V_{OS}}(\mathrm{R_{FB}} + \mathrm{R_G})/\mathrm{R_G} + \mathrm{I_B}(\mathrm{R_{FB}})
$$

If R_{FB} is limited to 1k, the last term of the equation contributes only 2mV since I_B is less than 2 μ A.

Figure 1. Simplified Input Stage Schematic

Instrumentation Amplifier Rejects High Voltage

Instrumentation amplifiers are often used to process slowly varying outputs from transducers. With the LT1189 it is easy to make an instrumentation amplifier that can respond to rapidly varying signals. Attenuation resistors in front of the LT1189 allow very large common-mode signals to be rejected while maintaining good frequency response. The input common-mode and differential-mode signals are reduced by 100:1, while the closed-loop gain is set to be 100, thereby maintaining unity-gain input to output. The unique topology allows for frequency response boost by adding 150pF to pin 8 as shown.

3.5MHz Instrumentation Amplifier Rejects 120VP-P

Output of Instrumentation Amplifier with 1MHz Square Wave Riding on 120V_{P-P} at the Input

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High Voltage Instrumentation Amplifier Response

Operating with Low Closed-Loop Gain

The LT1189 has been optimized for closed-loop gains of 10 or greater. The amplifier can be operated at much lower closed-loop gains with the aid of a capacitor C_{FB} across the feedback resistor, (feedback zero). This capacitor lowers the closed-loop 3dB bandwidth. The bandwidth cannot be made arbitrarily low because C_{FB} is a short at high frequency and the amplifier will appear configured unity-gain. As an approximate guideline, make BW \times A_{VCL} = 200MHz. This expression expands to:

$$
\frac{A_{\text{VCL}}}{2\pi(R_{\text{FB}})(C_{\text{FB}})} = 200 \text{MHz}
$$

or:

$$
C_{FB} = \frac{A_{VCL}}{(200MHz)(2\pi)(R_{FB})}
$$

The effect of the feedback zero on the transient and frequency response is shown for $A_V = 4$.

Closed-Loop Voltage Gain vs Frequency

Small-Signal Transient Response

 $A_V = 4$, $R_{FB} = 910Ω$, $R_G = 300Ω$

Small-Signal Transient Response

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 $A_V = 4$, $R_{FB} = 910Ω$, $R_G = 300Ω$, CFB = 5pF

Reducing the Closed-Loop Bandwidth

Although it is possible to reduce the closed-loop bandwidth by using a feedback zero, instability can occur if the bandwidth is made too low. An alternate technique is to do differential filtering at the input of the amplifier. This technique filters the differential input signal, and the differential noise, but does not filter common-mode noise. Common-mode noise is rejected by the LT1189's CMRR.

Using the Shutdown Feature

The LT1189 has a unique feature that allows the amplifier to be shutdown for conserving power, or for multiplexing several amplifiers onto a common cable. The amplifier will shutdown by taking pin 5 to V^- . In shutdown, the amplifier dissipates 15mW while maintaining a true high impedance output state of about 20kΩ in parallel with the feedback resistors. For MUX applications, the amplifiers may be configured inverting, non-inverting, or differential. When the output is loaded with as little as $1k\Omega$ from the amplifier's feedback resistors, the amplifier shuts off in 600ns. This shutoff can be under the control of HC CMOS operating between 0V and – 5V.

1MHz Sine Wave Gated Off with Shutdown Pin

The ability to maintain shutoff is shown on the curve Shut down Supply Current vs Temperature in the Typical Performance Characteristics section. At very high elevated temperature it is important to hold the shutdown pin close to the negative supply to keep the supply current from increasing.

TYPICAL APPLICATION

Differential Receiver MUX for Power Down Applications

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