

LT1469

Dual 90MHz, 22V/µs 16-Bit Accurate Operational Amplifier

### FEATURES

- <sup>n</sup> **90MHz Gain Bandwidth, f = 100kHz**
- Maximum Input Offset Voltage: 125µV
- **n** Settling Time: 900ns ( $A_V = -1$ , 150µV, 10V Step)
- 22V/µs Slew Rate
- **DEDUCA** Low Distortion:  $-96.5dB$  for 100kHz, 10V<sub>P-P</sub>
- Maximum Input Offset Voltage Drift: 3µV/°C
- Maximum Inverting Input Bias Current: 10nA
- Minimum DC Gain: 300V/mV
- $\blacksquare$  Minimum Output Swing into 2k:  $\pm$ 12.8V
- Unity-Gain Stable
- Input Noise Voltage: 5nV/ $\sqrt{Hz}$
- Input Noise Current: 0.6pA/ $\sqrt{Hz}$
- Total Input Noise Optimized for  $1kΩ < R<sub>S</sub> < 20kΩ$
- Specified at  $\pm$ 5V and  $\pm$ 15V Supplies

## **APPLICATIONS**

- **Precision Instrumentation**
- High Accuracy Data Acquisition Systems
- 16-Bit DAC Current-to-Voltage Converter
- ADC Buffer
- **E** Low Distortion Active Filters
- Photodiode Amplifiers

# **DESCRIPTION**

The LT®1469 is a dual, precision high speed operational amplifier with 16-bit accuracy and 900ns settling to 150µV for 10V steps. This unique blend of precision and AC performance makes the LT1469 the optimum choice for high accuracy applications such as DAC current-to-voltage conversion and ADC buffers. The initial accuracy and drift characteristics of the input offset voltage and inverting input bias current are tailored for inverting applications.

The 90MHz gain bandwidth ensures high open-loop gain at frequency for reducing distortion. In noninverting applications such as an ADC buffer, the low distortion and DC accuracy allow full 16-bit AC and DC performance.

The 22V/µs slew rate of the LT1469 improves large signal performance compared to other precision op amps in applications such as active filters and instrumentation amplifiers.

The LT1469 is available in a space saving 4mm  $\times$  4mm leadless package, as well as in small outline and DIP packages. A single version, the LT1468, is also available.

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## TYPICAL APPLICATION



#### **16-Bit DAC I-to-V Converter and Reference Inverter for Bipolar Output Swing (** $V_{\text{OUT}} = -10V$  **to 10V)**



1469fb

# ABSOLUTE MAXIMUM RATINGS **(Note 1)**

Total Supply Voltage (V+ to V–).................................36V Input Current (Note 2)..±10mA Output Short-Circuit Duration (Note 3)............ Indefinite Operating Temperature Range (Note 4).... –40°C to 85°C



# PIN CONFIGURATION



# ORDER INFORMATION



Consult LTC Marketing for parts specified with wider operating temperature ranges. \*The temperature grade is identified by a label on the shipping container. For more information on lead free part marking, go to: http://www.linear.com/leadfree/

For more information on tape and reel specifications, go to: http://www.linear.com/tapeandreel/



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#### The  $\bullet$  denotes the specifications which apply over the full operating temperature range,  $0^{\circ}C \leq T_A \leq 70^{\circ}C$ . V<sub>CM</sub> = 0V unless otherwise noted.





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temperature range, 0°C ≤ T<sub>A</sub> ≤ 70°C. V<sub>CM</sub> = 0V unless otherwise noted.





### **ELECTRICAL CHARACTERISTICS** The  $\bullet$  denotes the specifications which apply over the full operating

temperature range, −40°C ≤ T<sub>A</sub> ≤ 85°C, V<sub>CM</sub> = 0V unless otherwise noted. (Note 5)



**Note 1:** Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

**Note 2:** The inputs are protected by back-to-back diodes and two 100Ω series resistors. If the differential input voltage exceeds 0.7V, the input current should be limited to less than 10mA. Input voltages outside the supplies will be clamped by ESD protection devices and input currents should also be limited to less than 10mA.

**Note 3:** A heat sink may be required to keep the junction temperature below absolute maximum when the output is shorted indefinitely.

**Note 4:** The LT1469C and LT1469I are guaranteed functional over the operating temperature range of –40°C to 85°C.

**Note 5:** The LT1469C is guaranteed to meet specified performance from 0°C to 70°C and is designed, characterized and expected to meet specified performance from –40°C to 85°C but is not tested or QA sampled at these temperatures. The LT1469I is guaranteed to meet specified performance from –40°C to 85°C.

**Note 6:** Slew rate is measured between ±8V on the output with ±12V swing for  $\pm$ 15V supplies and  $\pm$ 2V on the output with  $\pm$ 3V swing for  $\pm$ 5V supplies.

**Note 7:** Full-power bandwidth is calculated from the slew rate. FPBW =  $SR/2\pi V_P$ .

**Note 8:** This parameter is not 100% tested.

**Note 9:** ∆CMRR and ∆PSRR are defined as follows: 1) CMRR and PSRR are measured in µV/V on each amplifier; 2) the difference between the two sides is calculated in  $\mu$ V/V; 3) the result is converted to dB.













1469 G25

**TLINEAR** 



1469 G26

1469 G27











**Large-Signal Transient, AV = 1 Large-Signal Transient, AV = –1**





## APPLICATIONS INFORMATION

#### **Layout and Passive Components**

The LT1469 requires attention to detail in board layout in order to maximize DC and AC performance. For best AC results (for example, fast settling time) use a ground plane, short lead lengths and RF quality bypass capacitors (0.01µF to 0.1µF) in parallel with low ESR bypass capacitors (1µF to 10µF tantalum). For best DC performance, use "star" grounding techniques, equalize input trace lengths and minimize leakage (e.g., 1.5G $\Omega$  of leakage between an input and a 15V supply will generate 10nA—equal to the maximum  $I_B$ – specification).

Board leakage can be minimized by encircling the input circuitry with a guard ring operated at a potential close to that of the inputs: for inverting configurations tie the ring to ground, in noninverting connections tie the ring to the inverting input (note the input capacitance will increase which may require a compensating capacitor as discussed below).

Microvolt level error voltages can also be generated in the external circuitry. Thermocouple effects caused by temperature gradients across dissimilar metals at the contacts to the inputs can exceed the inherent drift of



# APPLICATIONS INFORMATION

the amplifier. Air currents over device leads should be minimized, package leads should be short and the two input leads should be as close together as possible and maintained at the same temperature.

The parallel combination of the feedback resistor and gain setting resistor on the inverting input can combine with the input capacitance to form a pole which can cause peaking or even oscillations. For feedback resistors greater than 2k, a feedback capacitor of value  $C_F > R_G \cdot C_{IN}/R_F$  should be used to cancel the input pole and optimize dynamic performance. For applications where the DC noise gain is one, and a large feedback resistor is used,  $C_F$  should be greater than or equal to  $C_{IN}$ . An example would be a DAC I-to-V converter as shown on the front page of the data sheet where the DAC can have many tens of picofarads of output capacitance. Another example would be a gain of –1 with 5k resistors; a 5pF to 10pF capacitor should be added across the feedback resistor.

#### **Input Considerations**

Each input of the LT1469 is protected with a 100 $\Omega$  series resistor and back-to-back diodes across the bases of the input devices. If large differential input voltages are anticipated, limit the input current to less than 10mA with an external series resistor. Each input also has two ESD clamp diodes—one to each supply. If an input is driven beyond the supply, limit the current with an external resistor to less than 10mA.



**Figure 1. Nulling Input Capacitance**

The LT1469 employs bias current cancellation at the inputs. The inverting input current is trimmed at zero common mode voltage to minimize errors in inverting applications such as I-to-V converters. The noninverting input current is not trimmed and has a wider variation and therefore a larger maximum value. As the input offset current can be greater than either input current, the use of balanced source resistance is NOT recommended as it actually degrades DC accuracy and also increases noise.

The input bias currents vary with common mode voltage. The cancellation circuitry was not designed to track this common mode voltage because the settling time would have been adversely affected.

The LT1469 inputs can be driven to the negative supply and to within 0.5V of the positive supply without phase reversal. As the input moves closer than 0.5V to the positive supply, the output reverses phase.

#### **Total Input Noise**

The total input noise of the LT1469 is optimized for a source resistance between 1k and 20k. Within this range, the total input noise is dominated by the noise of the source resistance itself. When the source resistance is below 1k, voltage noise of the amplifier dominates. When the source resistance is above 20k, the input noise current is the dominant contributor.



**Figure 2. Input Stage Protection**



## APPLICATIONS INFORMATION

#### **Capacitive Loading**

The LT1469 drives capacitive loads of up to 100pF in unitygain and 300pF in a gain of –1. When there is a need to drive a larger capacitive load, a small series resistor should be inserted between the output and the load. In addition, a capacitor should be added between the output and the inverting input as shown in Figure 3.

#### **Settling Time**

The LT1469 is a single stage amplifier with an optimal thermal layout that leads to outstanding settling performance. Measuring settling even at the 12-bit level is very challenging, and at the 16-bit level requires a great deal of subtlety and expertise. Fortunately, there are two excellent Linear Technology reference sources for settling

measurements—Application Notes 47 and 74. Appendix B of AN47 is a vital primer on 12-bit settling measurements and AN74 extends the state-of-the-art while concentrating on settling time with a 16-bit current output DAC input.

The settling of the DAC I-to-V converter on the front page was measured using the exact methods of AN74. The optimum nulling of the DAC output capacitance requires 15pF across the 12k feedback resistor. The theoretical limit for 16-bit settling is 11.1 times this RC time constant or 2µs. The actual settling time is 2.4µs at the output of the LT1469.

The RC output noise filter adds a slight settling time delay but reduces the noise bandwidth to 1.6MHz which increases the output resolution for 16-bit accuracy.



**Figure 3. Driving Capacitive Loads**

## TYPICAL APPLICATIONS

#### **Ultralow Distortion Balanced Audio Line Driver**





\*1dBu = 1 milliwatt into 600 $\Omega$ 



1469 TA02

### TYPICAL APPLICATIONS

**Extending 16-Bit DAC Performance to 200V Output Swing**



## SIMPLIFIED SCHEMATIC





### PACKAGE DESCRIPTION



**DF Package 12-Lead Plastic DFN (4mm** × **4mm)** (Reference LTC DWG # 05-08-1733 Rev Ø)



### PACKAGE DESCRIPTION



**N8 Package**

NOTE.<br>1. DIMENSIONS ARE <mark>MILLIMETERS</mark><br>\*THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS.

MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED .010 INCH (0.254mm)

**S8 Package 8-Lead Plastic Small Outline (Narrow 0.150)**

(Reference LTC DWG # 05-08-1610)



(MILLIMETERS) 2. DRAWING NOT TO SCALE

3. THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS. MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED .006" (0.15mm)

SO8 0303





#### REVISION HISTORY **(Revision history begins at Rev B)**



