

- **Optimized Image Rejection for 850MHz to 965MHz**
- **High OIP3: +22.9dBm at 900MHz**
- **Low Output Noise Floor at 5MHz Offset:**
	- **No RF: –159.4dBm/Hz**
	- **POUT = 4dBm: –153dBm/Hz**
- **Integrated LO Buffer and LO Quadrature Phase Generator**
- **50**Ω **AC-Coupled Single-Ended LO and RF Ports**
- **50**Ω **DC Interface to Baseband Inputs**
- **Low Carrier Leakage: –43dBm at 900MHz**
- **High Image Rejection: –52dBc at 900MHz**
- 16-Lead 4mm \times 4mm QFN Package

APPLICATIONS

- Infrastructure Tx for GSM/Cellular Bands
- Image Reject Up-Converters for Cellular Bands
- Low-Noise Variable Phase-Shifter for 700MHz to 1050MHz Local Oscillator Signals
- RFID Reader

TYPICAL APPLICATIO U

GSM/EDGE Optimized, High Linearity Direct Quadrature Modulator **FEATURES DESCRIPTIO ^U**

The LT®5568-2 is a direct I/Q modulator designed for high performance wireless applications, including wireless infrastructure. It allows direct modulation of an RF signal using differential baseband I and Q signals. It supports GSM, EDGE, CDMA, CDMA2000 and other systems that operate in the 850MHz to 965MHz band. It may be configured as an image reject upconverting mixer, by applying 90° phase-shifted signals to the I and Q inputs. The I/Q baseband inputs consist of voltage-to-current converters that in turn drive double-balanced mixers. The outputs of these mixers are summed and applied to an on-chip RF transformer, which converts the differential mixer signals to a 50Ω single-ended output. The four balanced I and Q baseband input ports are intended for DC coupling from a source with a common mode voltage level of about 0.5V. The LO path consists of an LO buffer with single-ended input, and precision quadrature generators that produce the LO drive for the mixers. The supply voltage range is 4.5V to 5.25V.

 $\mathcal{I}\mathcal{I}$, LT, LTC and LTM are registered trademarks of Linear Technology Corporation. All other trademarks are the property of their respective owners.

850MHz to 965MHz Direct Conversion Transmitter Application

GSM EVM and Noise vs RF Output Power at 900MHz

1

ABSOLUTE MAXIMUM RATINGS

CAUTION: This part is sensitive to ESD. It is very important that proper ESD precautions be observed when handling the LT5568-2.

ORDER INFORMATION

Consult LTC Marketing for parts specified with wider operating temperature ranges.

Consult LTC Marketing for information on non-standard lead based finish parts.

For more information on lead free part marking, go to:<http://www.linear.com/leadfree/> For more information on tape and reel specifications, go to:<http://www.linear.com/tapeandreel/>

CLCL I ISILITE LATITISITE I CISID I ILD V_{CC} = 5V, EN = High, T_A = 25°C, f_{LO} = 900MHz, f_{RF} = 902MHz, P_{LO} = 0dBm. **ELECTRICAL CHARACTERISTICS**

BBPI, BBMI, BBPQ, BBMQ inputs 0.54V_{DC}, Baseband Input Frequency = 2MHz, I&Q 90° shifted (upper side-band selection). **PRF, OUT = –10dBm, unless otherwise noted. (Note 3)**

PIN CONFIGURATION

ELEL I RILITL LATITISITL I EISID I ILD V_{CC} = 5V, EN = High, T_A = 25°C, f_{LO} = 900MHz, f_{RF} = 902MHz, P_{LO} = 0dBm. **ELECTRICAL CHARACTERISTICS**

BBPI, BBMI, BBPQ, BBMQ inputs 0.54V_{DC}, Baseband Input Frequency = 2MHz, I&Q 90° shifted (upper side-band selection). P_{DE} $_{\text{OUT}}$ = -10 dBm, unless otherwise noted. (Note 3)

 $EN = Low$
 $EN = OV$

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

Note 2: Specifications over the -40° C to 85°C temperature range are assured by design, characterization and correlation with statistical process controls.

Note 3: Tests are performed as shown in the configuration of Figure 7. **Note 4:** On each of the four baseband inputs BBPI, BBMI, BBPQ and BBMQ.

Note 5: $V(BBPI) - V(BBMI) = 1V_{DC}$, $V(BBPQ) - V(BBMQ) = 1V_{DC}$.

Note 6: Maximum value within 850MHz to 965MHz.

Input Low Current

Sleep | Input Low Voltage

Note 7: An external coupling capacitor is used in the RF output line.

Note 8: At 20MHz offset from the LO signal frequency.

Note 9: At 20MHz offset from the CW signal frequency.

Note 10: At 5MHz offset from the CW signal frequency.

Note 11: RF power is within 10% of final value.

 $EN = OV$ 0.01

Note 12: RF power is at least 30dB lower than in the ON state.

Note 13: Baseband is driven by 2MHz and 2.1MHz tones. Drive level is set in such a way that the two resulting RF tones are –10dBm each.

Note 14: IM2 measured at LO frequency + 4.1MHz.

Note 15: IM3 measured at LO frequency + 1.9MHz and LO frequency + 2.2MHz. **Note 16:** Amplitude average of the characterization data set without image or LO feedthrough nulling (unadjusted).

Note 17: The difference in conversion gain between the spurious signal at $f = 3 \cdot LO - BB$ versus the conversion gain at the desired signal at $f = LO +$ BB for BB = 2MHz and LO = 900MHz.

Note 18: The input voltage corresponding to the output P1dB.

55682

 0.5 V

µA

4

TYPICAL PERFOR A CE CHARACTERISTICS U W

V_{CC} = 5V, EN = High, T_A = 25°C, f_{LO} = 900MHz, P_{LO} = 0dBm. BBPI, BBMI, BBPQ, BBMQ inputs 0.54V_{DC}, Baseband Input Frequency f_{BB} = 2MHz, I&Q 90° shifted. f_{RF} = f_{BB} + f_{LO} (upper **sideband selection). PRF, OUT = –10dBm (–10dBm/tone for 2-tone measurements), unless otherwise noted. (Note 3)**

TYPICAL PERFORMANCE CHARACTERISTICS $V_{CC} = 5V$, EN = High, TA = 25°C, f_{LO} = 900MHz,

P_{LO} = 0dBm. BBPI, BBMI, BBPQ, BBMQ inputs 0.54V_{DC}, Baseband Input Frequency f_{BB} = 2MHz, I&Q 90° shifted. f_{RF} = f_{BB} + f_{LO} (upper **sideband selection). PRF, OUT = –10dBm (–10dBm/tone for 2-tone measurements), unless otherwise noted. (Note 3)**

TYPICAL PERFORMANCE CHARACTERISTICS $V_{CC} = 5V$, EN = High, TA = 25°C, f_{LO} = 900MHz,

P_{LO} = 0dBm. BBPI, BBMI, BBPQ, BBMQ inputs 0.54V_{DC}, Baseband Input Frequency f_{BB} = 2MHz, I&Q 90° shifted. f_{RF} = f_{BB} + f_{LO} (upper **sideband selection). PRF, OUT = –10dBm (–10dBm/tone for 2-tone measurements), unless otherwise noted. (Note 3)**

RF Two-Tone Power (Each Tone), IM2 and IM3 vs Baseband Voltage and Supply Voltage

RF Two-Tone Power (Each Tone), IM2 and IM3 vs Baseband Voltage and Temperature

Gain Distribution 25 ė -40° C \Box 25°C \blacksquare 85 \circ C 20 PERCENTAGE (%) PERCENTAGE (%) 15 10 5 θ -8.5 -8 -7.5 -7 -6.5 -6 -5.5 –9 –7.5 GAIN (dB)

Noise Floor Distribution

LO Leakage Distribution and Community Com

55682 G23

PIN FUNCTIONS

EN (Pin 1): Enable Input. When the enable pin voltage is higher than 1V, the IC is turned on. When the input voltage is less than 0.5V, the IC is turned off.

GND (Pins 2, 4, 6, 9, 10, 12, 15): Ground. Pins 6, 9, 15 and 17 (exposed pad) are connected to each other internally. Pins 2 and 4 are connected to each other internally and function as the ground return for the LO signal. Pins 10 and 12 are connected to each other internally and function as the ground return for the on-chip RF balun. For best RF performance, pins 2, 4, 6, 9, 10, 12, 15 and the Exposed Pad 17 should be connected to the printed circuit board ground plane.

LO (Pin 3): LO Input. The LO input is an AC-coupled singleended input with approximately 50Ω input impedance at RF frequencies. Externally applied DC voltage should be within the range $-0.5V$ to V_{CC} + 0.5V in order to avoid turning on ESD protection diodes.

BBPQ, BBMQ (Pins 7, 5): Baseband Inputs for the Q-channel, each 50Ω input impedance. Internally biased at about 0.54V. Applied voltage must stay below 2.5V.

V_{CC} (Pins 8, 13): Power Supply. Pins 8 and 13 are connected to each other internally. It is recommended to use 0.1µF capacitors for decoupling to ground on each of these pins.

RF (Pin 11): RF Output. The RF output is an AC-coupled single-ended output with approximately 50Ω output impedance at RF frequencies. Externally applied DC voltage should be within the range $-0.5V$ to V_{CC} + 0.5V in order to avoid turning on ESD protection diodes.

BBPI, BBMI (Pins 14, 16): Baseband Inputs for the I-channel, each with 50Ω input impedance. Internally biased at about 0.54V. Applied voltage must stay below 2.5V.

Exposed Pad (Pin 17): Ground. This pin must be soldered to the printed circuit board ground plane.

7

BLOCK DIAGRAM

APPLICATIONS INFORMATION

The LT5568-2 consists of I and Q input differential voltage-to-current converters, I and Q up-conversion mixers, an RF output balun, an LO quadrature phase generator and LO buffers.

Figure 1. Simplified Circuit Schematic of the LT5568-2 (Only I-Half is Drawn)

External I and Q baseband signals are applied to the differential baseband input pins, BBPI, BBMI, and BBPQ, BBMQ. These voltage signals are converted to currents and translated to RF frequency by means of double-balanced up-converting mixers. The mixer outputs are combined in an RF output balun, which also transforms the output impedance to 50 Ω . The center frequency of the resulting RF signal is equal to the LO signal frequency. The LO input drives a phase shifter which splits the LO signal into inphase and quadrature LO signals. These LO signals are then applied to on-chip buffers which drive the up-conversion mixers. Both the LO input and RF output are single-ended, 50Ω-matched and AC coupled.

Baseband Interface

The baseband inputs (BBPI, BBMI), (BBPQ, BBMQ) present a differential input impedance of about 100Ω. At each of the four baseband inputs, a first-order lowpass filter using 25Ω

APPLICATIO S I FOR ATIO U W U U

and 12pF to ground is incorporated (see Figure 1), which limits the baseband bandwidth to approximately 330MHz (–1dB point). The common mode voltage is about 0.54V and is approximately constant over temperature.

It is important that the applied common mode voltage level of the I and Q inputs is about 0.54V in order to properly bias the LT5568-2. Some I/Q test generators allow setting the common mode voltage independently. In this case, the common mode voltage of those generators must be set to 0.27V to match the LT5568-2 internal bias, because for DC signals, there is no –6dB source-load voltage division (see Figure 2).

Figure 2. DC Voltage Levels for a Generator Programmed at 0.27V_{DC} for a 50Ω Load and the LT5568-2 as a Load

The baseband inputs should be driven differentially; otherwise, the even-order distortion products will degrade the overall linearity severely. Typically, a DAC will be the signal source for the LT5568-2. Reconstruction filters should be placed between the DAC output and the LT5568-2's baseband inputs. In Figure 3, a typical baseband interface schematic for GSM is drawn. It shows a ground referenced DAC output interface followed by a 3rd order active OpAmp RC lowpass filter with a 400kHz cutoff frequency (-3dB). The DAC in this example sources a current from 0mA to 20mA, with a voltage compliance range of at least 0V to 1V. This interface is DC coupled, which allows adjustment of the DAC's differential output current to minimize the LO feedthrough. The voltage swing at the LT5568-2 baseband inputs is about $2V_{\text{P-DIFF}}$, which results in a 1.2dBm GSM RF output power at 900MHz with noise floor of –154.3dBm/Hz at 6MHz offset (= –104.3dBm/100kHz). The RMS EVM is about 0.6%. The LT1819, which houses two LT1818s, can be used instead of U2 and U3. The total current in the positive supply is about 157mA and the current in the negative supply is about 40mA.

Figure 3. LT5568-2 GSM Baseband Interface with 3rd Order Lowpass Filter and Ground Referenced DAC (Only I-Channel is Shown)

LO Section

The internal LO input amplifier performs single-ended to differential conversion of the LO input signal. Figure 4 shows the equivalent circuit schematic of the LO input.

Figure 4. Equivalent Circuit Schematic of the LO Input

The internal, differential LO signal is then split into in-phase and quadrature (90° phase shifted) signals that drive LO buffer sections. These buffers drive the double balanced I and Q mixers. The phase relationship between the LO input and the internal in-phase LO and quadrature LO signals is fixed, and is independent of start-up conditions. The internal phase shifters are designed to deliver accurate quadrature signals. For LO frequencies significantly below 650MHz or above 1.25GHz, however, the quadrature accuracy will diminish, causing the image rejection to degrade. The LO pin input impedance is about 50Ω , and the recommended LO input power is 0dBm. For lower LO input power, the gain, OIP2, OIP3 and noise floor at P_{BF} = 4dBm will degrade, especially for P_{LO} below –2dBm and at $T_A = 85^{\circ}$ C. For high LO input power (e.g., +5dBm), the image rejection will degrade with no improvement in linearity or gain. Harmonics present on the LO signal can degrade the image rejection because they can introduce a small excess phase shift in the internal phase splitter. For the second (at 1.8GHz) and third harmonics (at 2.7GHz) at –20dBc, the resulting signal at the image frequency is about –61dBc or lower, corresponding to an excess phase shift of much less than 1 degree. For the second and third LO harmonics at -10 dBc, the introduced signal at the image frequency is about –51dBc. Higher harmonics than the third will have less impact. The LO return loss typically will be better than 11dB over the 700MHz to 1.05GHz range. Table 1 shows the LO port input impedance vs frequency.

Table 1. LO Port Input Impedance vs Frequency for EN = High and $P_{10} = 0$ dBm

Frequency	Input Impedance	S_{11}	
MHz	Ω	Mag	Angle
500	$47.5 + j12.1$	0.126	95.0
600	$59.4 + j8.4$	0.115	37.8
700	$66.2 - j1.14$	0.140	-3.41
800	$67.2 - 13.4$	0.185	-31.7
900	$61.1 - j23.9$	0.232	-53.2
1000	$53.3 - j26.8$	0.252	-68.7
1100	$48.2 - j26.1$	0.258	-79.4
1200	$42.0 - j27.4$	0.297	-90.0

If the part is in shutdown mode, the input impedance of the LO port will be different. The LO input impedance for EN = Low is given in Table 2.

RF Section

After up-conversion, the RF outputs of the I and Q mixers are combined. An on-chip balun performs internal differential to single-ended output conversion, while transforming the output signal impedance to 50Ω. Table 3 shows the RF port output impedance vs frequency.

Table 3. RF Port Output Impedance vs Frequency for EN = High and $P_{L0} = 0$ dBm

Frequency	Input Impedance	S_{22}	
MHz	Ω	Mag	Angle
500	$22.0 + j5.7$	0.395	164.2
600	$28.2 + j12.5$	0.317	141.3
700	$38.8 + j14.8$	0.206	117.5
800	$49.4 + j7.2$	0.072	90.6
900	$49.3 - j5.1$	0.051	-94.7
1000	$42.5 - j11.1$	0.143	-117.0
1100	$36.7 - j11.7$	0.202	-130.7
1200	$33.0 - j10.3$	0.238	-141.6

10

The RF output S_{22} with no LO power applied is given in Table 4.

Table 4. RF Port Output Impedance vs Frequency for EN = High and No LO Power Applied

Frequency	Input Impedance	S_{22}	
MHz	Ω	Mag	Angle
500	$22.7 + 15.6$	0.381	164.0
600	$29.7 + j11.6$	0.290	142.0
700	$40.5 + j11.6$	0.164	121.9
800	$47.3 + j2.2$	0.037	139.6
900	$44.1 - j6.7$	0.094	-126.9
1000	$38.2 - j9.8$	0.171	-133.9
1100	$34.0 - j9.4$	0.218	-143.1
1200	$31.5 - j7.8$	0.245	-151.6

For $EN = Low$ the S₂₂ is given in Table 5.

Table 5. RF Port Output Impedance vs Frequency for EN = Low

Frequency	Input Impedance	S_{22}	
MHz	Ω	Maq	Angle
500	$21.2 + j5.4$	0.409	164.9
600	$26.6 + j12.5$	0.340	142.5
700	$36.6 + j16.6$	0.241	118.1
800	$49.2 + j11.6$	0.116	87.4
900	$52.9 - j2.0$	0.034	-33.1
1000	$46.4 - j11.2$	0.121	-101.1
1100	$39.3 - j13.2$	0.188	-120.6
1200	$34.4 - j12.1$	0.231	-133.8

Figure 5. Equivalent Circuit Schematic of the RF Output Figure 6. EN Pin Interface

Note that an ESD diode is connected internally from the RF output to ground (see Figure 5). For strong output RF signal levels (higher than 3dBm), this ESD diode can degrade the linearity performance if the 50Ω termination impedance is connected directly to ground. To prevent this, a coupling capacitor can be inserted in the RF output line. This is strongly recommended during a 1dB compression measurement.

Enable Interface

Figure 6 shows a simplified schematic of the EN pin interface. The voltage necessary to turn on the LT5568-2 is 1V. To disable (shut down) the chip, the enable voltage must be below 0.5V. If the EN pin is not connected, the chip is disabled. This $EN = Low$ condition is assured by the 75k on-chip pull-down resistor. It is important that the voltage at the EN pin does not exceed V_{CC} by more than 0.5V. If this should occur, the supply current could be sourced through the EN pin ESD protection diodes, which are not designed to carry the full supply current, and damage may result.

Evaluation Board

Figure 7 shows the evaluation board schematic. A good ground connection is required for the exposed pad. If this is not done properly, the RF performance will degrade. Additionally, the exposed pad provides heat sinking for the part and minimizes the possibility of the chip overheating.

Figure 7. Evaluation Circuit Schematic

R1 (optional) limits the EN pin current in the event that the EN pin is pulled high while the V $_{\rm CC}$ inputs are low. In Figures 8 and 9 the silk screens and the PCB board layout are shown.

Figure 8. Component Side of Evaluation Board

Figure 9. Bottom Side of Evaluation Board

Application Measurements

The LT5568-2 is recommended for base-station applications using various modulation formats. Figure 10 shows a typical application. Figure 11 shows the ACPR performance for CDMA2000 using 1- and 3-carrier modulation. Figures 12 and 13 illustrate the 1- and 3-carrier CDMA2000 RF spectrum. To calculate ACPR, a correction is made for the spectrum analyzer noise floor. If the output power is high, the ACPR will be limited by the linearity performance of the part. If the output power is low, the ACPR will be limited by the noise performance of the part. In the middle, an optimum ACPR is observed.

Because of the LT5568-2's very high dynamic range, the test equipment can limit the accuracy of the ACPR measurement. See Application Note 99. Consult the factory for advice on the ACPR measurement, if needed.

The ACPR performance is sensitive to the amplitude match of the BBPI and BBMI (or BBPQ and BBMQ) inputs. This is because a difference in AC current amplitude will give rise to a difference in amplitude between the even-order harmonic products generated in the internal V-I converter. As a result, they will not cancel out entirely. Therefore, it is important to keep the currents in those pins exactly

the same (but of opposite sign). The current will enter the LT5568-2's common-base stage, and will flow to the mixer upper switches. This can be seen in Figure 1 where the internal circuit of the LT5568-2 is drawn.

 After calibration when the temperature changes, the LO feedthrough and the image rejection performance will

> TEMPERATURE (°C) $-40 -20$ –90 LO FEEDTHROUGH (dBm), IR (dBc) –70 –50 0 20 40 60 80 55682 F14 –80 –60 20 60 EN = High $V_{CC} = 5V$ $f_{\text{BBI}} = 2 \text{MHz}, 0^{\circ}$ $f_{BBO} = 2MHz$, 90° $f_{LO} = 900MHz$ $f_{RF} = f_{BB} + f_{LO}$ $P_{LO} = 0$ dBm IMAGE REJECTION LO FEED-**THROUGH** CALIBRATED WITH $P_{RF} = -10$ dBm

Figure 14. LO Feedthrough and Image Rejection vs Temperature after Calibration at 25°C

change. This is illustrated in Figure 14. The LO feedthrough and image rejection can also change as a function of the baseband drive level, as is depicted in Figure 15. In Figure 16 the GSM EVM and noise performance vs RF output power is drawn.

Figure 15. LO Feedthrough and Image Rejection vs Baseband Drive Voltage after Calibration at 25°C

Figure 16. GSM EVM and Noise vs RF Output Power at 900MHz

PACKAGE DESCRIPTION

OT LINEAR

Information furnished by Linear Technology Corporation is believed to be accurate and reliable. However, no responsibility is assumed for its use. Linear Technology Corporation makes no representation that the interconnection of its circuits as described herein will not infringe on existing patent rights.