

# LT6210/LT6211

Single/Dual Programmable Supply Current, R-R Output, Current Feedback Amplifiers

## Features

- **Programmable Supply Current and Bandwidth:** 10MHz at 300µA per Amplifier up to 200MHz at 6mA per Amplifier
- Rail-to-Rail Output: 0.05V to 2.85V on 3V Single Supply
- High Slew Rate: 700V/µs
- High Output Drive: ±75mA Minimum Output Current
- C-Load<sup>™</sup> Op Amp Drives All Capacitive Loads
- Low Distortion:  $-70$ dB HD2 at 1MHz 2V<sub>P-P</sub>  $-75$ dB HD3 at 1MHz 2V<sub>P-P</sub>
- <sup>n</sup> **Fast Settling:**  20ns 0.1% Settling for 2V Step
- <sup>n</sup> **Excellent Video Performance Into 150Ω Load:**  Differential Gain of 0.20%, Differential Phase of 0.10°
- Wide Supply Range: 3V to 12V Single Supply ±1.5V to ±6V Dual Supplies
- <sup>n</sup> **Small Size:**

Low Profile (1mm) 6-Lead ThinSOT™,  $3$ mm  $\times$  3mm  $\times$  0.8mm DFN and 10-Lead MSOP Packages

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# **DESCRIPTION**

The LT®6210/LT6211 are single/dual current feedback amplifiers with externally programmable supply current and bandwidth ranging from 10MHz at 300µA per amplifier to 200MHz at 6mA per amplifier. They feature a low distortion rail-to-rail output stage, 700V/µs slew rate and a minimum output current drive of 75mA.

The LT6210/LT6211 operate on supplies as low as a single 3V and up to either 12V or  $\pm$ 6V. The  $I_{\rm SFT}$  pin allows for the optimization of quiescent current for specific bandwidth, distortion or slew rate requirements. Regardless of supply voltage, the supply current is programmable from just 300µA to 6mA per amplifier with an external resistor or current source.

The LT6210 is available in the low profile (1mm) 6-lead TSOT-23 package. The LT6211 is available in the 10-lead MSOP and the  $3mm \times 3mm \times 0.8mm$  DFN packages.

## Applications

- Buffers
- $\blacksquare$  Video Amplifers
- $\blacksquare$  Cable Drivers
- Mobile Communication
- Low Power/Battery Applications

## Typical Application

**Line Driver Configuration for Various Supply Currents**



### **Small Signal Response vs Supply Current**





62101fc

1

# Absolute Maximum Ratings

**(Note 1)**





# Pin Configuration



# order information



Consult LTC Marketing for parts specified with wider operating temperature ranges. \*The temperature grade is identified by a label on the shipping container.

For more information on lead free part marking, go to: http://www.linear.com/leadfree/

For more information on tape and reel specifications, go to: http://www.linear.com/tapeandreel/



**ELECTRICAL CHARACTERISTICS**  $(I_S = 6mA per Amplifier)$  The  $\bullet$  denotes the specifications which apply over the specified operating temperature range, otherwise specifications are at T<sub>A</sub> = 25°C. For V<sup>+</sup> = 5V, V<sup>-</sup> = -5V: R<sub>SET</sub> = 20k to ground, A<sub>V</sub> = +2, R<sub>F</sub> = R<sub>G</sub> = 887Ω, R<sub>L</sub> = 150Ω; For V<sup>+</sup> = 3V, V<sup>−</sup> = 0V: R<sub>SET</sub> = 0Ω to V<sup>−</sup>, A<sub>V</sub> = +2, R<sub>F</sub> = 887Ω, R<sub>G</sub> = 887Ω to 1.5V,  $R_L$  = 150 $\Omega$  to 1.5V unless otherwise specified.



**ELECTRICAL CHARACTERISTICS** (I<sub>S</sub> = 6mA per Amplifier) The  $\bullet$  denotes the specifications which apply over the specified operating temperature range, otherwise specifications are at T<sub>A</sub> = 25°C. For V<sup>+</sup> = 5V, V<sup>-</sup> = -5V: R<sub>SET</sub> = 20k to ground,  $A_V$  = +2,  $R_F$  =  $R_G$  = 887Ω,  $R_L$  = 150Ω; For V<sup>+</sup> = 3V, V<sup>-</sup> = 0V:  $R_{SET}$  = 0Ω to V<sup>-</sup>,  $A_V$  = +2,  $R_F$  = 887Ω,  $R_G$  = 887Ω to 1.5V,  $R_L$  = 150 $\Omega$  to 1.5V unless otherwise specified.



**(I<sub>S</sub> = 3mA per Amplifier)** The  $\bullet$  denotes the specifications which apply over the specified operating temperature range,  $\delta$ therwise specifications are at T<sub>A</sub> = 25°C. For V<sup>+</sup> = 5V, V<sup>−</sup> = −5V: R<sub>SET</sub> = 56k to ground, A<sub>V</sub> = +2, R<sub>F</sub> = R<sub>G</sub> = 1.1k, R<sub>L</sub> = 150Ω; For V<sup>+</sup> = 3V, **V– = 0V: RSET = 10k to V–, AV = +2, RF = 1.27k, RG = 1.27k to 1.5V, RL = 150Ω to 1.5V unless otherwise specified.**





**ELECTRICAL CHARACTERISTICS**  $(I_S = 3mA per Amplifier)$  The  $\bullet$  denotes the specifications which apply over the specified operating temperature range, otherwise specifications are at T<sub>A</sub> = 25°C. For V<sup>+</sup> = 5V, V<sup>-</sup> = -5V: R<sub>SET</sub> = 56k to **ground, AV = +2, RF = RG = 1.1k, RL = 150Ω; For V+ = 3V, V– = 0V: RSET = 10k to V–, AV = +2, RF = 1.27k, RG = 1.27k to 1.5V,**   $R_L$  = 150 $\Omega$  to 1.5V unless otherwise specified.



**(I<sub>S</sub> = 300µA per Amplifier)** The  $\bullet$  denotes the specifications which apply over the specified operating temperature range, otherwise specifications are at T<sub>A</sub> = 25°C. For V<sup>+</sup> = 5V, V<sup>-</sup> = -5V: R<sub>SET</sub> = 1M to ground, A<sub>V</sub> = +2, R<sub>F</sub> = R<sub>G</sub> = 11k, R<sub>L</sub> = 1k; For V<sup>+</sup> = 3V,  $V^-$  = 0V: R<sub>SET</sub> = 270k to V<sup>-</sup>, A<sub>V</sub> = +2, R<sub>F</sub> = 9.31k, R<sub>G</sub> = 9.31k to 1.5V, R<sub>L</sub> = 1k to 1.5V unless otherwise specified.





**ELECTRICAL CHARACTERISTICS** (I<sub>S</sub> = 300µA per Amplifier) The  $\bullet$  denotes the specifications which apply over the specified operating temperature range, otherwise specifications are at  $T_A$  = 25°C. For V<sup>+</sup> = 5V, V<sup>-</sup> = –5V: R<sub>SET</sub> = 1M to ground,  $A_V = +2$ ,  $R_F = R_G = 11k$ ,  $R_L = 1k$ ; For V<sup>+</sup> = 3V, V<sup>-</sup> = 0V:  $R_{SET} = 270k$  to V<sup>-</sup>,  $A_V = +2$ ,  $R_F = 9.31k$ ,  $R_G = 9.31k$  to 1.5V,  $R_L = 1k$  to **1.5V unless otherwise specified.**



**Note 1:** Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

**Note 2:** As long as output current and junction temperature are kept below the absolute maximum ratings, no damage to the part will occur. Depending on the supply voltage, a heat sink may be required.

**Note 3:** The LT6210C/LT6211C is guaranteed functional over the operating temperature range of –40°C to 85°C.

**Note 4:** The LT6210C/LT6211C is guaranteed to meet specified performance from 0°C to 70°C. The LT6210C/LT6211C is designed, characterized and expected to meet specified performance from –40°C and 85°C but is not tested or QA sampled at these temperatures. The LT6210I/ LT6211I is guaranteed to meet specified performance from –40°C to 85°C.

**Note 5:** The LT6210 with no metal connected to the V<sup>-</sup> pin has a θ<sub>JA</sub> of 230°C/W, however, thermal resistances vary depending upon the amount of PC board metal attached to Pin 2 of the device. With the LT6210 mounted on a 2500mm2 3/32" FR-4 board covered with 2oz copper on both sides and with just 20mm<sup>2</sup> of copper attached to Pin 2,  $\theta_{JA}$  drops to 160°C/W. Thermal performance can be improved even further by using a 4-layer board or by attaching more metal area to Pin 2.

Thermal resistance of the LT6211 in MSOP-10 is specified for a 2500mm<sup>2</sup> 3/32" FR-4 board covered with 2oz copper on both sides and with 100mm2 of copper attached to Pin 5. Its performance can also be increased with additional copper much like the LT6210.

To achieve the specified  $\theta_{JA}$  of 43°C/W for the LT6211 DFN-10, the exposed pad must be soldered to the PCB. In this package,  $\theta_{JA}$  will benefit from increased copper area attached to the exposed pad.

 $T_{\text{J}}$  is calculated from the ambient temperature  $T_{\text{A}}$  and the power dissipation PD according to the following formula:

$$
T_{J} = T_{A} + (P_{D} \bullet \theta_{JA})
$$

The maximum power dissipation can be calculated by:

$$
P_{D(MAX)} = (V_S \cdot I_{S(MAX)}) + (V_S/2)^2 / R_{LOAD}
$$

**Note 6:** For PSRR and –IPSRR testing, the current into the I<sub>SET</sub> pin is constant, maintaining a consistent LT6210/LT6211 quiescent bias point. A graph of PSRR vs Frequency is included in the Typical Performance Characteristics showing +PSRR and  $-$ PSRR with  $R_{\text{SET}}$  connecting  $I_{\text{SET}}$  to ground.

**Note 7:** While the LT6210 and LT6211 circuitry is capable of significant output current even beyond the levels specified, sustained shortcircuit current exceeding the Absolute Maximum Rating of  $\pm 80$ mA may permanently damage the device.

**Note 8:** This parameter is guaranteed to meet specified performance through design and characterization. It is not production tested.

**Note 9:** Differential gain and phase are measured using a Tektronix TSG120YC/NTSC signal generator and a Tektronix 1780R Video Measurement Set. The resolution of this equipment is 0.1% and 0.1°. Five identical amplifier stages were cascaded giving an effective resolution of 0.02% and 0.02°.

**Note 10:** Input voltage range on ±5V dual supplies is guaranteed by CMRR. On 3V single supply it is guaranteed by design and by correlation to the ±5V input voltage range limits.

**Note 11:** This parameter is tested by forcing a 50mV differential voltage between the inverting and noninverting inputs.



## Typical AC Performance



# Typical Performance Characteristics





### **Supply Current per Amplifier vs Temperature**



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**CMRR and PSRR vs Frequency (IS = 6mA per Amplifier)**



**Frequency Response vs Closed**  Loop Gain (I<sub>S</sub> = 6mA per Amplifier) 9  $\frac{1}{A_V}$  = 2 T TI  $R_F = R_G = 887\Omega$ 6 3 GAIN (dB)  $\theta$  $A_V = 1$  $R_V = 1$ <br>  $R_F = 1.2k$ <br>  $\parallel \parallel$  $\mathbb{H}$  $V_S = \pm 5V$ –3  $R_{L}$  = 150 $\Omega$  $A_V =$  $T_A = 25^{\circ}C$  $R_F = R_G = 698\Omega$  $V_{\text{OUT}} = 100 \text{mV}_{\text{P-F}}$ –ا 6–<br>1.0 1 0.1 10 100 1000 FREQUENCY (MHz) 6210 G19

**CMRR and PSRR vs Frequency (IS = 3mA per Amplifier)**



**Frequency Response vs Closed**  Loop Gain (I<sub>S</sub> = 3mA per Amplifier)

= 1100 $Ω$ 

 $A_V = 2$ <br> $R_F = R_G$ 

GAIN (dB)

9

6

3

0

–3

 $V_S = \pm 5V$  $R_L = 150\Omega$  $T_A = 25^{\circ}C$  $V_{\text{OUT}} = 100 \text{mVp-p}$ 

–ا 6–<br>1.0

FREQUENCY (MHz)

1

0.1 10 100 1000

 $A_V = -1$  $R_F = R_G = 1200Ω$ 

> $A_V = 1$  $R_F$  = 1690Ω

> > 6210 G20

**CMRR and PSRR vs Frequency (IS = 300µA per Amplifier)**



**Frequency Response vs Closed**  Loop Gain  $I_s = 300 \mu A$  per **Amplifier)**















**Small-Signal Transient Response** 

**(IS = 3mA per Amplifier)**

 $V_S = \pm 5V$  TIME (10ns/DIV)

62101 G35

### **1MHz 2nd and 3rd Harmonic Distortion vs Supply Current** –30  $V_S = \pm 5V$  $A_V = 2$  $V_{\text{OUT}} = 2V_{\text{P-P}}$ –40 HARMONIC DISTORTION (dBc) HARMONIC DISTORTION (dBc)  $T_A = 25\degree C$ –50 HD2 –60 HD3 –70 –80 <sup>∟</sup><br>1.0 0.1 1 10 SUPPLY CURRENT PER AMPLIFIER (mA)



### **Small-Signal Transient Response (IS = 6mA per Amplifier)**







### **Large-Signal Transient Response (IS = 3mA per Amplifier)**

 $V_{IN} = \pm 25 \text{mV}$  $R_F = R_G = 1.1k$  $R_{\text{SET}} = 56k$  TO GND  $R_L = 150\Omega$ 

OUTPUT (50mV/DIV)



### **Small-Signal Transient Response (IS = 300µA per Amplifier)**



### **Large-Signal Transient Response (IS = 300µA per Amplifier)**



**TLINEAR** 

# Applications Information

### **Setting the Quiescent Operating Current (ISET Pin)**

The quiescent bias point of the LT6210/LT6211 is SET with either an external resistor from the  $I_{\text{SET}}$  pin to a lower potential or by drawing a current out of the  $I_{\text{SFT}}$ pin. However, the  $I_{\text{SET}}$  pin is not designed to function as a shutdown. The LT6211 uses two entirely independent bias networks, so while each channel can be programmed for a different supply current, neither  $I_{\text{SET}}$  pin should be left unconnected. A simplified schematic of the internal biasing structure can be seen in Figure 1. Figure 2 illustrates the results of varying  $R_{\text{SFT}}$  on 3V and  $\pm 5V$  supplies. Note that shorting the  $I_{\text{SFT}}$  pin under 3V operation results in a quiescent bias of approximately 6mA. Attempting to bias the LT6210/LT6211 at a current level higher than 6mA by using a smaller resistor may result in instability and decreased performance. However, internal circuitry clamps the supply current of the part at a safe level of approximately 15mA in case of accidental connection of the  $I_{\text{SFT}}$  pin directly to a negative potential.



**Figure 1. Internal Bias Setting Circuitry**



**Figure 2. Setting RSET to Control Is** 

### **Input Considerations**

The inputs of the LT6210/LT6211 are protected by backto-back diodes. If the differential input voltage exceeds 1.4V, the input current should be limited to less than the absolute maximum ratings of  $±10$ mA. In normal operation, the differential voltage between the inputs is small, so the ±1.4V limit is generally not an issue. ESD diodes protect both inputs, so although the part is not guaranteed to function outside the common mode range, input voltages that exceed a diode beyond either supply will also require current limiting to keep the input current below the absolute maximum of  $±10mA$ .

### **Feedback Resistor Selection**

The small-signal bandwidth of the LT6210/LT6211 is set by the external feedback resistors and the internal junction capacitances. As a result, the bandwidth is a function of the quiescent supply current, the supply voltage, the value of the feedback resistor, the closed-loop gain and the load resistor. Refer to the Typical AC Performance table for more information.

### **Layout and Passive Components**

As with all high speed amplifiers, the LT6210/LT6211 require some attention to board layout. Low ESL/ESR bypass capacitors should be placed directly at the positive and negative supply (0.1µF ceramics are recommended). For best transient performance, additional 4.7µF tantalums should be added. A ground plane is recommended and trace lengths should be minimized, especially on the inverting input lead.

### **Capacitance on the Inverting Input**

Current feedback amplifiers require resistive feedback from the output to the inverting input for stable operation. Capacitance on the inverting input will cause peaking in the frequency response and overshoot in the transient response. Take care to minimize the stray capacitance at the inverting input to ground and between the output and the inverting input. If significant capacitance is unavoidable in a given application, an inverting gain configuration should be considered. When configured inverting, the amplifier inputs do not slew and the effect of parasitics is greatly reduced.



# Applications Information

### **Capacitive Loads**

The LT6210/LT6211 are stable with any capacitive load. Although peaking and overshoot may result in the AC transient response, the amplifier's compensation decreases bandwidth with increasing output capacitive load to ensure stability. To maintain a response with minimal peaking, the feedback resistor can be increased at the cost of bandwidth as shown in the Typical Performance Characteristics. Alternatively, a small resistor (5 $\Omega$  to 35 $\Omega$ ) can be put in series with the output to isolate the capacitive load from the amplifier output. This has the advantage that the amplifier bandwidth is only reduced when the capacitive load is present. The disadvantage of this technique is that the gain is a function of the load resistance.

### **Power Supplies**

The LT6210/LT6211 will operate on single supplies from 3V to 12V and on split supplies from  $\pm$ 1.5V to  $\pm$ 6V. If split supplies of unequal absolute value are used, input offset voltage and inverting input current will shift from the values specified in the Electrical Characteristics table. Input offset voltage will shift 2mV and inverting input current will shift 0.5µA for each volt of supply mismatch.

### **Slew Rate**

Unlike a traditional voltage feedback op amp, the slew rate of a current feedback amplifier is not independent of the amplifier gain configuration. In a current feedback amplifier, both the input stage and the output stage have slew rate limitations. In the inverting mode, and for gains of 2 or more in the noninverting mode, the signal amplitude between the input pins is small and the overall slew rate is that of the output stage. For gains less than 2 in the noninverting mode, the overall slew rate is limited by the input stage. The input slew rate of the LT6210/LT6211 on  $±5V$  supplies with an R<sub>SFT</sub> resistor of 20k ( $I_S = 6$ mA) is approximately 600V/µs and is set by internal currents and capacitances. The output slew rate is additionally constrained by the value of the feedback resistor and internal capacitance. At a gain of 2 with  $887\Omega$  feedback and gain resistors, ±5V supplies and the same biasing as above, the output slew rate is typically 700V/µs. Larger feedback resistors, lower supply voltages and lower supply current levels will all reduce slew rate. Input slew rates significantly exceeding the output slew capability can actually decrease slew performance in a positive gain configuration; the cleanest transient response will be obtained from input signals with slew rates slower than 1000V/us.

### **Output Swing and Drive**

The output stage of the LT6210/LT6211 consists of a pair of class-AB biased common emitters that enable the output to swing rail-to-rail. Since the amplifiers can potentially deliver output currents well beyond the specified minimum short-circuit current, care should be taken not to short the output of the device indefinitely. Attention must be paid to keep the junction temperature of the IC below the absolute maximum rating of 150°C if the output is used to drive low impedance loads. See Note 5 for details. Additionally, the output of the amplifier has reverse-biased ESD diodes connected to each supply. If the output is forced beyond either supply, large currents will flow through these diodes. If the current is limited to 80mA or less, no damage to the part will occur.



# Typical Applications

### **3V Cable Driver with Active Termination**

Driving back-terminated cables on single supplies usually results in very limited signal amplitude at the receiving end of the cable. However, positive feedback can be used to reduce the size of the series back termination resistor, thereby decreasing the attenuation between the series and shunt termination resistors while still maintaining controlled output impedance from the line-driving amplifier. Figure 3 shows the LT6210 using this "active termination" scheme on a single 3V supply. The amplifier is AC-coupled and in an inverting gain configuration to maximize the input



**Figure 3. 3V Cable Driver with Active Termination Figure 4. Response of Circuit at 1MHz**

signal range. The gain from  $V_{IN}$  to the receiving end of the cable,  $V_{\text{OUT}}$ , is set to -1. The effective impedance looking into the amplifier circuit from the cable is  $50\Omega$  throughout the usable bandwidth.

The response of the cable driver with a 1MHz sinusoid is shown in Figure 4. The circuit is capable of transmitting a 1.5V<sub>P-P</sub> undistorted sinusoid to the 50 $\Omega$  termination resistor and has a full signal  $1V_{P-P}$  bandwidth of 50MHz. Small signal –3dB bandwidth extends from 1kHz to 56MHz with the selected coupling capacitors.





## Simplified Schematic



### Package Description



**DD Package DD Package 10-Lead Plastic DFN (3mm** × **3mm) 10-Lead Plastic DFN (3mm** × **3mm)** (Reference LTC DWG # 05-08-1699 Rev C) (Reference LTC DWG # 05-08-1699 Rev C)

NOTE:

1. DRAWING TO BE MADE A JEDEC PACKAGE OUTLINE M0-229 VARIATION OF (WEED-2).

CHECK THE LTC WEBSITE DATA SHEET FOR CURRENT STATUS OF VARIATION ASSIGNMENT

2. DRAWING NOT TO SCALE

3. ALL DIMENSIONS ARE IN MILLIMETERS

4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE

 MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE 5. EXPOSED PAD SHALL BE SOLDER PLATED

6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE

TOP AND BOTTOM OF PACKAGE



# Package Description



**MS Package 10-Lead Plastic MSOP**

**S6 Package 6-Lead Plastic TSOT-23**

(Reference LTC DWG # 05-08-1636)



NOTE: 1. DIMENSIONS ARE IN MILLIMETERS

2. DRAWING NOT TO SCALE 3. DIMENSIONS ARE INCLUSIVE OF PLATING

4. DIMENSIONS ARE EXCLUSIVE OF MOLD FLASH AND METAL BURR<br>5. MOLD FLASH SHALL NOT EXCEED 0.254mm<br>6. JEDEC RASHAGE REFERENCE IS MO-193



### REVISION HISTORY (Revision history begins at Rev C)





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