

# 25 $\mu$ V, 0.3 $\mu$ V/ $^{\circ}$ C, Low Noise Instrumentation Amplifier

## FEATURES

- **Single Gain Set Resistor:  $G = 1$  to  $>1000$**
- **Excellent DC Precision**
  - **Input Offset Voltage: 25 $\mu$ V Max**
  - **Input Offset Voltage Drift: 0.3 $\mu$ V/ $^{\circ}$ C Max**
  - **Low Gain Error: 0.01% Max ( $G = 1$ )**
  - **Low Gain Drift: 30ppm/ $^{\circ}$ C Max ( $G > 1$ )**
  - **High DC CMRR: 94dB Min ( $G = 1$ )**
- **Input Bias Current: 400pA Max**
- **3.1MHz  $-3$ dB Bandwidth ( $G = 1$ )**
- **Low Noise:**
  - **0.1Hz to 10Hz Noise: 0.2 $\mu$ V<sub>P-P</sub>**
  - **1kHz Voltage Noise: 7nV/ $\sqrt{\text{Hz}}$**
- **Integrated Input RFI Filter**
- **Wide Supply Range 4.75V to 35V**
- **Specified Temperature Ranges:**  
 $-40^{\circ}\text{C}$  to  $85^{\circ}\text{C}$ ,  $-40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$
- **MS8, S8E and 10-pin 3mm  $\times$  3mm DFN Packages**

## APPLICATIONS

- Bridge Amplifier
- Data Acquisition
- Multiplexed Signals
- Thermocouple Amplifier
- Strain Gauge Amplifier
- Medical Instrumentation
- Transducer Interfaces
- Differential to Single-Ended Conversion

## DESCRIPTION

The **LT<sup>®</sup>6370** is a gain programmable, high precision instrumentation amplifier that delivers industry leading DC precision. This high precision enables smaller signals to be sensed and eases calibration requirements, particularly over temperature.

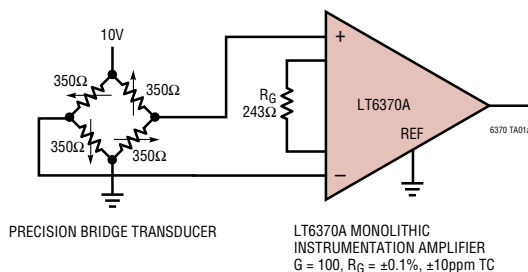
The LT6370 uses a proprietary high performance bipolar process which enables industry leading accuracy coupled with exceptional long-term stability. The LT6370 is laser trimmed for very low input offset voltage (25 $\mu$ V) and high CMRR (94dB,  $G = 1$ ). Proprietary on-chip test capability allows the input offset voltage drift (0.3 $\mu$ V/ $^{\circ}$ C) and gain drift (30ppm/ $^{\circ}$ C) to be guaranteed with automated testing on the S8E package.

In addition to excellent DC specifications, the LT6370's wide bandwidth (3.1MHz,  $G = 1$ ) and fast settling time allow it to operate well in multiplexed applications. EMI filtering is integrated on the LT6370's inputs to maintain accuracy in the presence of harsh RF interference.

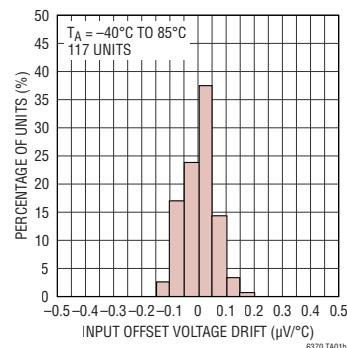
The LT6370 is available in a compact 8-pin MSOP or S8E which use the conventional instrumentation amplifier pin-out as well as a 10-pin 3mm  $\times$  3mm DFN. The S8E package is also offered as an A grade which has superior DC specifications. The LT6370 is fully specified over the  $-40^{\circ}\text{C}$  to  $85^{\circ}\text{C}$  and  $-40^{\circ}\text{C}$  to  $125^{\circ}\text{C}$  temperature ranges.

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## TYPICAL APPLICATION



**Distribution of Input Offset Voltage Drift, MS8 Package**



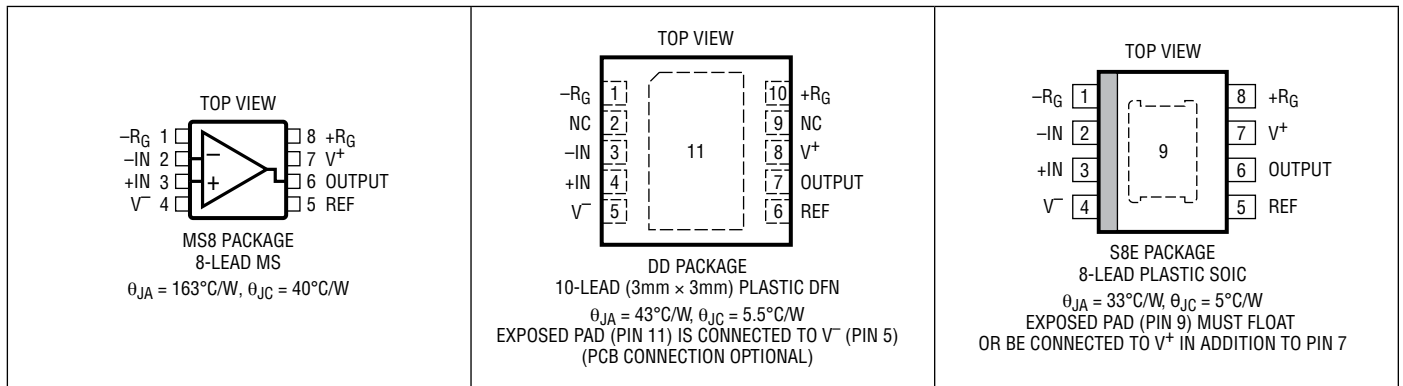
# LT6370

## ABSOLUTE MAXIMUM RATINGS

(Note 1)

Total Supply Voltage ( $V^+$ to $V^-$ ) .....	36V	Output Current .....	80mA
Input Voltage (+IN, -IN, +R <sub>G</sub> , -R <sub>G</sub> , REF) .....	( $V^- - 0.3V$ ) to ( $V^+ + 0.3V$ )	Operating and Specified Temperature Range	
Differential Input Voltage (+IN to -IN) .....	±36V	I-Grade .....	-40°C to 85°C
Input Current (+R <sub>G</sub> , -R <sub>G</sub> ) .....	±2mA	H-Grade .....	-40°C to 125°C
Input Current (+IN, -IN) .....	±10mA	Maximum Junction Temperature .....	150°C
Input Current (REF) .....	-10mA	Storage Temperature Range .....	-65°C to 150°C
Output Short-Circuit Duration .....	Thermally Limited	Lead Temperature (Soldering, 10 sec) .....	300°C

## PIN CONFIGURATION



## ORDER INFORMATION

TUBE	TAPE AND REEL	PART MARKING*	PACKAGE DESCRIPTION	TEMPERATURE RANGE
LT6370IS8E#PBF	LT6370IS8E#TRPBF	6370	8-Lead Plastic SO	-40°C to 85°C
LT6370HS8E#PBF	LT6370HS8E#TRPBF	6370	8-Lead Plastic SO	-40°C to 125°C
LT6370IMS8#PBF	LT6370IMS8#TRPBF	LTGZP	8-Lead Plastic MSOP	-40°C to 85°C
LT6370HMS8#PBF	LT6370HMS8#TRPBF	LTGZP	8-Lead Plastic MSOP	-40°C to 125°C
LT6370IDD#PBF	LT6370IDD#TRPBF	LGZN	10-Lead (3mm x 3mm) Plastic DFN	-40°C to 85°C
LT6370HDD#PBF	LT6370HDD#TRPBF	LGZN	10-Lead (3mm x 3mm) Plastic DFN	-40°C to 125°C
LT6370AIS8E#PBF	LT6370AIS8E#TRPBF	6370	8-Lead Plastic SO	-40°C to 85°C
LT6370AHS8E#PBF	LT6370AHS8E#TRPBF	6370	8-Lead Plastic SO	-40°C to 125°C

Contact the factory for parts specified with wider operating temperature ranges. \*The temperature grade is identified by a label on the shipping container.

[Tape and reel specifications.](#) Some packages are available in 500 unit reels through designated sales channels with #TRMPBF suffix.

**ELECTRICAL CHARACTERISTICS** The ● denotes the specifications which apply over the specified temperature range, otherwise specifications are at  $T_A = 25^\circ\text{C}$ .  $V_S = \pm 15\text{V}$ ,  $V_{CM} = V_{REF} = 0\text{V}$ ,  $R_L = 2\text{k}\Omega$ .

SYMBOL	PARAMETER	CONDITIONS	LT6370A			LT6370			UNITS
			MIN	TYP	MAX	MIN	TYP	MAX	
G	Gain Range	$G = (1 + 24.2\text{k}/R_G)$ (Note 2)	1		1000	1		1000	V/V
	Gain Error (Notes 3, 4)	$G = 1$		-0.004	0.01	-0.004	0.015	%	
		$G = 1$ ●			0.02		0.025	%	
		$G = 10$		-0.02	0.08	-0.02	0.1	%	
		$G = 10, T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ ●			0.4		0.42	%	
		$G = 10, T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ ●			0.58		0.6	%	
		$G = 100$		-0.02	0.08	-0.02	0.1	%	
		$G = 100, T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ ●			0.4		0.42	%	
		$G = 100, T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ ●			0.58		0.6	%	
		$G = 1000$		-0.05	0.15	-0.05	0.2	%	
	$G = 1000, T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ ●			0.47		0.52	%		
	$G = 1000, T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ ●			0.65		0.7	%		
	Gain vs Temperature (Notes 3, 4)	$G = 1$ (Note 5)		0.2	0.5	0.2	0.5	ppm/ $^\circ\text{C}$	
		$G > 1$ (Note 6)			20	30	20	50	ppm/ $^\circ\text{C}$
	Gain Nonlinearity (Notes 3, 7)	$V_{OUT} = \pm 10\text{V}, G = 1$		1	3	1	5	ppm	
		$V_{OUT} = \pm 10\text{V}, G = 1$ ●			6		8	ppm	
		$V_{OUT} = \pm 10\text{V}, G = 10$		3	20	3	30	ppm	
		$V_{OUT} = \pm 10\text{V}, G = 10$ ●			65		75	ppm	
		$V_{OUT} = \pm 10\text{V}, G = 100$		20	30	20	55	ppm	
		$V_{OUT} = \pm 10\text{V}, G = 100$ ●			105		130	ppm	
		$V_{OUT} = \pm 10\text{V}, G = 1000$		50	200	50	300	ppm	
		$V_{OUT} = \pm 10\text{V}, G = 1000$ ●			270		370	ppm	
		$V_{OUT} = \pm 10\text{V}, G = 1, R_L = 600\Omega$			4		4	ppm	
		$V_{OUT} = \pm 10\text{V}, G = 10, R_L = 600\Omega$			6		6	ppm	
	$V_{OUT} = \pm 10\text{V}, G = 100, R_L = 600\Omega$			30		30	ppm		
	$V_{OUT} = \pm 10\text{V}, G = 1000, R_L = 600\Omega$			250		250	ppm		

**$V_{OST}$ , Total Input Referred Offset Voltage,  $V_{OST} = V_{OSI} + V_{OSO}/G$**

$V_{OSI}$	Input Offset Voltage (Note 8)	S8E Package		$\pm 9$	$\pm 25$	$\pm 15$	$\pm 55$	$\mu\text{V}$
		MS8 Package				$\pm 8$	$\pm 35$	$\mu\text{V}$
		DD10 Package				$\pm 15$	$\pm 60$	$\mu\text{V}$
		S8E Package, $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ ●			$\pm 100$		$\pm 130$	$\mu\text{V}$
		S8E Package, $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ ●			$\pm 125$		$\pm 155$	$\mu\text{V}$
		MS8 Package, $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ ●					$\pm 125$	$\mu\text{V}$
		MS8 Package, $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ ●					$\pm 150$	$\mu\text{V}$
		DD10 Package, $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ ●					$\pm 155$	$\mu\text{V}$
		DD10 Package, $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ ●					$\pm 180$	$\mu\text{V}$
$V_{OSO}$	Output Offset Voltage (Note 8)	S8E Package		$\pm 60$	$\pm 165$	$\pm 70$	$\pm 265$	$\mu\text{V}$
		MS8 Package				$\pm 30$	$\pm 150$	$\mu\text{V}$
		DD10 Package				$\pm 45$	$\pm 250$	$\mu\text{V}$
		S8E Package, $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ ●			$\pm 390$		$\pm 490$	$\mu\text{V}$
		S8E Package, $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ ●			$\pm 515$		$\pm 615$	$\mu\text{V}$
		MS8 Package, $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ ●					$\pm 325$	$\mu\text{V}$
		MS8 Package, $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ ●					$\pm 400$	$\mu\text{V}$
		DD10 Package, $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ ●					$\pm 510$	$\mu\text{V}$
		DD10 Package, $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ ●					$\pm 650$	$\mu\text{V}$
$V_{OSI}/T$	Input Offset Voltage Drift (Notes 5, 8)	S8E Package, $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ ●			$\pm 0.3$		$\pm 0.4$	$\mu\text{V}/^\circ\text{C}$
		S8E Package, $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ ●			$\pm 0.4$		$\pm 0.5$	$\mu\text{V}/^\circ\text{C}$
		MS8 Package, $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ ●					$\pm 0.3$	$\mu\text{V}/^\circ\text{C}$
		MS8 Package, $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ ●					$\pm 0.4$	$\mu\text{V}/^\circ\text{C}$
		DD10 Package, $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ ●					$\pm 0.4$	$\mu\text{V}/^\circ\text{C}$
		DD10 Package, $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ ●					$\pm 0.5$	$\mu\text{V}/^\circ\text{C}$
	Input Offset Voltage Hysteresis (Note 9)	$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ ●		$\pm 1.5$		$\pm 1.5$	$\mu\text{V}$	
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ ●		$\pm 3$		$\pm 3$	$\mu\text{V}$	

## ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the specified temperature range, otherwise specifications are at  $T_A = 25^\circ\text{C}$ .  $V_S = \pm 15\text{V}$ ,  $V_{CM} = V_{REF} = 0\text{V}$ ,  $R_L = 2\text{k}\Omega$ .

SYMBOL	PARAMETER	CONDITIONS	LT6370A			LT6370			UNITS
			MIN	TYP	MAX	MIN	TYP	MAX	
$V_{OS0}/T$	Output Offset Voltage Drift (Notes 5, 8)	S8E Package, $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	●		±1.5		±2.5	$\mu\text{V}/^\circ\text{C}$	
		S8E Package, $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	●		±1.5		±3.5	$\mu\text{V}/^\circ\text{C}$	
		MS8 Package, $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	●				±2	$\mu\text{V}/^\circ\text{C}$	
		MS8 Package, $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	●				±2.5	$\mu\text{V}/^\circ\text{C}$	
		DD10 Package, $T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	●				±3	$\mu\text{V}/^\circ\text{C}$	
		DD10 Package, $T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	●				±4	$\mu\text{V}/^\circ\text{C}$	
	Output Offset Voltage Hysteresis (Note 9)	$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	●	±10		±10		$\mu\text{V}$	
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	●	±20		±20		$\mu\text{V}$	
$I_B$	Input Bias Current	MS8 and S8E Packages		±0.1	±0.4	±0.1	±0.6	nA	
		DD10 Package				±0.1	±0.8	nA	
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ , MS8 and S8E Packages	●		±1.3		±1.5	nA	
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$ , DD10 Package	●				±1.7	nA	
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ , MS8 and S8E Packages	●		±2.8		±3	nA	
	$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$ , DD10 Package	●				±3.2	nA		
$I_{OS}$	Input Offset Current	MS8 and S8E Packages		±0.2	±0.7	±0.2	±1	nA	
		DD10 Package				±0.2	±1.4	nA	
		MS8 and S8E Packages	●		±1.7		±2	nA	
	DD10 Package	●				±2.4	nA		
	Input Noise Voltage (Note 10)	0.1Hz to 10Hz, $G = 1$		2		2		$\mu\text{V}_{P-P}$	
		0.1Hz to 10Hz, $G = 1000$		0.2		0.2		$\mu\text{V}_{P-P}$	

### Total RTI Noise = $\sqrt{e_{ni}^2 + (e_{no}/G)^2}$ (Note 10)

$e_{ni}$	Input Noise Voltage Density	$f = 1\text{kHz}$		7		7		$\text{nV}/\sqrt{\text{Hz}}$	
$e_{no}$	Output Noise Voltage Density	$f = 1\text{kHz}$		65		65		$\text{nV}/\sqrt{\text{Hz}}$	
	Input Noise Current	0.1Hz to 10Hz		10		10		$\text{pA}_{P-P}$	
$i_n$	Input Noise Current Density	$f = 1\text{kHz}$		200		200		$\text{fA}/\sqrt{\text{Hz}}$	
$R_{IN}$	Input Resistance	$V_{IN} = -12.6\text{V}$ to $13\text{V}$		225		225		$\text{G}\Omega$	
$C_{IN}$	Differential Common Mode	$f = 100\text{kHz}$		0.9		0.9		pF	
		$f = 100\text{kHz}$		15.9		15.9		pF	
$V_{CM}$	Input Voltage Range	Guaranteed by CMRR		$V^- + 1.8/V^+ - 1.4$		$V^- + 1.8/V^+ - 1.4$		V	
		●	$V^- + 2.4$	$V^+ - 2$	$V^- + 2.4$	$V^+ - 2$	V		
CMRR	Common Mode Rejection Ratio	DC to 60Hz, 1k Source Imbalance, $V_{CM} = -12.6\text{V}$ to $13\text{V}$							
		$G = 1$	●	94	112	88	112	dB	
		$G = 1$	●	87		83		dB	
		$G = 10$	●	112	132	110	132	dB	
		$G = 10$	●	106		104		dB	
		$G = 100$	●	126	144	120	144	dB	
		$G = 100$	●	120		114		dB	
		$G = 1000$	●	134	148	130	148	dB	
		$G = 1000$	●	122		120		dB	
		AC Common Mode Rejection Ratio	$f = 20\text{kHz}$ , DD10 Package	$G = 1$				77	
$G = 10$						98		dB	
$G = 100$						135		dB	
$G = 1000$						128		dB	
$f = 20\text{kHz}$ , MS8 Package $f = 20\text{kHz}$ , S8E Package	$G = 1$				71		71		dB
	$G = 10$				91		91		dB
	$G = 100$		101		101		dB		
	$G = 1000$		103		103		dB		

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SYMBOL	PARAMETER	CONDITIONS	LT6370A			LT6370			UNITS	
			MIN	TYP	MAX	MIN	TYP	MAX		
PSRR	Power Supply Rejection Ratio	$V_S = \pm 2.375\text{V}$ to $\pm 17.5\text{V}$								
		$G = 1$	●	116	130		110	130	dB	
		$G = 1$	●	114			106		dB	
		$G = 10$	●	134	140		130	140	dB	
		$G = 10$	●	124			120		dB	
		$G = 100$	●	136	142		130	142	dB	
		$G = 100$	●	125			120		dB	
		$G = 1000$	●	136	146		130	146	dB	
		$G = 1000$	●	125			120		dB	
$V_S$	Supply Voltage	Guaranteed by PSRR	●	4.75	35		4.75	35	V	
$I_S$	Supply Current	$V_S = \pm 15\text{V}$	●		2.65	2.75		2.65	2.75	mA
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	●			2.9		2.9	mA	
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	●				3		3	mA
		$V_S = \pm 2.375\text{V}$	●		2.55	2.6		2.55	2.6	mA
		$T_A = -40^\circ\text{C}$ to $85^\circ\text{C}$	●			2.75		2.75	mA	
		$T_A = -40^\circ\text{C}$ to $125^\circ\text{C}$	●				2.85		2.85	mA
$V_{OUT}$	Output Voltage Swing	$V_S = \pm 15\text{V}$ , $R_L = 10\text{k}\Omega$	●	-14.5	-14.9/14	13.7	-14.5	-14.9/14	13.7	V
			●	-14.3		13.6	-14.3		13.6	V
		$V_S = \pm 2.375\text{V}$ , $R_L = 10\text{k}\Omega$	●	-2	-2.3/1.6	1.5	-2	-2.3/1.6	1.5	V
			●	-1.8		1.3	-1.8		1.3	V
			●							V
$I_{OUT}$	Output Short Circuit Current		●	35	55		35	55	mA	
			●	30			30		mA	
BW	-3dB Bandwidth	$G = 1$			3100			3100	kHz	
		$G = 10$			1150			1150	kHz	
		$G = 100$			184			184	kHz	
		$G = 1000$			19			19	kHz	
SR	Slew Rate	$G = 1$ , $V_{OUT} = \pm 10\text{V}$	●	8	11		8	11	V/ $\mu\text{s}$	
			●	6			6		V/ $\mu\text{s}$	
$t_S$	Settling Time	20V Output Step to 0.0015%								
		$G = 1$			5.8		5.8		$\mu\text{s}$	
		$G = 10$			9.8		9.8		$\mu\text{s}$	
		$G = 100$			16		16		$\mu\text{s}$	
		$G = 1000$			100		100	$\mu\text{s}$		
$R_{REFIN}$	REF Input Resistance				20		20	$\text{k}\Omega$		
$I_{REFIN}$	REF Input Current	$V_{+IN} = V_{-IN} = V_{REF} = 0\text{V}$	●	-40	-27	-14	-40	-27	-14	$\mu\text{A}$
			●	-60		6	-60		6	$\mu\text{A}$
$V_{REF}$	REF Voltage Range		●	$V^-$		$V^+$	$V^-$		$V^+$	V
$A_{VREF}$	REF Gain to Output	$V_{REF} = \pm 10\text{V}$			1		1		V/V	
	REF Gain Error	$V_{REF} = \pm 10\text{V}$	●	-80	-20	40	-100	-20	60	ppm
			●	-95		55	-115		75	ppm

## ELECTRICAL CHARACTERISTICS

**Note 1:** Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

**Note 2:** Gains higher than 1000 are possible but the resulting low  $R_G$  values can make PCB and package lead resistance a significant error source.

**Note 3:** Gain tests are performed with  $-IN$  at mid-supply and  $+IN$  driven.

**Note 4:** When the gain is greater than 1 the gain error and gain drift specifications do not include the effect of external gain set resistor  $R_G$ .

**Note 5:** This specification is guaranteed by design.

**Note 6:** This specification is guaranteed with high-speed automated testing on the LT6370A. This specification is guaranteed by design and characterization on the LT6370.

**Note 7:** This parameter is measured in a high speed automatic tester that does not measure the thermal effects with longer time constants. The

magnitude of these thermal effects are dependent on the package used, PCB layout, heat sinking and air flow conditions.

**Note 8:** For more information on how offsets relate to the amplifiers, see section "Input and Output Offset Voltage" in the Applications section.

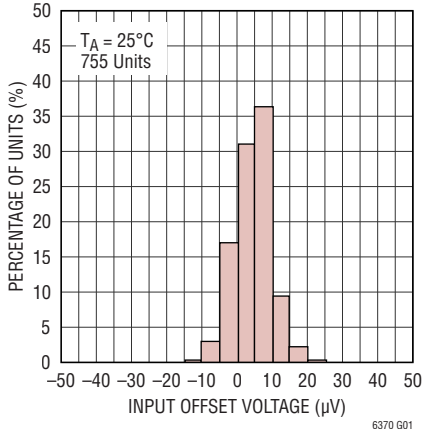
**Note 9:** Hysteresis in output voltage is created by mechanical stress that differs depending on whether the IC was previously at a higher or lower temperature. Output voltage is always measured at 25°C, but the IC is cycled to the hot or cold temperature limit before successive measurements. Hysteresis is roughly proportional to the square of the temperature change. For instruments that are stored at well controlled temperatures (within 20 or 30 degrees of operational temperature), hysteresis is usually not a significant error source. Typical hysteresis is the worst case of 25°C to cold to 25°C or 25°C to hot to 25°C, preconditioned by one thermal cycle.

**Note 10:** Referred to the input.

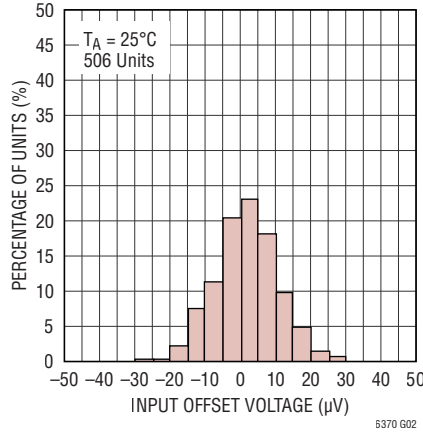
# TYPICAL PERFORMANCE CHARACTERISTICS

$V_S = \pm 15V$ ,  $V_{CM} = V_{REF} = 0V$ ,  $T_A = 25^\circ C$ ,  $R_L = 2k$ , unless otherwise noted.

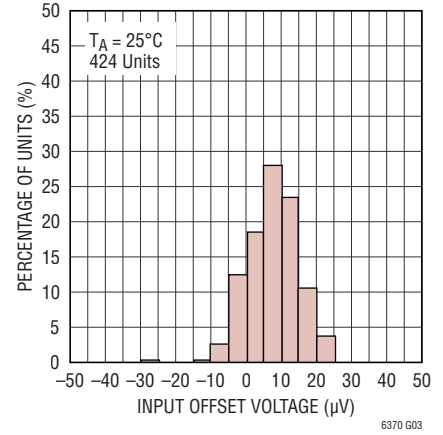
**Distribution of Input Offset Voltage, MS8 Package**



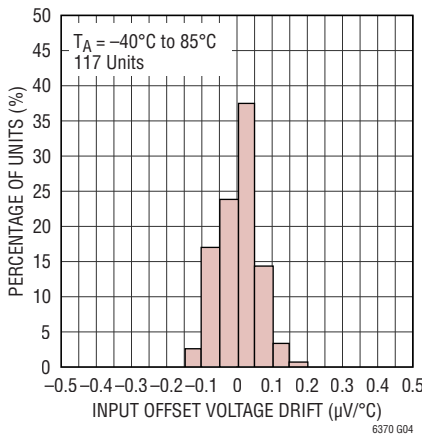
**Distribution of Input Offset Voltage, S8E Package**



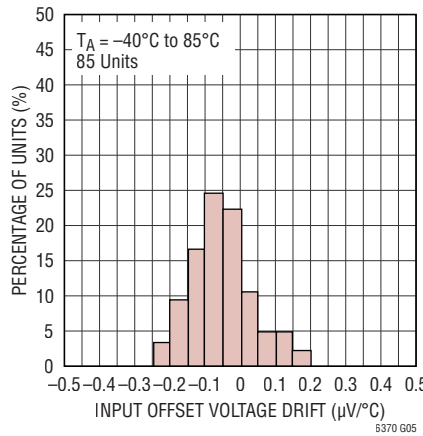
**Distribution of Input Offset Voltage, DD10 Package**



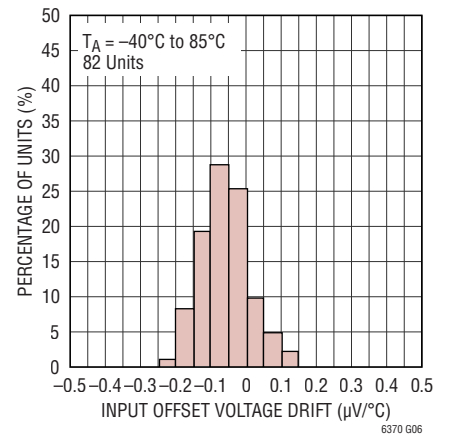
**Distribution of Input Offset Voltage Drift, MS8 Package**



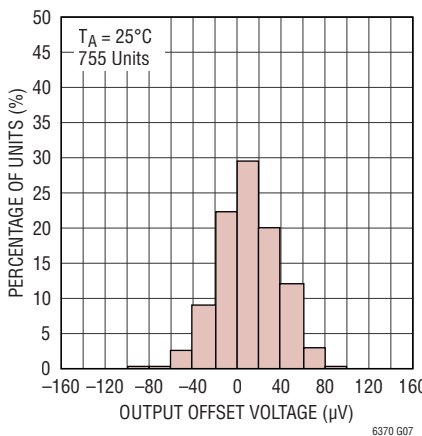
**Distribution of Input Offset Voltage Drift, S8E Package**



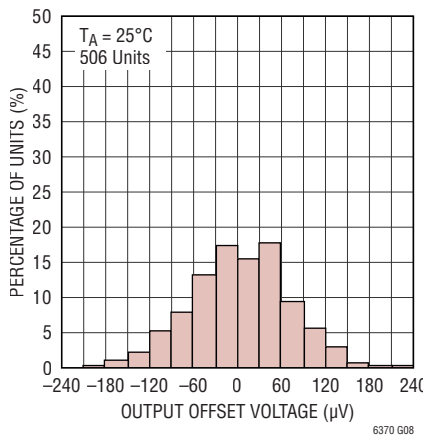
**Distribution of Input Offset Voltage Drift, DD10 Package**



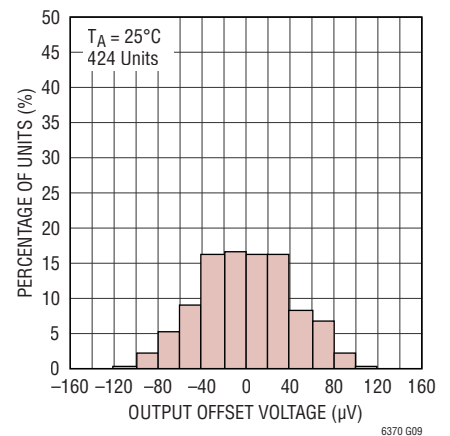
**Distribution of Output Offset Voltage, MS8 Package**



**Distribution of Output Offset Voltage, S8E Package**



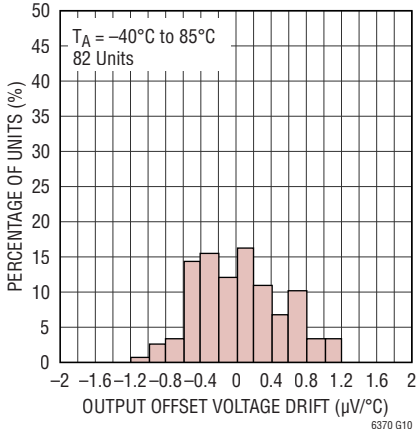
**Distribution Output Offset Voltage, DD10 Package**



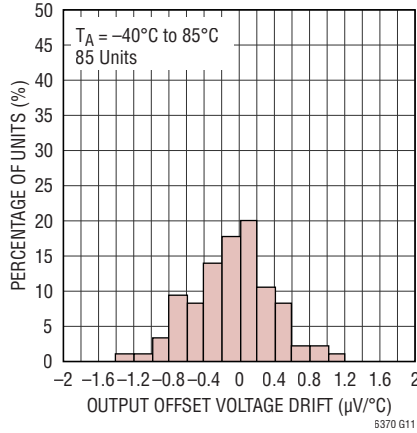
## TYPICAL PERFORMANCE CHARACTERISTICS

$V_S = \pm 15V$ ,  $V_{CM} = V_{REF} = 0V$ ,  $T_A = 25^\circ C$ ,  $R_L = 2k$ , unless otherwise noted.

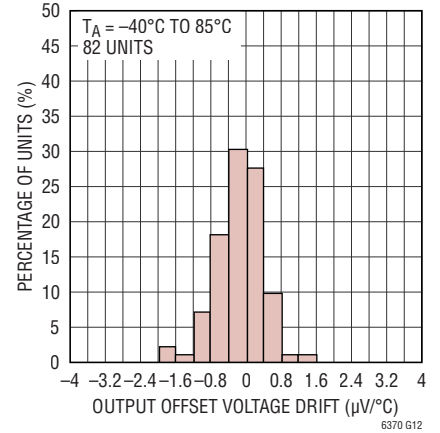
**Distribution of Output Offset Voltage Drift, MS8 Package**



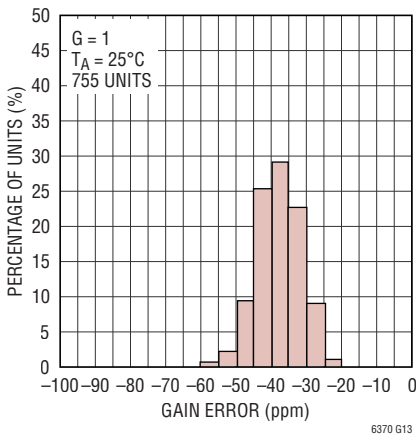
**Distribution of Output Offset Voltage Drift, S8E Package**



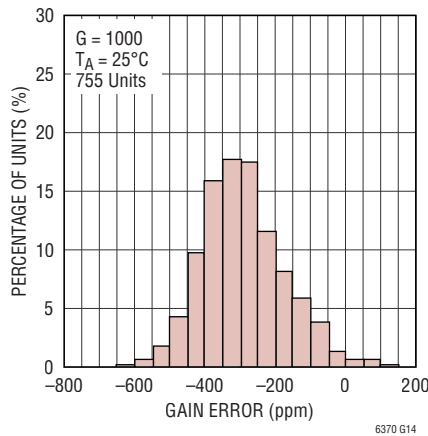
**Distribution of Output Offset Voltage Drift, DD10 Package**



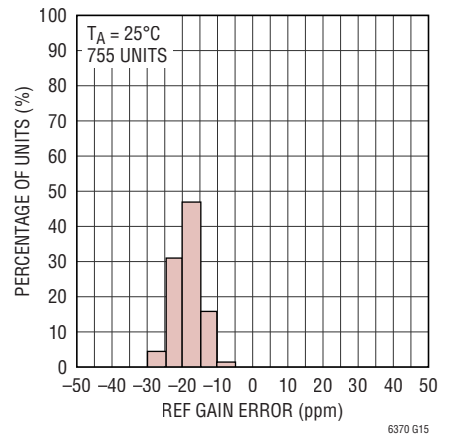
**Distribution of Gain Error**



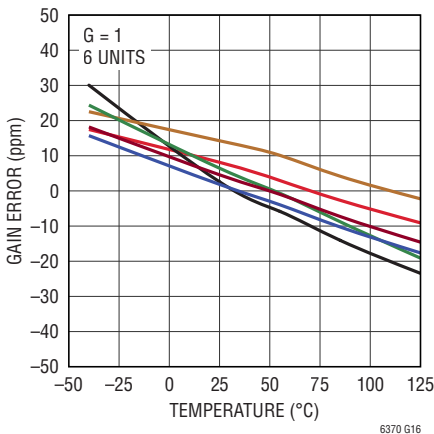
**Distribution of Gain Error**



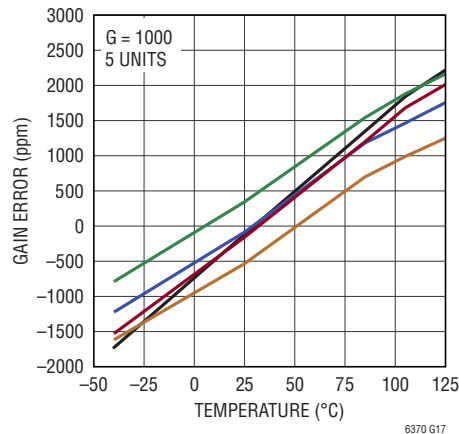
**Distribution of REF Gain Error**



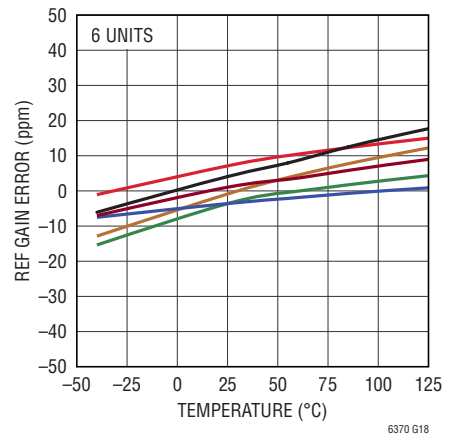
**Gain Drift (G = 1)**



**Gain Drift (G = 1000)**



**REF Gain Drift**

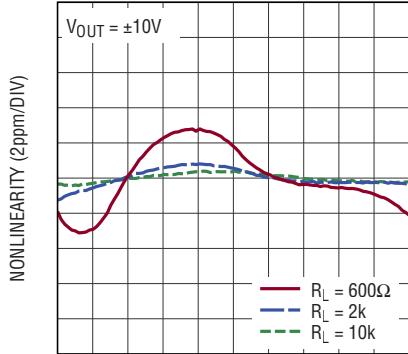




# TYPICAL PERFORMANCE CHARACTERISTICS

$V_S = \pm 15V$ ,  $V_{CM} = V_{REF} = 0V$ ,  $T_A = 25^\circ C$ ,  $R_L = 2k$ , unless otherwise noted.

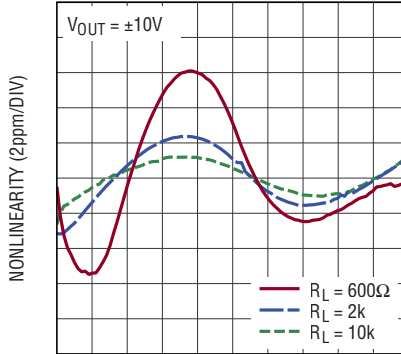
**Gain Nonlinearity (G = 1)**



OUTPUT VOLTAGE (2V/DIV)

6370 G19

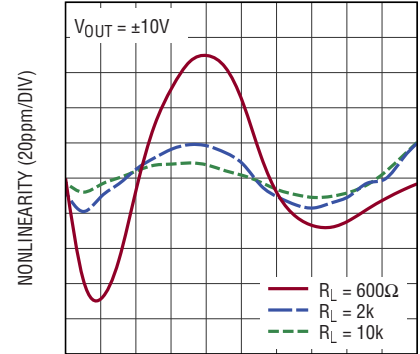
**Gain Nonlinearity (G = 10)**



OUTPUT VOLTAGE (2V/DIV)

6370 G20

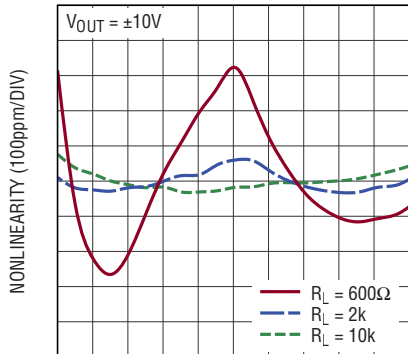
**Gain Nonlinearity (G = 100)**



OUTPUT VOLTAGE (2V/DIV)

6370 G21

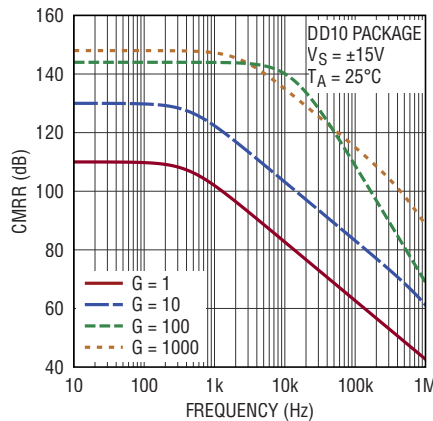
**Gain Nonlinearity (G = 1000)**



OUTPUT VOLTAGE (2V/DIV)

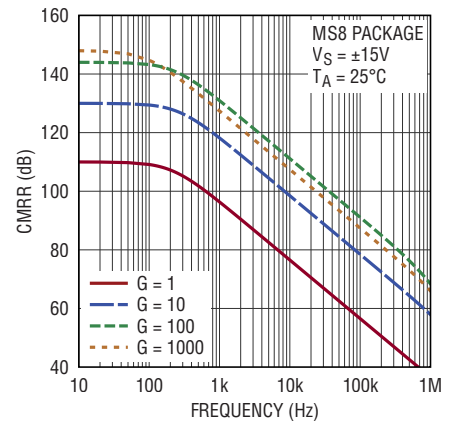
6370 G22

**CMRR vs Frequency, RTI  
DD10 Package**



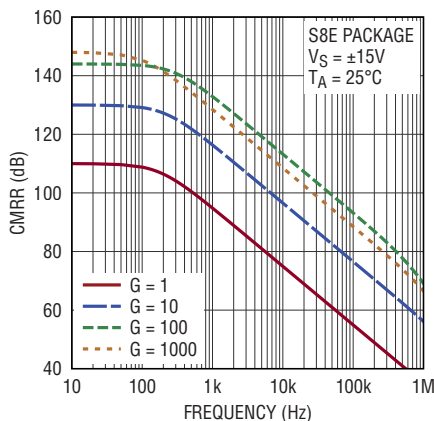
6370 G23

**CMRR vs Frequency, RTI  
MS8 Package**



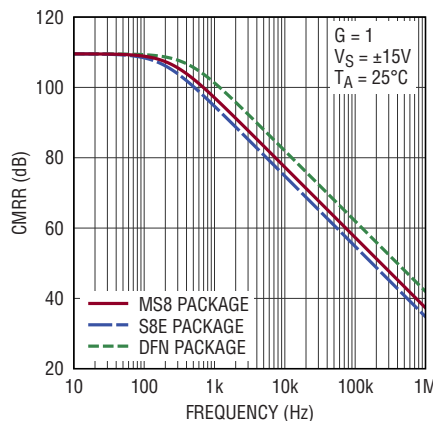
6370 G24

**CMRR vs Frequency, RTI  
S8E Package**



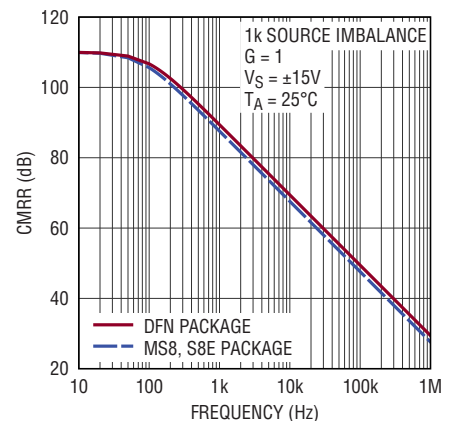
6370 G25

**CMRR vs Frequency, RTI**



6370 G26

**CMRR vs Frequency, RTI**

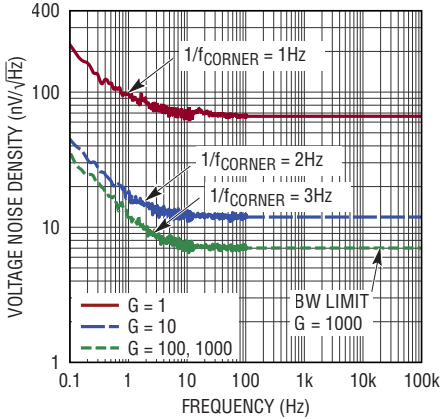


6370 G27

# TYPICAL PERFORMANCE CHARACTERISTICS

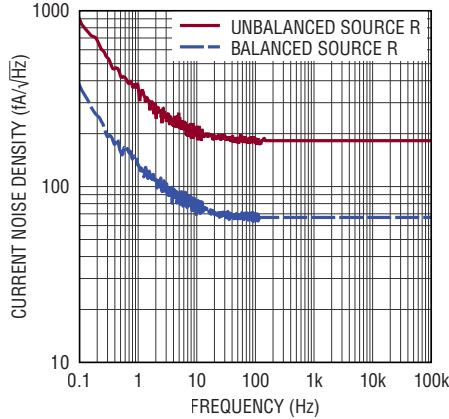
$V_S = \pm 15V$ ,  $V_{CM} = V_{REF} = 0V$ ,  $T_A = 25^\circ C$ ,  $R_L = 2k$ , unless otherwise noted.

**Input-Referred Voltage Noise Density vs Frequency**



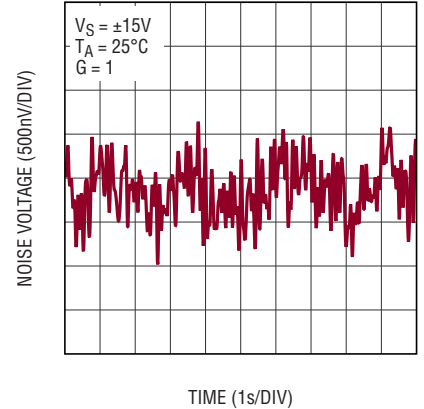
6370 G28

**Current Noise Density vs Frequency**



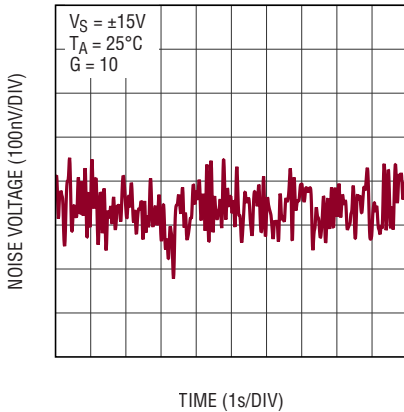
6370 G29

**0.1Hz to 10Hz Voltage Noise, G = 1, RTI**



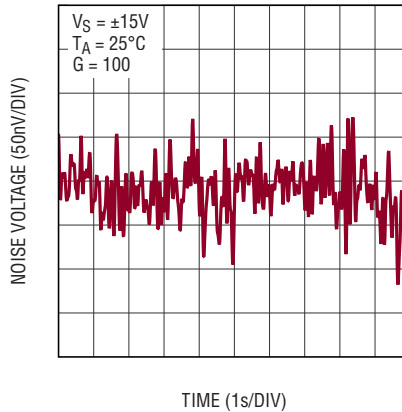
6370 G30

**0.1Hz to 10Hz Voltage Noise, G = 10, RTI**



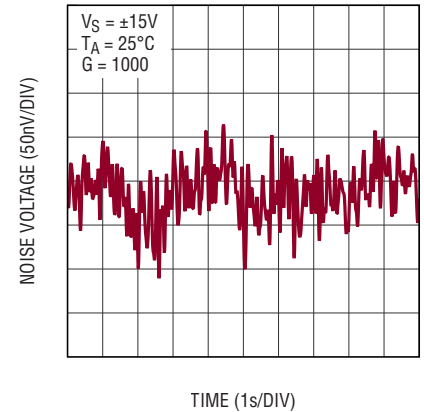
6370 G31

**0.1Hz to 10Hz Voltage Noise, G = 100, RTI**



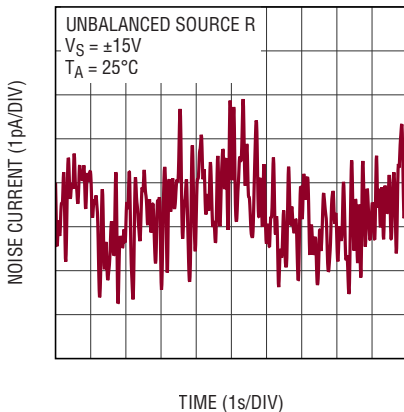
6370 G32

**0.1Hz to 10Hz Voltage Noise, G = 1000, RTI**



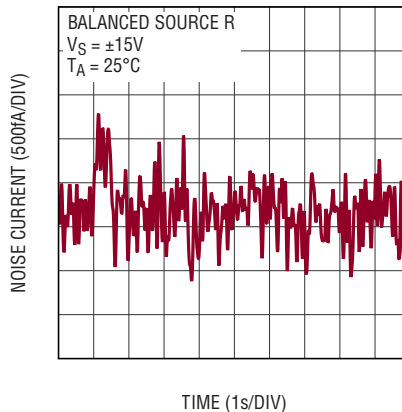
6370 G33

**0.1Hz to 10Hz Noise Current, Unbalanced Source R**



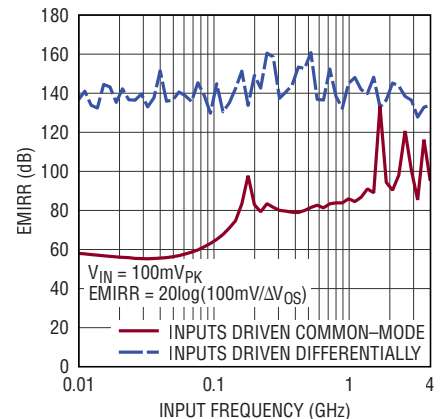
6370 G34

**0.1Hz to 10Hz Noise Current, Balanced Source R**



6370 G35

**EMIRR vs Frequency, RTI**

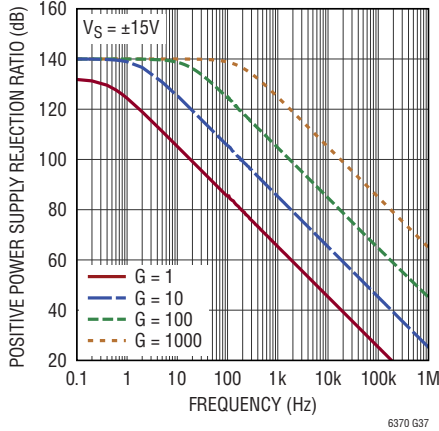


6370 G36

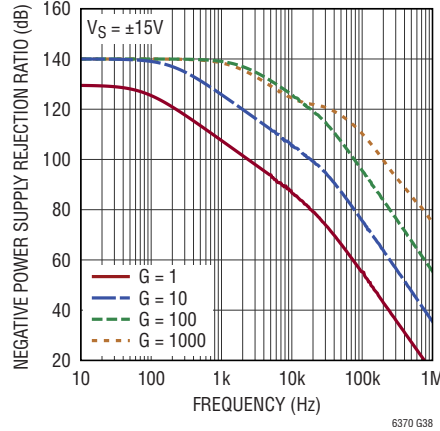
# TYPICAL PERFORMANCE CHARACTERISTICS

$V_S = \pm 15V$ ,  $V_{CM} = V_{REF} = 0V$ ,  $T_A = 25^\circ C$ ,  $R_L = 2k$ , unless otherwise noted.

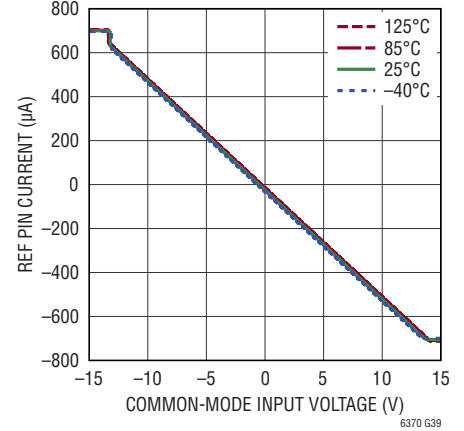
**Positive Power Supply Rejection Ratio vs Frequency**



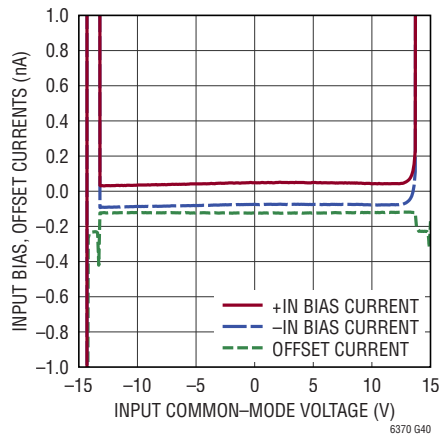
**Negative Power Supply Rejection Ratio vs Frequency**



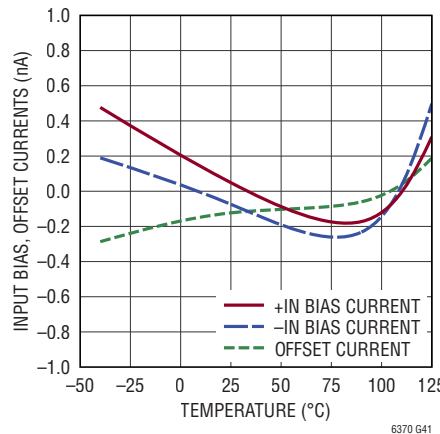
**REF Pin Current vs Input Common Mode Voltage**



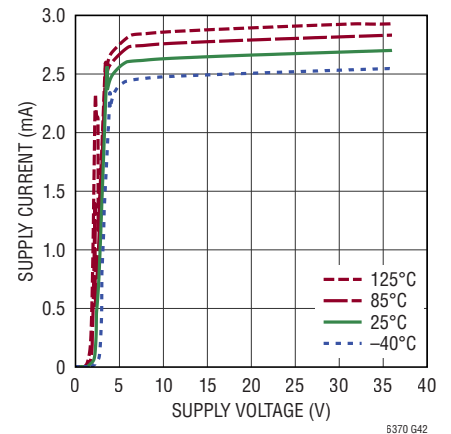
**Input Bias Current vs Common Mode Voltage**



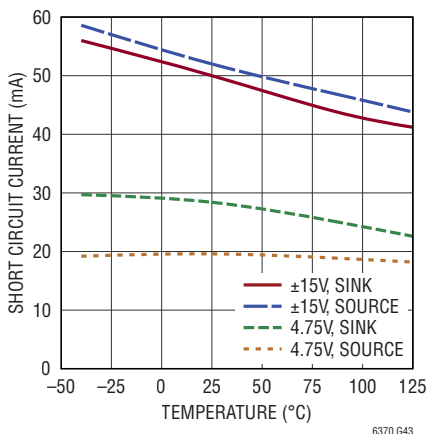
**Input Bias and Offset Current vs Temperature**



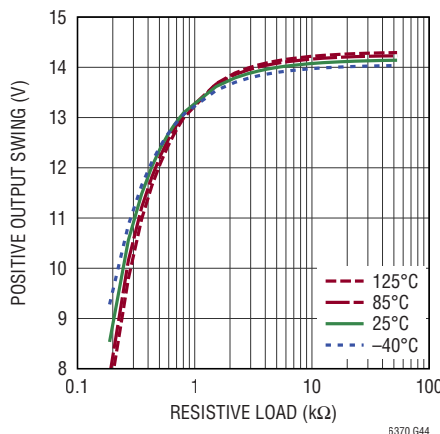
**Supply Current vs Supply Voltage**



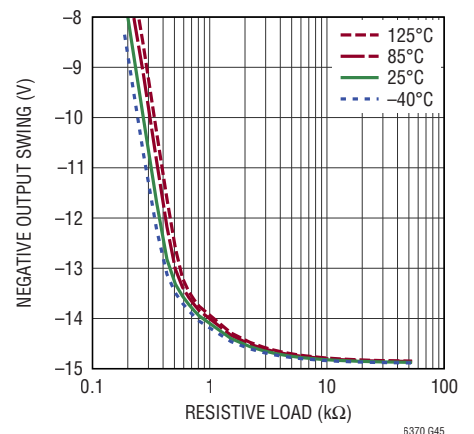
**Output Short Circuit Current vs Temperature**



**Output Voltage Swing vs Load Resistance**



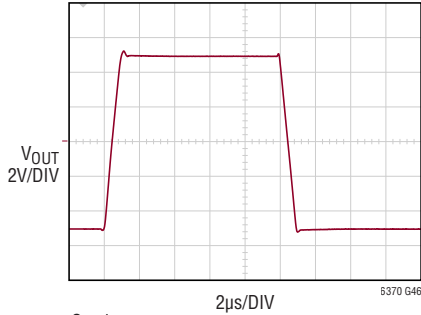
**Output Voltage Swing vs Load Resistance**



## TYPICAL PERFORMANCE CHARACTERISTICS

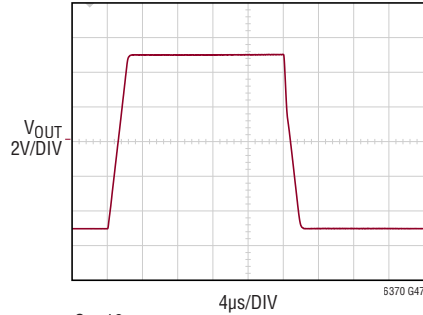
$V_S = \pm 15V$ ,  $V_{CM} = V_{REF} = 0V$ ,  $T_A = 25^\circ C$ ,  $R_L = 2k$ , unless otherwise noted.

**Large Signal Transient Response**



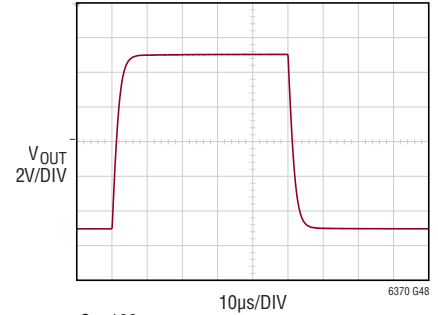
$G = 1$   
 $V_S = \pm 15V$   
 $T_A = 25^\circ C$   
 $C_L = 100pF$

**Large Signal Transient Response**



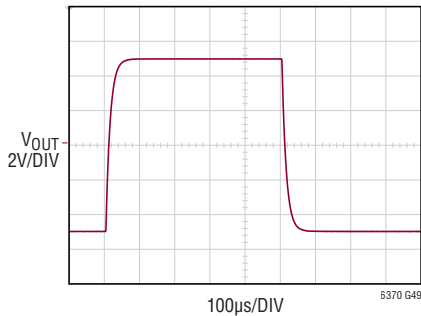
$G = 10$   
 $V_S = \pm 15V$   
 $T_A = 25^\circ C$   
 $C_L = 100pF$

**Large Signal Transient Response**



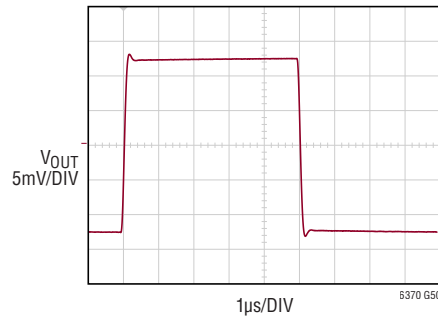
$G = 100$   
 $V_S = \pm 15V$   
 $T_A = 25^\circ C$   
 $C_L = 100pF$

**Large Signal Transient Response**



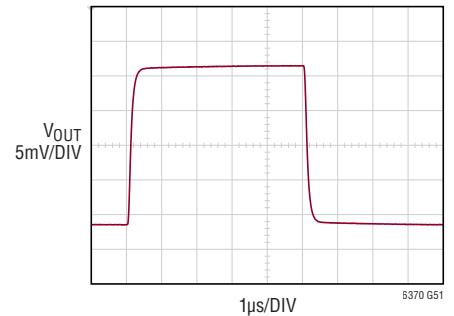
$G = 1000$   
 $V_S = \pm 15V$   
 $T_A = 25^\circ C$   
 $C_L = 100pF$

**Small Signal Transient Response**



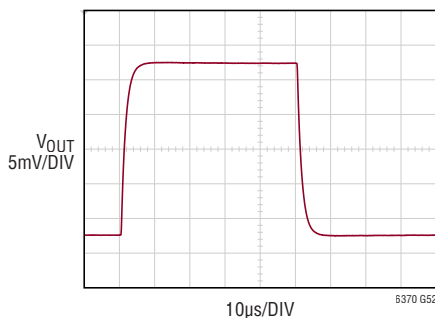
$G = 1$   
 $V_S = \pm 15V$   
 $T_A = 25^\circ C$   
 $C_L = 100pF$

**Small Signal Transient Response**



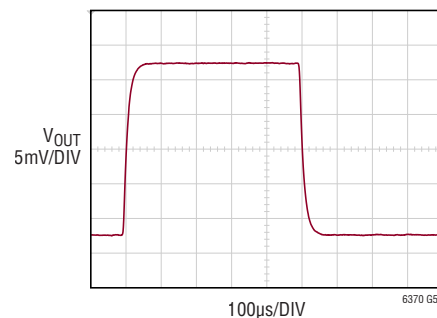
$G = 10$   
 $V_S = \pm 15V$   
 $T_A = 25^\circ C$   
 $C_L = 100pF$

**Small Signal Transient Response**



$G = 100$   
 $V_S = \pm 15V$   
 $T_A = 25^\circ C$   
 $C_L = 100pF$

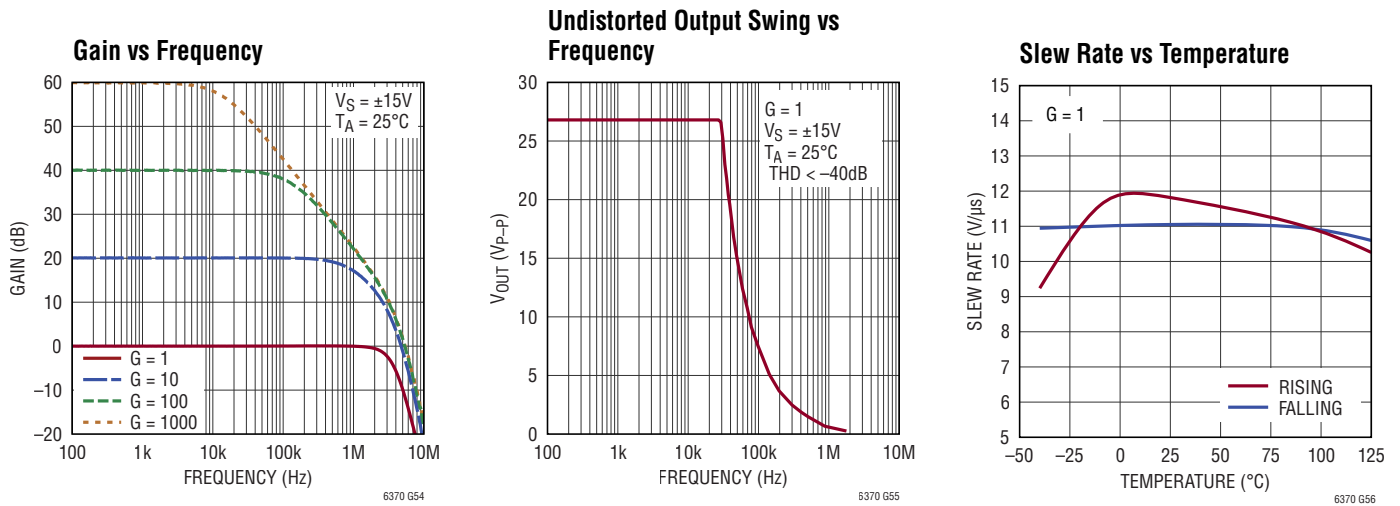
**Small Signal Transient Response**



$G = 1000$   
 $V_S = \pm 15V$   
 $T_A = 25^\circ C$   
 $C_L = 100pF$

## TYPICAL PERFORMANCE CHARACTERISTICS

$V_S = \pm 15V$ ,  $V_{CM} = V_{REF} = 0V$ ,  $T_A = 25^\circ C$ ,  $R_L = 2k$ , unless otherwise noted.



## PIN FUNCTIONS (MS/DFN/SOIC)

**-R<sub>G</sub> (Pin 1/Pin 1/Pin 1):** For use with an external gain setting resistor.

**-IN (Pin 2/Pin 3/Pin 2):** Negative Input Terminal. This input is high impedance.

**+IN (Pin 3/Pin 4/Pin 3):** Positive Input Terminal. This input is high impedance.

**V<sup>-</sup> (Pin 4/Pin 5/Pin 4):** Negative Power Supply. A bypass capacitor should be used between supply pins and ground.

**REF (Pin 5/Pin 6/Pin 5):** Reference for the output voltage.

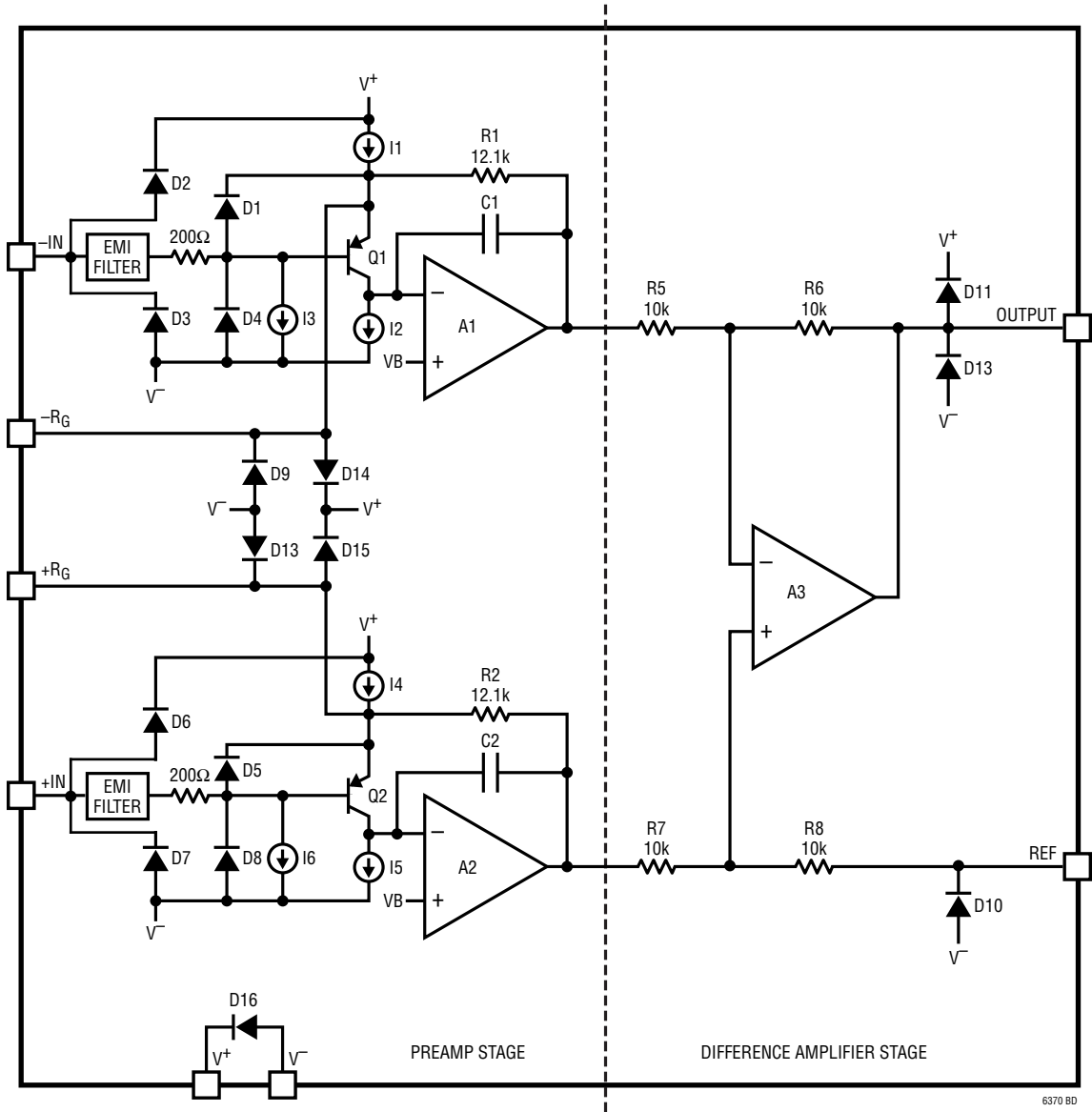
**OUTPUT (Pin 6/Pin 7/Pin 6):** Output voltage referenced to the REF pin.

**V<sup>+</sup> (Pin 7/Pin 8/Pin 7):** Positive Power Supply. A bypass capacitor should be used between supply pins and ground.

**+R<sub>G</sub> (Pin 8/Pin 10/Pin 8):** For use with an external gain setting resistor.

**NC (DFN Pins 2, 9):** No Internal Connection.

**SIMPLIFIED BLOCK DIAGRAM**



## THEORY OF OPERATION

The LT6370 is an improved version of the classic three op amp instrumentation amplifier topology. Laser trimming and proprietary monolithic construction allow for tight matching and extremely low drift of circuit parameters over the specified temperature range. Refer to the Simplified Block Diagram to aid in understanding the following circuit description. The collector currents in Q1 and Q2 as well as I1 and I4 are trimmed to minimize input offset voltage drift, thus assuring a high level of performance. R1 and R2 are trimmed to an absolute value of 12.1k to assure that the gain can be set accurately (0.08% at G = 100) with only one external resistor, R<sub>G</sub>. The value of R<sub>G</sub> determines the transconductance of the preamp stage. As R<sub>G</sub> is reduced to increase the programmed gain, the transconductance of the input preamp stage also increases to that of the input transistors Q1 and Q2. This causes the open-loop gain to increase when the programmed gain is increased, reducing the input related errors and noise. The input voltage noise at high gains is determined only by Q1 and Q2. At lower gains the noise of the difference amplifier and preamp gain setting resistors may increase the noise. The gain bandwidth product is determined by C1, C2 and the preamp transconductance, which increases with programmed gain. Therefore, the bandwidth is self-adjusting and does not drop directly proportional to gain.

The input transistors Q1 and Q2 offer excellent matching, drift and noise performance, which is due to using a proprietary high performance process, as well as low input bias current due to the high beta of these input devices. The input bias current is further reduced by trimming I3 and I6. The collector currents in Q1 and Q2 are held constant due to the feedback through the Q1-A1-R1 loop and Q2-A2-R2 loop. The action of the amplifier loops impresses the differential input voltage across the external gain set resistor R<sub>G</sub>. Since the current that flows through R<sub>G</sub> also flows through R1 and R2, the ratios provide a gained-up differential voltage,

$$G = 1 + \frac{R1 + R2}{R_G}$$

to the difference amplifier A3. The difference amplifier removes the common mode voltage and provides a single-ended output voltage referenced to the voltage on the REF pin. The offset voltage of the difference amplifier is trimmed to minimize output offset voltage drift, thus assuring a high level of performance, even in low gains. Resistors R5 to R8 are trimmed to maximize CMRR and minimize gain error. The resulting gain equation is:

$$G = 1 + \frac{24.2k}{R_G}$$

Solving for the gain set resistor gives:

$$R_G = \frac{24.2k}{G - 1}$$

Table 1 shows appropriate 1% resistor values for a variety of gains.

**Table 1. LT6370 Gain and R<sub>G</sub> Lookup.**

Resulting Gains for Various 1% Standard Resistor Values	
Gain	Standard 1% Resistor Value (Ω)
1	—
1.996	24.3k
5.007	6.04k
10.06	2.67k
20.06	1.27k
50.69	487
100.6	243
201	121
497.9	48.7
996.9	24.3
Convenient Integer Gains Using Various Standard 1% Resistor Values	
Integer Gain	Standard 1% Resistor Value (Ω)
1	—
3	12.1k
21	1.21k
23	1.1k
122	200
201	121
221	110
243	100
1211 (Note 2)	20

## APPLICATIONS INFORMATION

### Valid Input and Output Range

Instrumentation amplifiers traditionally specify a valid input common mode range and an output swing range. This however often fails to identify limitations associated with internal swing limits. Referring to the Simplified

Block Diagram, the output swing of pre-amplifiers A1 and A2 as well as the common-mode input range of the difference amplifier A3 impose limitations on the valid operating range. The following graphs show the operating region where a valid output is produced.

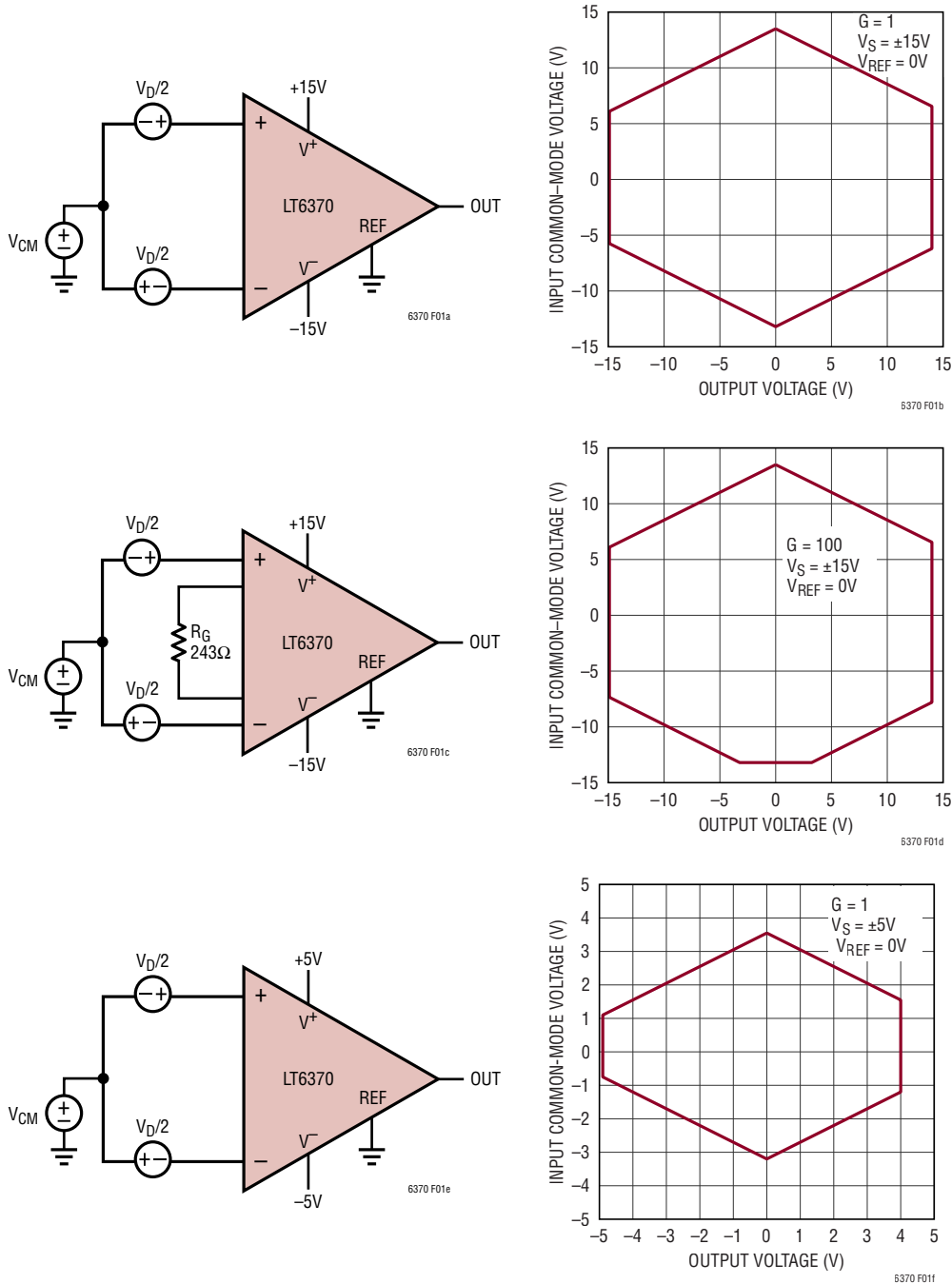


Figure 1. Input Common Mode Range vs Output Voltage



APPLICATIONS INFORMATION

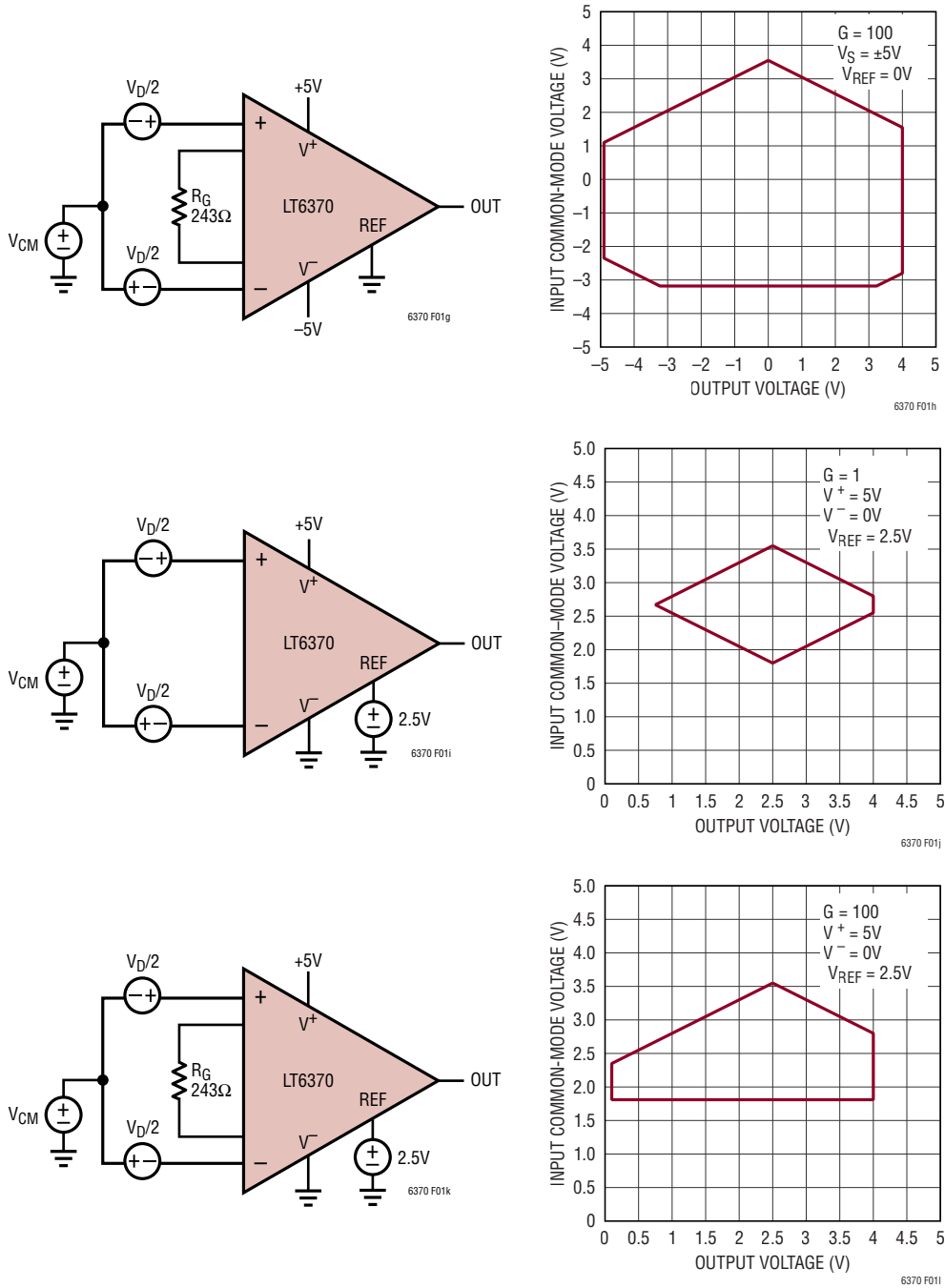


Figure 1 (Continued). Input Common Mode Range vs Output Voltage

## APPLICATIONS INFORMATION

### REF Pin

The REF pin has a nominal gain of 1 to the output. Resistance in series with the REF pin must be minimized to preserve high common mode rejection. For example, a series resistance of 2Ω from the REF pin to ground will not only increase the gain error by 0.02% but will lower the CMRR to 80dB. If this pin is driven by an amplifier as shown in Figure 2, the closed-loop output impedance of this amplifier at the desired frequency must also be low to avoid degrading the AC CMRR shown in the typical curves section.

It is also important to note that the drift in the circuitry used to drive the REF pin will result in an additional output drift term. Therefore, it may be important to consider the temperature accuracy of the circuitry used to drive the REF pin.

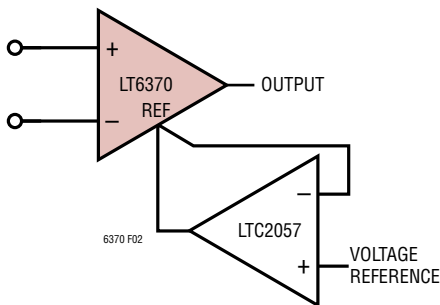


Figure 2. Buffering the REF Pin

### Input and Output Offset Voltage

The offset voltage of the LT6370 has two main components: the input offset voltage due to the input amplifiers and the output offset due to the output amplifier. The total offset voltage referred to the input (RTI) is found by dividing the output offset by the programmed gain and adding it to the input offset voltage. At high gains the input offset voltage dominates, whereas at low gains the output offset voltage dominates. The total offset voltage is:

$$\text{Total input offset voltage (RTI)} = V_{OSI} + V_{OSO}/G$$

$$\text{Total output offset voltage (RTO)} = V_{OSI} \cdot G + V_{OSO}$$

The preceding equations can also be used to calculate offset drift in a similar manner.

### Output Offset Trimming

The LT6370 is laser trimmed for low offset voltage so that no external offset trimming is required for most applications. In the event that the offset voltage needs to be adjusted, the circuit in Figure 3 is an example of an optional offset adjustment circuit. The op amp buffer provides a low impedance signal to the REF pin in order to achieve the best CMRR and lowest gain error.

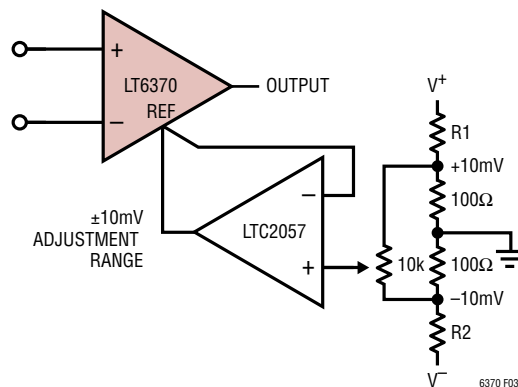


Figure 3. Optional Trimming of Output Offset Voltage

### Thermocouple Effects

In order to achieve accuracy on the microvolt level, thermocouple effects must be considered. Any connection of dissimilar metals forms a thermoelectric junction and generates a small temperature-dependent voltage. Also known as the Seebeck Effect, these thermal EMFs can be the dominant error source in low-drift circuits.

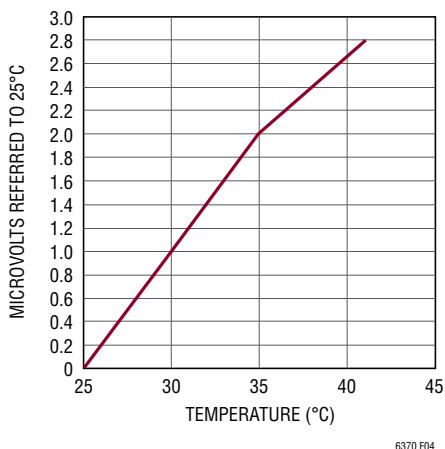
Connectors, switches, relay contacts, sockets, resistors, and solder are all candidates for significant thermal EMF generation. Even junctions of copper wire from different manufacturers can generate thermal EMFs of 200nV/°C, which is comparable to the maximum input offset voltage drift specification of the LT6370. Figures 4 and 5 illustrate the potential magnitude of these voltages and their sensitivity to temperature.

In order to minimize thermocouple-induced errors, attention must be given to circuit board layout and component selection. It is good practice to minimize the number of junctions in the amplifier's input and R<sub>G</sub> signal paths and avoid connectors, sockets, switches, and relays whenever possible. If such components are required, they should be

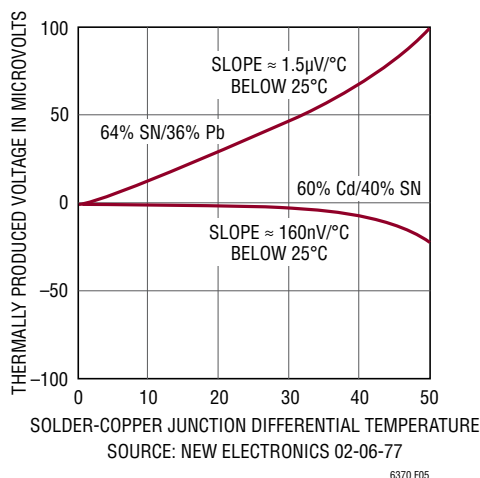
## APPLICATIONS INFORMATION

selected for low thermal EMF characteristics. Furthermore, the number, type, and layout of junctions should be matched for both inputs with respect to thermal gradients on the circuit board. Doing so may involve deliberately introducing dummy junctions to offset unavoidable junctions.

Air currents can also lead to thermal gradients and cause significant noise in measurement systems. It is important to prevent airflow across sensitive circuits. Doing so will often reduce thermocouple noise substantially. Placing PCB input traces close together, and on an internal PCB layer, can help minimize temperature differentials resulting from air currents reacting with the input trace thermal surface area.



**Figure 4. Thermal EMF Generated by Two Copper Wires From Different Manufacturers**

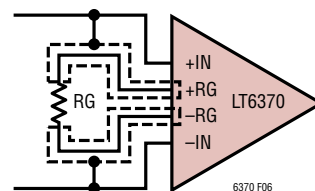


**Figure 5. Solder-Copper Thermal EMFs**

### Reducing Board-Related Leakage Effects

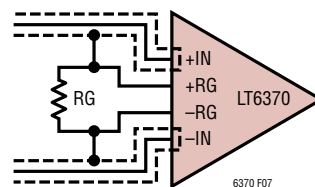
Leakage currents can have a significant impact on system accuracy, particularly in high temperature and high voltage applications. Quality insulation materials should be used, and insulating surfaces should be cleaned to remove fluxes and other residues. For humid environments, surface coating may be necessary to provide a moisture barrier.

Leakage into the  $R_G$  pin conducts through the on-chip feedback resistor, creating an error at the output of the pre-amplifiers. This error is independent of gain and degrades accuracy the most at low gains. This leakage can be minimized by encircling the  $R_G$  connections with a guard-ring operated at a potential very close to that of the  $R_G$  pins. The DFN package has NC pins adjacent to each  $R_G$  pin which can be used to simplify the implementation of this guard-ring. These NC pins do not provide any bias and have no internal connections. In some cases, the guard-ring can be connected to the input voltage which biases one diode drop below  $R_G$ .



**Figure 6. Guard-Rings Can Be Used to Minimize Leakage into the  $R_G$  Pins**

Leakage into the input pins reacts with the source resistance, creating an error directly at the input. This leakage can be minimized by encircling the input connections with a guard-rings operated at a potential very close to that of the input pins. In some cases, the guard-ring can be connected to  $R_G$  which biases one diode above the input.



**Figure 7. Guard-Rings Can Be Used to Minimize Leakage into the Input Pins**

## APPLICATIONS INFORMATION

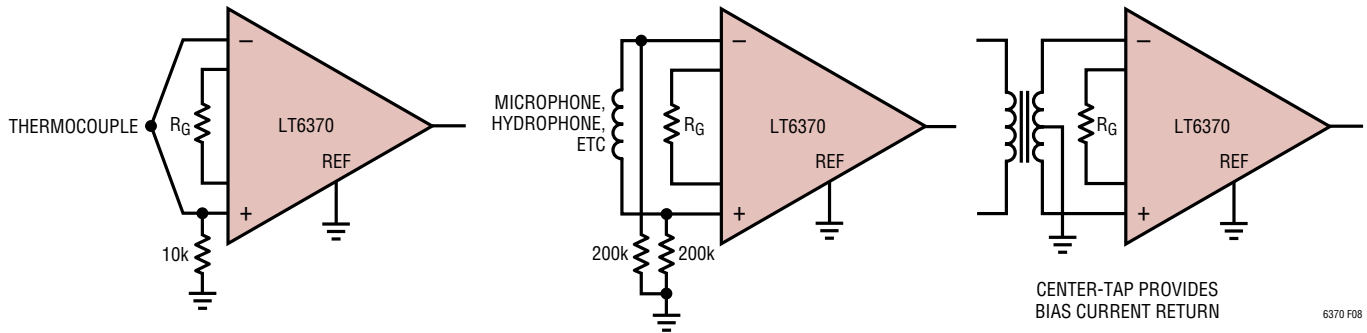


Figure 8. Providing an Input Common Mode Current Path

For the lowest leakage, amplifiers can be used to drive the guard ring. These buffers must have very low input bias current since that will now be a leakage.

### Input Bias Current Return Path

The low input bias current of the LT6370 (400pA max) and high input impedance (225GΩ) allow the use of high impedance sources without introducing additional offset voltage errors, even when the full common mode range is required. However, a path must be provided for the input bias currents of both inputs when a purely differential signal is being amplified. Without this path, the inputs will float to either rail and exceed the input common mode range of the LT6370, resulting in a saturated input amplifier. Figure 8 shows three examples of an input bias current path. The first example is of a purely differential signal source with a 10kΩ input current path to ground. Since the impedance of the signal source is low, only one resistor is needed. Two matching resistors are needed for higher impedance signal sources as shown in the second example. Balancing the input impedance improves both AC and DC common mode rejection and DC offset. The need for input resistors is eliminated if a center tap is present as shown in the third example.

### Input Protection

Additional input protection can be achieved by adding external resistors in series with each input. If low value resistors are needed, a clamp diode from the positive supply to each input will help improve robustness. A 2N4394 drain/source to gate is a good low leakage diode which can be used as shown in Figure 9. Robust input resistors should be chosen, such as carbon composite or bulk metal foil. Metal film and carbon film should not be used because of their poor performance.

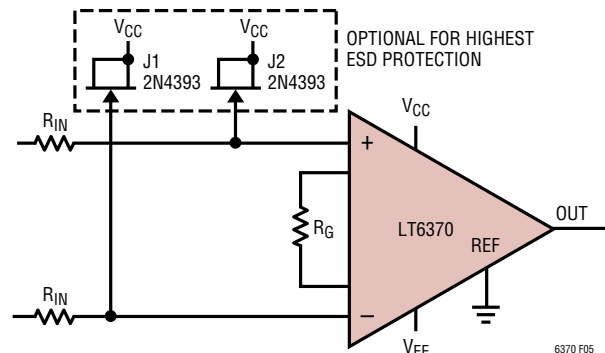


Figure 9. Input Protection

### Maintaining AC CMRR

To achieve optimum AC CMRR, it is important to balance the capacitance on the  $R_G$  gain setting pins. Furthermore, if the source resistance on each input is not equal, adding an additional resistance to one input to improve input source resistance matching will improve AC CMRR.

## APPLICATIONS INFORMATION

### RFI Reduction/Internal RFI Filter

In many industrial and data acquisition applications, the LT6370 will be used to amplify small signals accurately in the presence of large common mode voltages or high levels of noise. Typically, the sources of these very small signals (on the order of microvolts or millivolts) are sensors that can be a significant distance from the signal conditioning circuit. Although these sensors may be connected to signal conditioning circuitry using shielded or unshielded twisted-pair cabling, the cabling may act as an antenna, conveying very high frequency interference directly into the input stage of the LT6370.

The amplitude and frequency of the interference can have an adverse effect on an instrumentation amplifier's input stage by causing any unwanted DC shift in the amplifier's input offset voltage. This well known effect is called RFI rectification and is produced when out-of-band interference is coupled (inductively, capacitively or via radiation) and rectified by the instrumentation amplifier's input transistors. These transistors act as high frequency signal detectors, in the same way diodes were used as RF envelope detectors in early radio designs. Regardless of the type of interference or the method by which it is coupled into the circuit, an out-of-band error signal appears in series with the instrumentation amplifier's inputs.

To help minimize this effect, the LT6370 has 50MHz on-chip RFI filters to help attenuate high frequencies before they can interact with its input transistors. These on-chip filters are well matched due to their monolithic construction, which helps minimize any degradation in AC CMRR. To reduce the effect of these out-of-band signals on the input offset voltage of the LT6370 further, an additional external low-pass filter can be used at the inputs. The filter should be located very close to the input pins of the circuit. An effective filter configuration is illustrated in Figure 10, where three capacitors have been added to the inputs of the LT6370.

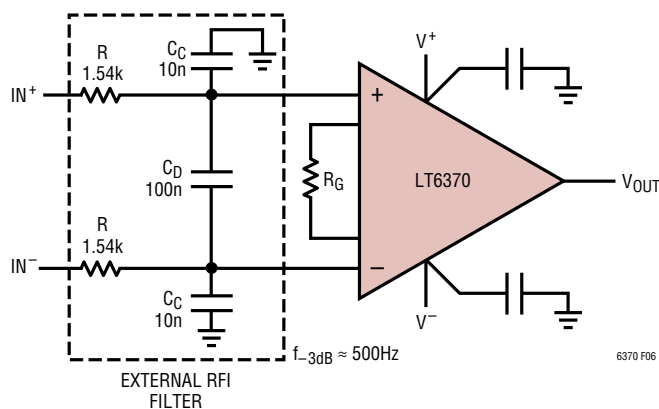
The filter limits the input signal according to the following relationship:

$$\text{FilterFreq}_{\text{DIFF}} = \frac{1}{2\pi R(2C_D + C_C)}$$

$$\text{FilterFreq}_{\text{CM}} = \frac{1}{2\pi RC_C}$$

where  $C_D \geq 10C_C$ .

$C_D$  affects the difference signal.  $C_C$  affects the common-mode signal. Any mismatch in  $R \times C_C$  degrades the LT6370 CMRR. To avoid inadvertently reducing CMRR-bandwidth performance, make sure that  $C_C$  is at least one order of magnitude smaller than  $C_D$ . The effect of mismatched  $C_C$ 's is reduced with a larger  $C_D:C_C$  ratio.



**Figure 10. Adding a Simple External RC Filter at the Inputs to an Instrumentation Amplifier Is Effective in Further Reducing Rectification of High Frequency Out-Of-Band Signals.**

To avoid any possibility of common mode to differential mode signal conversion, match the common mode low-pass filter on each input to 1% or better. Here are the steps to help determine appropriate values for the filter:

1. Pick R and  $C_D$  to have a low pass pole at least 10x higher than the highest signal of interest (e.g. 500Hz for a 50Hz signal) using:

$$\begin{aligned} \text{FilterFreq}_{\text{DIFF}} &= \frac{1}{2\pi R(2C_D + C_C)} \\ &= \frac{1}{2\pi R(2C_D + 0.1C_D)} \\ &= \frac{1}{4.2\pi RC_D} \end{aligned}$$

2. Select  $C_C = C_D/10$ .

## APPLICATIONS INFORMATION

If implemented this way, the common-mode pole frequency is placed about 20x higher than the differential pole frequency. Here are the differential and common-mode low pass pole frequencies for the values shown in Figure 10:

$$\text{FilterFreq}_{\text{DIFF}} = 500\text{Hz}$$

$$\text{FilterFreq}_{\text{CM}} = 10\text{kHz}$$

### Error Budget Analysis

The LT6370 offers performance superior to that of competing monolithic instrumentation amplifiers. A typical application that amplifies and buffers a bridge transducer's differential output is shown in Figure 11. The amplifier is set to a gain of 100 and amplifies a differential, full-scale transducer's output voltage of 20mV over the industrial temperature range. The LT6370 will be compared to other monolithic instrumentation amplifiers. As

shown, the LT6370 outperforms these other instrumentation amplifiers. The error budget comparison in Table 2 shows how various errors are calculated and how each error affects the total error budget. The table shows the clear benefit to low offset voltage, low offset voltage drift and low gain drift.

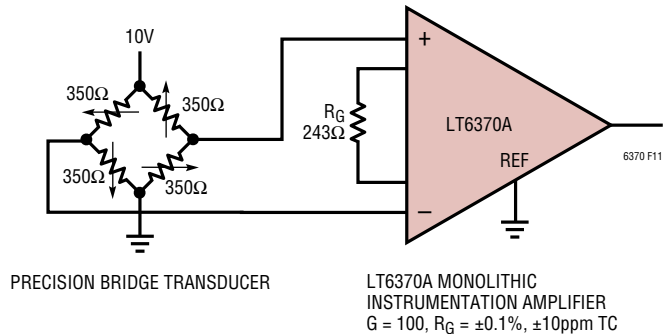


Figure 11. Precision Bridge Amplifier

Table 2. Error Budget Comparison

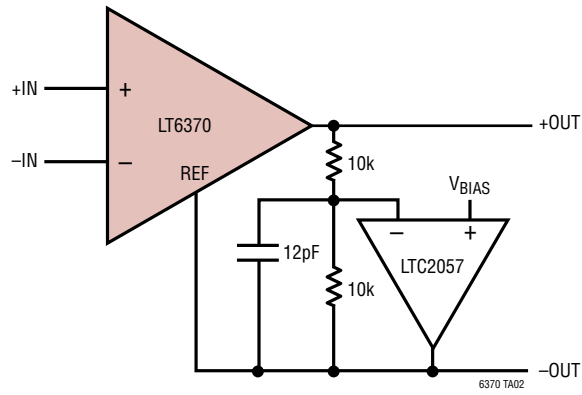
ERROR SOURCE	CALCULATION	ERROR, ppm OF FULL SCALE						
		LT6370A	IA1	IA2	IA3	IA4	IA5	IA6
<b>Absolute Accuracy at T<sub>A</sub> = 25°C</b>								
Gain Error, %	Gain Error in % • 10k + 1000	1800	2500	2500	2000	6000	2500	1800
Input Offset Voltage, μV	V <sub>OSI</sub> /20mV	1250	6250	1250	3500	2500	7500	3000
Output Offset Voltage, μV	[V <sub>OSO</sub> /100]/20mV	83	500	100	300	250	350	150
Input Offset Current, nA	[(I <sub>OS</sub> )(350)/2]/20mV	6.1	18	3.5	17.5	43.75	43.75	4
CMRR, dB	[(CMRR in ppm)(5V)/20mV	125	791	79	158	250	250	790
<b>Total Accuracy Error</b>		<b>3264.1</b>	<b>10059</b>	<b>3932.5</b>	<b>5975.5</b>	<b>9043.75</b>	<b>10643.75</b>	<b>5744</b>
<b>Drift to 85°C</b>								
Gain Drift, ppm/°C	(Gain Drift + 10ppm)(60°C)	2400	3600	3600	5400	6600	2700	3600
Input Offset Voltage Drift, μV/°C	[(V <sub>OSI</sub> Drift)(60°C)]/20mV	900	3000	900	2700	1500	6000	1200
Output Offset Voltage Drift, μV/°C	[(V <sub>OSO</sub> Drift)(60°C)]/100/20mV	45	450	150	270	600	300	180
<b>Total Drift Error</b>		<b>3345</b>	<b>7050</b>	<b>4650</b>	<b>8370</b>	<b>8700</b>	<b>9000</b>	<b>4980</b>
<b>Resolution</b>								
Gain Nonlinearity, ppm of Full Scale		30	40	15	10	20	5	15
Typ 0.1Hz to 10Hz Voltage Noise, μV <sub>p-p</sub>	(0.1Hz to 10Hz Noise)/20mV	10	14	12.5	3.5	10	26	14
<b>Total Resolution Error</b>		<b>40</b>	<b>54</b>	<b>27.5</b>	<b>13.5</b>	<b>30</b>	<b>31</b>	<b>29</b>
<b>Grand Total Error</b>		<b>6649.1</b>	<b>17163</b>	<b>8610</b>	<b>14359</b>	<b>17773.8</b>	<b>19674.8</b>	<b>10753</b>

G = 100

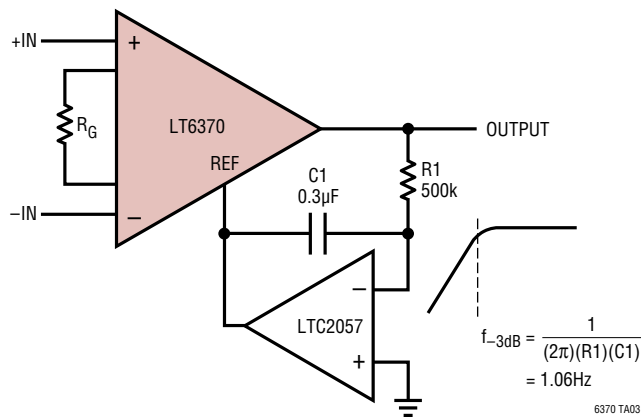
All errors are min/max and referred to input.

# TYPICAL APPLICATIONS

## Differential Output Instrumentation Amplifier

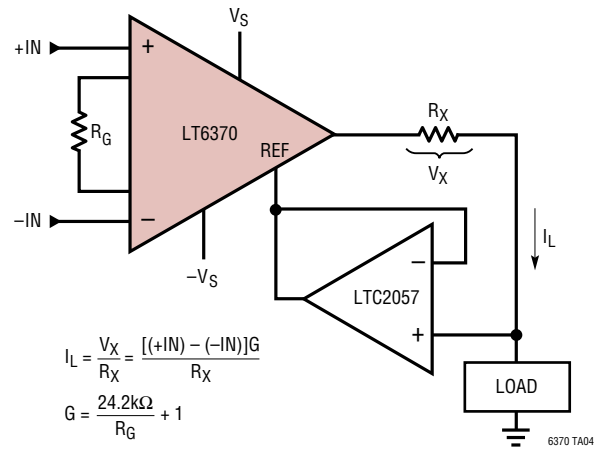


## AC Coupled Instrumentation Amplifier

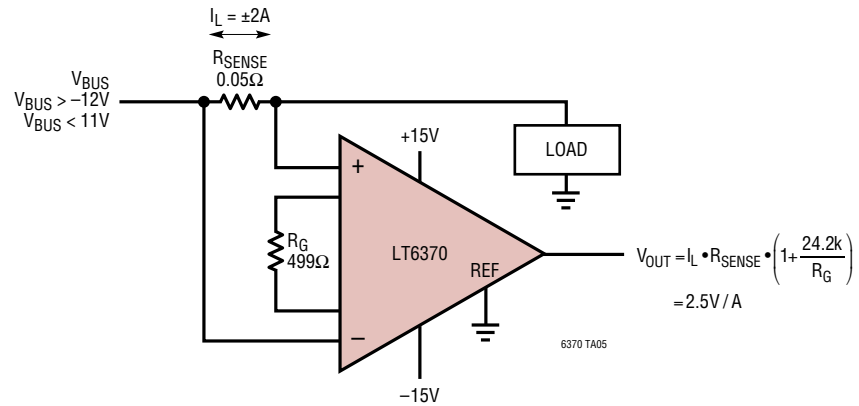


## TYPICAL APPLICATIONS

### Precision Voltage-to-Current Converter



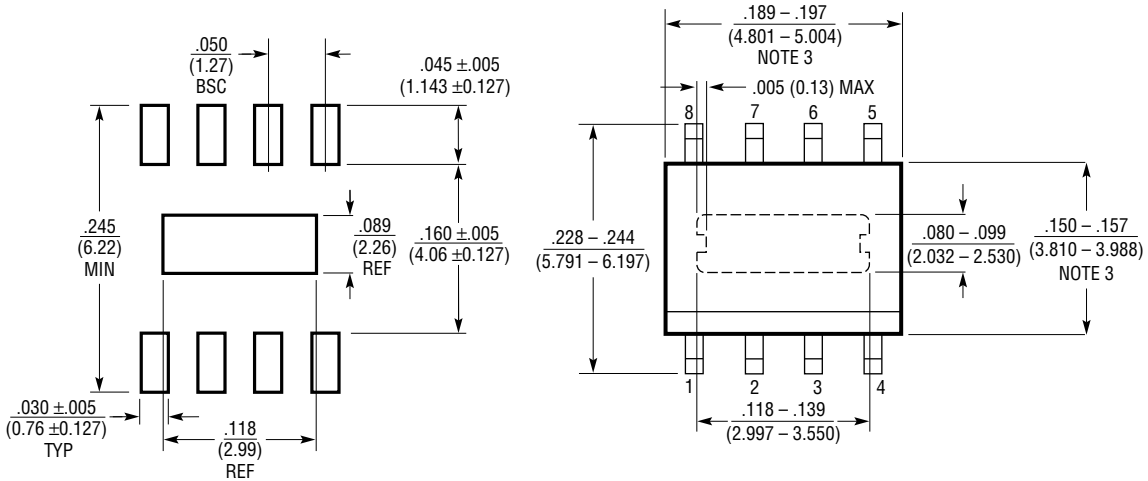
### High Side, Bidirectional Current Sense



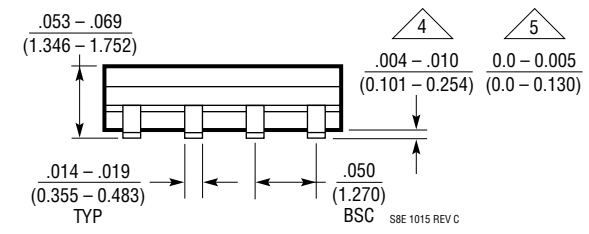
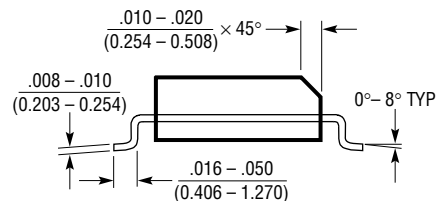


**PACKAGE DESCRIPTION**

**S8E Package**  
**8-Lead Plastic SOIC (Narrow .150 Inch) Exposed Pad**  
 (Reference LTC DWG # 05-08-1857 Rev C)



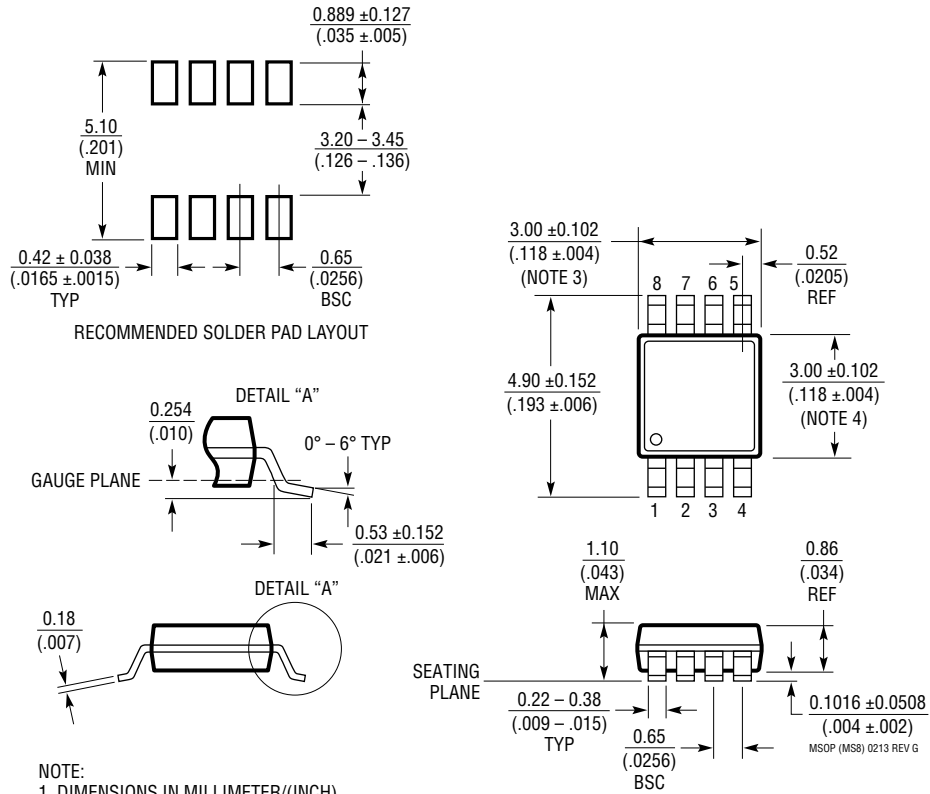
RECOMMENDED SOLDER PAD LAYOUT



- NOTE:  
 1. DIMENSIONS IN  $\frac{\text{INCHES}}{\text{MILLIMETERS}}$   
 2. DRAWING NOT TO SCALE  
 3. THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS.  
 MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED .010" (0.254mm)  
 4. STANDARD LEAD STANDOFF IS 4mils TO 10mils (DATE CODE BEFORE 542)  
 5. LOWER LEAD STANDOFF IS 0mils TO 5mils (DATE CODE AFTER 542)

**PACKAGE DESCRIPTION**

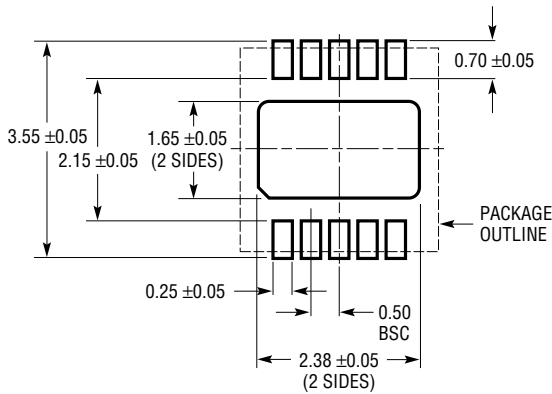
**MS8 Package**  
**8-Lead Plastic MSOP**  
 (Reference LTC DWG # 05-08-1660 Rev G)



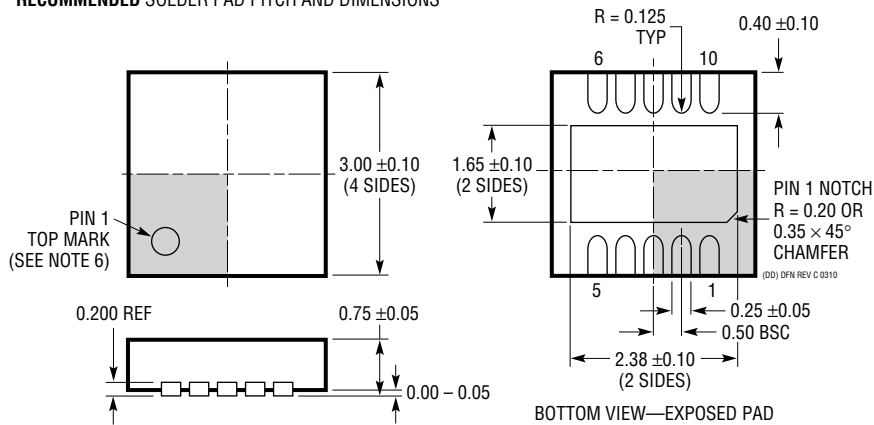
- NOTE:
1. DIMENSIONS IN MILLIMETER/(INCH)
  2. DRAWING NOT TO SCALE
  3. DIMENSION DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS.  
MOLD FLASH, PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.152mm (.006") PER SIDE
  4. DIMENSION DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS.  
INTERLEAD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.152mm (.006") PER SIDE
  5. LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.102mm (.004") MAX

**PACKAGE DESCRIPTION**

**DD Package**  
**10-Lead Plastic DFN (3mm × 3mm)**  
 (Reference LTC DWG # 05-08-1699 Rev C)



**RECOMMENDED SOLDER PAD PITCH AND DIMENSIONS**



- NOTE:
1. DRAWING TO BE MADE A JEDEC PACKAGE OUTLINE MO-229 VARIATION OF (WEED-2). CHECK THE LTC WEBSITE DATA SHEET FOR CURRENT STATUS OF VARIATION ASSIGNMENT
  2. DRAWING NOT TO SCALE
  3. ALL DIMENSIONS ARE IN MILLIMETERS
  4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE
  5. EXPOSED PAD SHALL BE SOLDER PLATED
  6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE TOP AND BOTTOM OF PACKAGE