

# LTC4075/LTC4075X

# Dual Input USB/AC Adapter Standalone Li-Ion Battery Chargers

- **Charges Single-Cell Li-Ion Batteries from Wall Adapter and USB Inputs**
- **Automatic Input Power Detection and Selection**
- **Charge Current Programmable up to 950mA from Wall Adapter Input**
- **No External MOSFET, Sense Resistor or Blocking Diode Needed**
- Thermal Regulation Maximizes Charging Rate Without Risk of Overheating\*
- Preset Charge Voltage with ±0.6% Accuracy
- Programmable Charge Current Termination
- 18µA USB Suspend Current in Shutdown
- Independent "Power Present" Status Outputs
- Charge Status Output
- Automatic Recharge
- Available Without Trickle Charge (LTC4075X)
- Available in a Thermally Enhanced, Low Profile (0.75mm) 10-Lead (3mm  $\times$  3mm) DFN Package

# **APPLICATIONS**

- Cellular Telephones
- Handheld Computers
- Portable MP3 Players
- Digital Cameras

# **FEATURES DESCRIPTIO <sup>U</sup>**

The LTC®4075/LTC4075X are standalone linear chargers that are capable of charging a single-cell Li-Ion battery from both wall adapter and USB inputs. The chargers can detect power at the inputs and automatically select the appropriate power source for charging.

No external sense resistor or blocking diode is required for charging due to the internal MOSFET architecture. Internal thermal feedback regulates the battery charge current to maintain a constant die temperature during high power operation or high ambient temperature conditions. The float voltage is fixed at 4.2V and the charge current is programmed with an external resistor. The LTC4075 terminates the charge cycle when the charge current drops below the programmed termination threshold after the final float voltage is reached. With power applied to both inputs, the LTC4075/LTC4075X can be put into shutdown mode reducing the DCIN supply current to 20µA, the USBIN supply current to 10µA, and the battery drain current to less than 2µA.

Other features include automatic recharge, undervoltage lockout, charge status outputs, and "power present" status outputs to indicate the presence of wall adapter or USB power.

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# **TYPICAL APPLICATIO U**

**Dual Input Battery Charger for Single-Cell Li-Ion**



#### **Complete Charge Cycle (1100mAh Battery)**





**(Note 1)**



# **ABSOLUTE MAXIMUM RATINGS PACKAGE/ORDER INFORMATION**



Consult LTC Marketing for parts specified with wider operating temperature ranges.

#### **The** ● **denotes the specifi cations which apply over the full operating**  temperature range, otherwise specifications are at T<sub>A</sub> = 25°C. V<sub>DCIN</sub> = 5V, V<sub>USBIN</sub> = 5V unless otherwise noted. **ELECTRICAL CHARACTERISTICS**





### **ELECTRICAL CHARACTERISTICS** The  $\bullet$  denotes the specifications which apply over the full operating

temperature range, otherwise specifications are at  $T_A = 25^{\circ}$ C.  $V_{DCIN} = 5V$ ,  $V_{USBIN} = 5V$  unless otherwise noted.



**Note 1:** Absolute Maximum Ratings are those values beyond which the life of a device may be impaired.

**Note 2:** The LTC4075E/LTC4075XE are guaranteed to meet the performance specifications from 0°C to 70°C. Specifications over the –40°C to 85°C operating temperature range are assured by design, characterization and correlation with statistical process controls.

**Note 3:** Failure to correctly solder the exposed backside of the package to the PC board will result in a thermal resistance much higher than 40°C/W. See Thermal Considerations.

**Note 4:** Supply current includes IDC and ITERM pin current (approximately 100µA each) but does not include any current delivered to the battery through the BAT pin.

**Note 5:** Supply current includes IUSB and ITERM pin current (approximately 100µA each) but does not include any current delivered to the battery through the BAT pin.

**Note 6:** This parameter is not applicable to the LTC4075X.

**Note 7:** Guaranteed by long term current density limitations.



# **TYPICAL PERFORMANCE CHARACTERISTICS**



4075X G08

0

 $V_{CHRG}$  (V) 0 1 2 3 4 5 6 7

4075Xfa



VUSBPWR (V)

3 5

1 2 3 4 5 6 7

 $\pmb{0}$ 

VPWR (V)

3 5

1 2 3 4 5 6 7

4075X G07

### **TYPICAL PERFORMANCE CHARACTERISTICS**



**DCIN Power FET "On" Resistance vs Temperature**



**DCIN Shutdown Current vs Temperature**





**USBIN Power "On" Resistance vs Temperature**



**USBIN Shutdown Current vs Temperature**







#### **ENABLE Pin Threshold (On-to-Off) vs Temperature**



**ENABLE Pin Pulldown Resistance vs Temperature**



4075Xfa



# **TYPICAL PERFORMANCE CHARACTERISTICS**









**Charge Current During Turn-On and Turn-Off**





# **PIN FUNCTIONS**

**USBIN (Pin 1):** USB Input Supply Pin. Provides power to the battery charger. The maximum supply current is 650mA. This pin should be bypassed with a 1µF capacitor.

**IUSB (Pin 2):** Charge Current Program for USB Power. The charge current is set by connecting a resistor,  $R_{\text{HJSB}}$ , to ground. When charging in constant-current mode, this pin servos to 1V. The voltage on this pin can be used to measure the battery current delivered from the USB input using the following formula:

$$
I_{BAT} = \frac{V_{IUSE}}{R_{IUSE}} \cdot 1000
$$

**ITERM (Pin 3):** Termination Current Threshold Program. The termination current threshold, ITERMINATE, is set by connecting a resistor,  $R_{\text{ITERM}}$ , to ground. I<sub>TERMINATE</sub> is set by the following formula:

$$
I_{\text{TERMINATE}} = \frac{100V}{R_{\text{ITERM}}}
$$

When the battery current,  $I_{BAT}$ , falls below the termination threshold, charging stops and the CHRG output becomes high impedance.

This pin is internally clamped to approximately 1.5V. Driving this pin to voltages beyond the clamp voltage can draw large currents and should be avoided.

⎯ **PWR (Pin 4):** Open-Drain Power Supply Status Output. When the DCIN or USBIN pin voltage is sufficient to begin charging (i.e. when the supply is greater than the undervoltage lockout threshold and at least 180mV above the battery terminal), the PWR pin is pulled low by an internal M-channel MOSFET. Otherwise **PWR** is high impedance. This output is capable of sinking up to 10mA, making it suitable for driving an LED.

 $\overline{\phantom{a}}$ **CHRG (Pin 5):** Open-Drain Charge Status Output. When **the LTC4075** is charging, the CHRG pin is pulled low by an internal N-channel MOSFET. When the charge cycle is an internal is enalmer moor ET. When the enarge eyere is<br>completed, CHRG becomes high impedance. This output is capable of sinking up to 10mA, making it suitable for driving an LED.

**ENABLE (Pin 6):** Enable Input. When the LTC4075 is charging from the DCIN source, a logic low on this pin enables the charger. When the LTC4075 is charging from the USBIN source, a logic high on this pin enables the charger. If this input is left floating, an internal  $2M\Omega$ pulldown resistor defaults the LTC4075 to charge when a wall adapter is applied and to shut down if only the USB source is applied.

**USBPWR (Pin 7):** Open-Drain USB Power Status Output. When the voltage on the USBIN pin is sufficient to begin charging and there is insufficient power at DCIN, the USB-PWR pin is high impedance. In all other cases, this pin is pulled low by an internal N-channel MOSFET, provided that there is power present at the DCIN, USBIN, or BAT inputs. This output is capable of sinking up to 1mA, making it suitable for driving high impedance logic inputs.

**IDC (Pin 8):** Charge Current Program for Wall Adapter Power. The charge current is set by connecting a resistor,  $R_{IDC}$ , to ground. When charging in constant-current mode, this pin servos to 1V. The voltage on this pin can be used to measure the battery current delivered from the DC input using the following formula:

$$
I_{BAT} = \frac{V_{IDC}}{R_{IDC}} \cdot 1000
$$

**BAT (Pin 9):** Charger Output and Regulator Input. This pin provides charge current to the battery and regulates the final float voltage to 4.2V.

**DCIN (Pin 10):** Wall Adapter Input Supply Pin. Provides power to the battery charger. The maximum supply current is 950mA. This should be bypassed with a  $1\mu$ F capacitor.

**Exposed Pad (Pin 11):** GND. The exposed backside of the package is ground and must be soldered to PC board ground for electrical connection and maximum heat transfer.



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# LTC4075/LTC4075X

# **BLOCK DIAGRAM**





1EAR

## **OPERATION**

The LTC4075 is designed to efficiently manage charging of a single-cell lithium-ion battery from two separate power sources: a wall adapter and USB power bus. Using the constant-current/constant-voltage algorithm, the charger can deliver up to 950mA of charge current from the wall adapter supply or up to 650mA of charge current from the USB supply with a final float voltage accuracy of  $\pm 0.6\%$ . The LTC4075 has two internal P-channel power MOSFETs and thermal regulation circuitry. No blocking diodes or external sense resistors are required.

### **Power Source Selection**

The LTC4075 can charge a battery from either the wall adapter input or the USB port input. The LTC4075 automatically senses the presence of voltage at each input. If both power sources are present, the LTC4075 defaults to the wall adapter source provided sufficient power is present at the DCIN input. "Sufficient power" is defined as:

- Supply voltage is greater than the UVLO threshold.
- Supply voltage is greater than the battery voltage by 50mV (180mV rising, 50mV falling).

The open drain power status outputs (PWR and USBPWR) indicate which power source has been selected. Table 1 describes the behavior of these status outputs.

#### **Table 1. Power Source Selection**



### **Programming and Monitoring Charge Current**

The charge current delivered to the battery from the wall adapter supply is programmed using a single resistor from the IDC pin to ground. Likewise, the charge current from the USB supply is programmed using a single resistor from the IUSB pin to ground. The program resistor and the charge current ( $I_{CHRG}$ ) are calculated using the following equations:

$$
R_{IDC} = \frac{1000V}{I_{CHRG-DC}}, I_{CHRG-DC} = \frac{1000V}{R_{IDC}}
$$

$$
R_{IUSB} = \frac{1000V}{I_{CHRG-USB}}, I_{CHRG-USB} = \frac{1000V}{R_{IUSB}}
$$

Charge current out of the BAT pin can be determined at any time by monitoring the IDC or IUSB pin voltage and using the following equations:

$$
I_{BAT} = \frac{V_{IDC}}{R_{IDC}} \cdot 1000, \text{ (charging from wall adapter)}
$$
  

$$
I_{BAT} = \frac{V_{IUSE}}{R_{IUSE}} \cdot 1000, \text{ (charging from USB supply)}
$$

### **Programming Charge Termination**

The charge cycle terminates when the charge current falls below the programmed termination threshold during constant-voltage mode. This threshold is set by connecting an external resistor,  $R_{\text{ITERM}}$ , from the ITERM pin to ground. The charge termination current threshold  $(I_{TFRMIMATE})$  is set by the following equation:

$$
R_{ITERM} = \frac{100V}{I_{TERMINATE}}, I_{TERMINATE} = \frac{100V}{R_{ITERM}}
$$

# **OPERATION**

The termination condition is detected by using an internal filtered comparator to monitor the ITERM pin. When the ITERM pin voltage drops below 100mV\* for longer than  $t_{TFRMIMATE}$  (typically 1.5ms), charging is terminated. The charge current is latched off and the LTC4075 enters standby mode.

When charging, transient loads on the BAT pin can cause the ITERM pin to fall below 100mV for short periods of time before the DC charge current has dropped below the programmed termination current. The 1.5ms filter time  $(t_{\text{TFRMIMATE}})$  on the termination comparator ensures that transient loads of this nature do not result in premature charge cycle termination. Once the *average* charge current drops below the programmed termination threshold, the LTC4075 terminates the charge cycle and ceases to provide any current out of the BAT pin. In this state, any load on the BAT pin must be supplied by the battery.

### **Low Battery Charge Conditioning (Trickle Charge)**

This feature ensures that near-dead batteries are gradually charged before reapplying full charge current . If the BAT pin voltage is below 2.9V, the LTC4075 supplies 1/10th of the full charge current to the battery until the BAT pin rises back above 2.9V. For example, if the charger is programmed to charge at 800mA from the wall adapter input and 500mA from the USB input, the charge current during trickle charge mode would be 80mA and 50mA, respectively.

The LTC4075X does not include the trickle charge feature; it outputs full charge current to the battery when the BAT pin voltage is below 2.9V. The LTC4075X is useful in applications where the trickle charge current may be insufficient to supply the load during low battery voltage conditions.

### **Automatic Recharge**

In standby mode, the charger sits idle and monitors the battery voltage using a comparator with a 6ms filter time  $(t_{\text{RFCHRG}})$ . A charge cycle automatically restarts when the battery voltage falls below 4.1V (which corresponds to approximately 80%-90% battery capacity). This ensures that the battery is kept at, or near, a fully charged condi-

\*Any external sources that hold the ITERM pin above 100mV will prevent the LTC4075 from terminating a charge cycle.

If the battery is removed from the charger, a sawtooth waveform of approximately 100mV appears at the battery output. This is caused by the repeated cycling between termination and recharge events. This cycling results in pulsing at the CHRG output; an LED connected to this pin will exhibit a blinking pattern, indicating to the user that a battery is not present. The frequency of the sawtooth is dependent on the amount of output capacitance.

### **Manual Shutdown**

The ENABLE pin has a 2MΩ pulldown resistor to GND. The definition of this pin depends on which source is supplying power. When the wall adapter input is supplying power, logic low enables the charger and logic high disables it (the pulldown defaults the charger to the charging state). The opposite is true when the USB input is supplying power; logic low disables the charger and logic high enables it (the default is the shutdown state).

The DCIN input draws 20µA when the charger is in shutdown. The USBIN input draws 18µA during shutdown if no power is applied to DCIN, but draws only 10µA when  $V<sub>DCIN</sub> > V<sub>USBIN</sub>$ .

### **Charge Current Soft-Start and Soft-Stop**

The LTC4075 includes a soft-start circuit to minimize the inrush current at the start of a charge cycle. When a charge cycle is initiated, the charge current ramps from zero to full-scale current over a period of 250µs. Likewise, internal circuitry slowly ramps the charge current from full-scale to zero in a period of approximately 30µs when the charger shuts down or self terminates. This minimizes the transient current load on the power supply during start-up and shut-off.

### **Status Indicators**

The charge status output (CHRG) has two states: pull-down and high impedance. The pull-down state indicates that the LTC4075 is in a charge cycle. Once the charge cycle has terminated or the LTC4075 is disabled, the pin state becomes high impedance. The pull-down state is capable of sinking up to 10mA.



# **OPERATION**

The power supply status output ( $\overline{\text{PWR}}$ ) has two states: pulldown and high impedance. The pull-down state indicates that power is present at either DCIN or USBIN. This output is strong enough to drive an LED. If no power is applied at either pin, the PWR pin is high impedance, indicating that the LTC4075 lacks sufficient power to charge the battery. The pull-down state is capable of sinking up to 10mA.

The USB power status output (USBPWR) has two states: pull-down and high impedance. The high impedance state indicates that the LTC4075 is being powered from the USBIN input. The pull-down state indicates that the charger is either powered from DCIN or is in a UVLO condition (see Table 1). The pull-down state is capable of sinking up to 1mA.

### **Thermal Limiting**

An internal thermal feedback loop reduces the programmed charge current if the die temperature attempts to rise above a preset value of approximately 105°C. This feature protects the LTC4075 from excessive temperature and allows the user to push the limits of the power handling capability of a given circuit board without risk of damaging the device. The charge current can be set according to typical (not worst-case) ambient temperature with the assurance that the charger will automatically reduce the current in worstcase conditions. DFN power considerations are discussed further in the Applications Information section.





# **APPLICATIONS INFORMATION**

### **Using a Single Charge Current Program Resistor**

The LTC4075 can program the wall adapter charge current and USB charge current independently using two program resistors,  $R_{\text{IDC}}$  and  $R_{\text{HISR}}$ . Figure 2 shows a charger circuit that sets the wall adapter charge current to 800mA and the USB charge current to 500mA.



**Figure 2. Full Featured Dual Input Charger Circuit**

In applications where the programmed wall adapter charge current and USB charge current are the same, a single program resistor can be used to set both charge currents. Figure 3 shows a charger circuit that uses one charge current program resistor.



**Figure 3. Dual Input Charger Circuit. The Wall Adapter Charge Current and USB Charge Current are Both Programmed to be 500mA**

In this circuit, the programmed charge current from both the wall adapter supply is the same value as the programmed charge current from the USB supply:

$$
I_{CHRG-DC} = I_{CHRG-USB} = \frac{1000V}{R_{ISET}}
$$

### **Stability Considerations**

The constant-voltage mode feedback loop is stable without any compensation provided a battery is connected to the charger output. However, a 1µF capacitor with a 1 $\Omega$  series resistor is recommended at the BAT pin to keep the ripple voltage low when the battery is disconnected.

When the charger is in constant-current mode, the charge current program pin (IDC or IUSB) is in the feedback loop, not the battery. The constant-current mode stability is affected by the impedance at the charge current program pin. With no additional capacitance on this pin, the charger is stable with program resistor values as high as 20k  $(I_{CHRG} = 50 \text{mA})$ ; however, additional capacitance on these nodes reduces the maximum allowed program resistor.

### **Power Dissipation**

When designing the battery charger circuit, it is not necessary to design for worst-case power dissipation scenarios because the LTC4075 automatically reduces the charge current during high power conditions. The conditions that cause the LTC4075 to reduce charge current through thermal feedback can be approximated by considering the power dissipated in the IC. Most of the power dissipation is generated from the internal charger MOSFET. Thus, the power dissipation is calculated to be:

$$
P_D = (V_{IN} - V_{BAT}) \bullet I_{BAT}
$$



### **APPLICATIONS INFORMATION**

 $P_D$  is the power dissipated,  $V_{IN}$  is the input supply voltage (either DCIN or USBIN),  $V_{BAT}$  is the battery voltage and  $I<sub>BAT</sub>$  is the charge current. The approximate ambient temperature at which the thermal feedback begins to protect the IC is:

$$
T_A = 105^{\circ}\text{C} - \text{P}_\text{D} \cdot \text{\theta}_{\text{JA}}
$$

$$
T_A = 105^{\circ}\text{C} - (\text{V}_{\text{IN}} - \text{V}_{\text{BAT}}) \cdot \text{I}_{\text{BAT}} \cdot \text{\theta}_{\text{JA}}
$$

Example: An LTC4075 operating from a 5V wall adapter (on the DCIN input) is programmed to supply 800mA full-scale current to a discharged Li-Ion battery with a voltage of 3.3V. Assuming  $\theta_{JA}$  is 40°C/W (see Thermal Considerations), the ambient temperature at which the LTC4075 will begin to reduce the charge current is approximately:

$$
T_A = 105^{\circ}\text{C} - (5\text{V} - 3.3\text{V}) \cdot (800\text{mA}) \cdot 40^{\circ}\text{C/W}
$$

$$
T_A = 105^{\circ}\text{C} - 1.36\text{W} \cdot 40^{\circ}\text{C/W} = 105^{\circ}\text{C} - 54.4^{\circ}\text{C}
$$

$$
T_A = 50.6^{\circ}\text{C}
$$

The LTC4075 can be used above 50.6°C ambient, but the charge current will be reduced from 800mA. The approximate current at a given ambient temperature can be approximated by:

$$
I_{BAT} = \frac{105^{\circ}C - T_A}{(V_{IN} - V_{BAT}) \cdot \theta_{JA}}
$$

Using the previous example with an ambient temperature of 60°C, the charge current will be reduced to approximately:

$$
I_{BAT} = \frac{105\degree C - 60\degree C}{(5V - 3.3V) \cdot 40\degree C / W} = \frac{45\degree C}{68\degree C / A}
$$
  

$$
I_{BAT} = 662mA
$$

It is important to remember that LTC4075 applications do not need to be designed for worst-case thermal conditions, since the IC will automatically reduce power dissipation when the junction temperature reaches approximately 105°C.

### **Thermal Considerations**

In order to deliver maximum charge current under all conditions, it is critical that the exposed metal pad on the backside of the LTC4075 package is properly soldered to the PC board ground. When correctly soldered to a 2500mm2 double sided 1oz copper board, the LTC4075 has a thermal resistance of approximately 40°C/W. Failure to make thermal contact between the exposed pad on the backside of the package and the copper board will result in thermal resistances far greater than 40°C/W. As an example, a correctly soldered LTC4075 can deliver over 800mA to a battery from a 5V supply at room temperature. Without a good backside thermal connection, this number would drop to much less than 500mA.

### **Protecting the USB Pin and Wall Adapter Input from Overvoltage Transients**

Caution must be exercised when using ceramic capacitors to bypass the USBIN pin or the wall adapter inputs. High voltage transients can be generated when the USB or wall adapter is hot plugged. When power is supplied via the USB bus or wall adapter, the cable inductance along with the self resonant and high Q characteristics of ceramic capacitors can cause substantial ringing which could exceed the maximum voltage pin ratings and damage the LTC4075. Refer to Linear Technology Application Note 88, entitled "Ceramic Input Capacitors Can Cause Overvoltage Transients" for a detailed discussion of this problem. The long cable lengths of most wall adapters and USB cables



# **APPLICATIONS INFORMATION**

makes them especially susceptible to this problem. To bypass the USB pin and the wall adapter input, add a 1 $\Omega$ resistor in series with a ceramic capacitor to lower the effective Q of the network and greatly reduce the ringing. A tantalum, OS-CON, or electrolytic capacitor can be used in place of the ceramic and resistor, as their higher ESR reduces the Q, thus reducing the voltage ringing.

The oscilloscope photograph in Figure 4 shows how serious the overvoltage transient can be for the USB and wall adapter inputs. For both traces, a 5V supply is hot-plugged using a three foot long cable. For the top trace, only a 4.7µF capacitor (without the recommended  $1\Omega$  series resistor) is used to locally bypass the input. This trace shows excessive ringing when the 5V cable is inserted, with the overvoltage spike reaching 10V. For the bottom trace, a 1 $\Omega$  resistor is added in series with the 4.7µF capacitor to locally bypass the 5V input. This trace shows the clean response resulting from the addition of the 1Ω resistor.

Even with the additional 1 $\Omega$  resistor, bad design techniques and poor board layout can often make the overvoltage



**Figure 4. Waveforms Resulting from Hot-Plugging a 5V Input Supply**

problem even worse. System designers often add extra inductance in series with input lines in an attempt to minimize the noise fed back to those inputs by the application. In reality, adding these extra inductances only makes the overvoltage transients worse. Since cable inductance is one of the fundamental causes of the excessive ringing, adding a series ferrite bead or inductor increases the effective cable inductance, making the problem even worse. For this reason, **do not** add additional inductance (ferrite beads or inductors) in series with the USB or wall adapter inputs. For the most robust solution, 6V transorbs or zener diodes may also be added to further protect the USB and wall adapter inputs. Two possible protection devices are the SM2T from STMicroelectronics and the EDZ series devices from ROHM.

**Always use an oscilloscope to check the voltage waveforms at the USBIN and DCIN pins during USB and wall adapter hot-plug events to ensure that overvoltage transients have been adequately removed.**

### **Reverse Polarity Input Voltage Protection**

In some applications, protection from reverse polarity voltage on the input supply pins is desired. If the supply voltage is high enough, a series blocking diode can be used. In other cases where the voltage drop must be kept low, a P-channel MOSFET can be used (as shown in Figure 5).



**Figure 5. Low Loss Input Reverse Polarity Protection**



### **PACKAGE DESCRIPTION**



**DD Package 10-Lead Plastic DFN (3mm × 3mm) (Reference LTC DWG # 05-08-1699)**

> CHECK THE LTC WEBSITE DATA SHEET FOR CURRENT STATUS OF VARIATION ASSIGNMENT 2. DRAWING NOT TO SCALE

3. ALL DIMENSIONS ARE IN MILLIMETERS

4. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE 5. EXPOSED PAD SHALL BE SOLDER PLATED

6. SHADED AREA IS ONLY A REFERENCE FOR PIN 1 LOCATION ON THE TOP AND BOTTOM OF PACKAGE

