

LTC4446

High Voltage High Side/ Low Side N-Channel MOSFFT Driver

FEATURES

- Bootstrap Supply Voltage Up to 114V
- \blacksquare Wide V_{CC} Voltage: 7.2V to 13.5V
- ⁿ **2.5A Peak Top Gate Pull-Up Current**
- 3A Peak Bottom Gate Pull-Up Current
- ⁿ **1.2**Ω **Top Gate Driver Pull-Down**
- ⁿ **0.55**Ω **Bottom Gate Driver Pull-Down**
- ⁿ **5ns Top Gate Fall Time Driving 1nF Load**
- \blacksquare **8ns Top Gate Rise Time Driving 1nF Load**
- 3ns Bottom Gate Fall Time Driving 1nF Load
- 6ns Bottom Gate Rise Time Driving 1nF Load
- Drives Both High and Low Side N-Channel MOSFETs
- Undervoltage Lockout
- Thermally Enhanced 8-Pin MSOP Package

APPLICATIONS

- Distributed Power Architectures
- Automotive Power Supplies
- High Density Power Modules
- Telecommunication Systems

 \mathcal{L} , LT, LTC and LTM are registered trademarks of Linear Technology Corporation. All other trademarks are the property of their respective owners. Protected by U.S. Patents including 6677210.

DESCRIPTION

The LTC®4446 is a high frequency high voltage gate driver that drives two N-channel MOSFETs in a DC/DC converter with supply voltages up to 100V. The powerful driver capability reduces switching losses in MOSFETs with high gate capacitance. The LTC4446's pull-up for the top gate driver has a peak output current of 2.5A and its pull-down has an output impedance of 1.2 Ω . The pull-up for the bottom gate driver has a peak output current of 3A and the pull-down has an output impedance of 0.55 Ω .

The LTC4446 is configured for two supply-independent inputs. The high side input logic signal is internally level-shifted to the bootstrapped supply, which may function at up to 114V above ground.

The LTC4446 contains undervoltage lockout circuits that disable the external MOSFETs when activated.

The LTC4446 is available in the thermally enhanced 8-lead MSOP package.

The LTC4446 does not have adaptive shoot-through protection. For similar drivers with adaptive shoot-through protection, please refer to the chart below.

TYPICAL APPLICATION

Two Switch Forward Converter LTC4446 Driving a 1000pF Capacitive Load

ABSOLUTE MAXIMUM RATINGS PIN CONFIGURATION

Supply Voltage **(Note 1)**

ORDER INFORMATION

Consult LTC Marketing for parts specified with wider operating temperature ranges. *The temperature grade is identified by a label on the shipping container. Consult LTC Marketing for information on non-standard lead based finish parts.

For more information on lead free part marking, go to: http://www.linear.com/leadfree/

For more information on tape and reel specifications, go to: http://www.linear.com/tapeandreel/

ELECTRICAL CHARACTERISTICS The \bullet denotes the specifications which apply over the full operating

temperature range, otherwise specifications are at T_A = 25°C. V_{CC} = V_{BOOST} = 12V, V_{TS} = GND = 0V, unless otherwise noted.

ELECTRICAL CHARACTERISTICS The \bullet denotes the specifications which apply over the full operating

temperature range, otherwise specifications are at $T_A = 25^{\circ}$ C. V_{CC} = V_{BOOST} = 12V, V_{TS} = GND = 0V, unless otherwise noted.

Note 1: Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. Exposure to any Absolute Maximum Rating condition for extended periods may affect device reliability and lifetime.

with statistical process controls. The LTC4446I is guaranteed over the full –40°C to 85°C operating temperature range.

Note 3: T_{J} is calculated from the ambient temperature T_A and power dissipation P_D according to the following formula:

 $T_J = T_A + (P_D \cdot \theta_{JA}^{\circ} C/W)$

Note 2: The LTC4446E is guaranteed to meet specifications from 0°C to 85°C. Specifications over the -40°C to 85°C operating temperature range are assured by design, characterization and correlation

Note 4: Failure to solder the exposed back side of the MS8E package to the PC board will result in a thermal resistance much higher than 40°C/W.

TYPICAL PERFORMANCE CHARACTERISTICS

TYPICAL PERFORMANCE CHARACTERISTICS

Input Thresholds (TINP, BINP) vs Supply Voltage

Input Thresholds (TINP, BINP) Hysteresis vs Temperature

Input Thresholds (TINP, BINP) vs Temperature

V_{CC} Undervoltage Lockout **Thresholds vs Temperature**

RISING THRESHOLD

TEMPERATURE (°C)

FALLING THRESHOLD

–10 5 20 50 80 95 110 125

4446 G11

–40 –25 35 65

6.0

6.1

6.3 6.4 6.5

6.2

6.7

 $BOOST = V_{CC}$ TS = GND

6.6

V_{CC} SUPLLY VOLTAGE (V)

V_{CC} SUPLLY VOLTAGE (V)

Supply Voltage 15 $T_A = 25^{\circ}C$ 14 \angle BOOST = V_{CC} $TS = GND$ TG OR BG OUTPUT VOLTAGE (V) TG OR BG OUTPUT VOLTAGE (V) 13 12 –1mA 11 $-10mA$ 10 –100mA 9 8 7 6

Output High Voltage (V_{OH}) vs

Input Thresholds (TINP, BINP) Hysteresis vs Voltage

7 5

SUPPLY VOLTAGE (V)

9 11 12

Rise and Fall Time vs V_{CC} Supply Voltage

TYPICAL PERFORMANCE CHARACTERISTICS

TUREAR

PIN FUNCTIONS

TINP (Pin 1): High Side Input Signal. Input referenced to GND. This input controls the high side driver output (TG).

BINP (Pin 2): Low Side Input Signal. This input controls the low side driver output (BG).

V_{CC} (Pin 3): Supply. This pin powers input buffers, logic and the low side gate driver output directly and the high side gate driver output through an external diode connected between this pin and BOOST (Pin 6). A low ESR ceramic bypass capacitor should be tied between this pin and GND (Pin 9).

BG (Pin 4): Low Side Gate Driver Output (Bottom Gate). This pin swings between V_{CC} and GND.

NC (Pin 5): No Connect. No connection required.

BOOST (Pin 6): High Side Bootstrapped Supply. An external capacitor should be tied between this pin and TS (Pin 8). Normally, a bootstrap diode is connected between V_{CC} (Pin 3) and this pin. Voltage swing at this pin is from $V_{CC} - V_D$ to $V_{IN} + V_{CC} - V_D$, where V_D is the forward voltage drop of the bootstrap diode.

TG (Pin 7): High Side Gate Driver Output (Top Gate). This pin swings between TS and BOOST.

TS (Pin 8): High Side MOSFET Source Connection (Top Source).

Exposed Pad (Pin 9): Ground. Must be soldered to PCB ground for optimal thermal performance.

BLOCK DIAGRAM

TIMING DIAGRAM

OPERATION

Overview

The LTC4446 receives ground-referenced, low voltage digital input signals to drive two N-channel power MOSFETs in a synchronous buck power supply configuration. The gate of the low side MOSFET is driven either to V_{CC} or GND, depending on the state of the input. Similarly, the gate of the high side MOSFET is driven to either BOOST or TS by a supply bootstrapped off of the switching node (TS).

Input Stage

The LTC4446 employs CMOS compatible input thresholds that allow a low voltage digital signal to drive standard power MOSFETs. The LTC4446 contains an internal voltage regulator that biases both input buffers for high side and low side inputs, allowing the input thresholds $(V_{\text{IH}} = 2.75V, V_{\text{IL}} = 2.3V)$ to be independent of variations in V_{CC} . The 450mV hysteresis between V_{IH} and V_{II} eliminates false triggering due to noise during switching transitions. However, care should be taken to keep both input pins (TINP and BINP) from any noise pickup, especially in high frequency, high voltage applications. The LTC4446 input buffers have high input impedance and draw negligible input current, simplifying the drive circuitry required for the inputs.

Output Stage

A simplified version of the LTC4446's output stage is shown in Figure 1. The pull-up devices on the BG and TG outputs are NPN bipolar junction transistors (Q1 and Q2). The BG and TG outputs are pulled up to within an NPN V_{BF} (~0.7V) of their positive rails (V_{CC} and BOOST, respectively). Both BG and TG have N-channel MOSFET pull-down devices (M1 and M2) which pull BG and TG down to their negative rails, GND and TS. The large voltage swing of the BG and TG output pins is important in driving external power MOSFETs, whose $R_{DS(ON)}$ is inversely proportional to the gate overdrive voltage (V_{GS} – V_{TH}).

Figure 1. Capacitance Seen by BG and TG During Switching

Rise/Fall Time

The LTC4446's rise and fall times are determined by the peak current capabilities of Q1 and M1. The predriver that drives Q1 and M1 uses a nonoverlapping transition scheme to minimize cross-conduction currents. M1 is fully turned off before Q1 is turned on and vice versa.

Since the power MOSFET generally accounts for the majority of the power loss in a converter, it is important to quickly turn it on or off, thereby minimizing the transition time in its linear region. An additional benefit of a strong pull-down on the driver outputs is the prevention of crossconduction current. For example, when BG turns the low side (synchronous) power MOSFET off and TG turns the high side power MOSFET on, the voltage on the TS pin will rise to V_{IN} very rapidly. This high frequency positive voltage transient will couple through the C_{GD} capacitance of the low side power MOSFET to the BG pin. If there is an insufficient pull-down on the BG pin, the voltage on the BG pin can rise above the threshold voltage of the low side power MOSFET, momentarily turning it back on. With

OPERATION

both the high side and low side MOSFETs conducting, significant cross-conduction current will flow through the MOSFETs from V_{IN} to ground and will cause substantial power loss. A similar effect occurs on TG due to the C_{GS} and C_{GD} capacitances of the high side MOSFET.

The powerful output driver of the LTC4446 reduces the switching losses of the power MOSFET, which increase with transition time. The LTC4446's high side driver is capable of driving a 1nF load with 8ns rise and 5ns fall times using a bootstrapped supply voltage $V_{\text{BODST-TS}}$ of 12V while its low side driver is capable of driving a 1nF

load with 6ns rise and 3ns fall times using a supply voltage V_{CC} of 12V.

Undervoltage Lockout (UVLO)

The LTC4446 contains an undervoltage lockout detector that monitors V_{CC} supply. When V_{CC} falls below 6.15V, the output pins BG and TG are pulled down to GND and TS, respectively. This turns off both external MOSFETs. When V_{CG} has adequate supply voltage, normal operation will resume.

APPLICATIONS INFORMATION

Power Dissipation

To ensure proper operation and long-term reliability, the LTC4446 must not operate beyond its maximum temperature rating. Package junction temperature can be calculated by:

 $T_{\rm J} = T_{\rm A} + P_{\rm D} (\theta_{\rm JA})$

where:

 $T_{\rm J}$ = Junction temperature

 T_A = Ambient temperature

 P_D = Power dissipation

 θ_{JA} = Junction-to-ambient thermal resistance

Power dissipation consists of standby and switching power losses:

 $P_D = P_{DC} + P_{AC} + P_{OG}$

where:

 P_{DC} = Quiescent power loss

 P_{AC} = Internal switching loss at input frequency, f_{IN}

 P_{QG} = Loss due turning on and off the external MOSFET with gate charge QG at frequency f_{IN}

The LTC4446 consumes very little quiescent current. The DC power loss at V_{CC} = 12V and $V_{BOOST-TS}$ = 12V is only $(350\mu A)(12V) = 4.2mW.$

At a particular switching frequency, the internal power loss increases due to both AC currents required to charge and discharge internal node capacitances and cross-conduction currents in the internal logic gates. The sum of the quiescent current and internal switching current with no load are shown in the Typical Performance Characteristics plot of Switching Supply Current vs Input Frequency.

The gate charge losses are primarily due to the large AC currents required to charge and discharge the capacitance of the external MOSFETs during switching. For identical pure capacitive loads C_{LOAD} on TG and BG at switching frequency f_{IN} , the load losses would be:

$$
P_{CLOAD} = (C_{LOAD})(f)[(V_{BOOST-TS})^2 + (V_{CC})^2]
$$

In a typical synchronous buck configuration, $V_{\text{BOOST-TS}}$ is equal to $V_{CC} - V_D$, where V_D is the forward voltage drop across the diode between V_{CC} and BOOST. If this drop is small relative to V_{CC} , the load losses can be approximated as:

 $P_{\text{CLOAD}} = 2(C_{\text{LOAD}})(f_{\text{IN}})(V_{\text{CC}})^2$

APPLICATIONS INFORMATION

Unlike a pure capacitive load, a power MOSFET's gate capacitance seen by the driver output varies with its V_{GS} voltage level during switching. A MOSFET's capacitive load power dissipation can be calculated using its gate charge, Q_G . The Q_G value corresponding to the MOSFET's V_{GS} value (V_{CC} in this case) can be readily obtained from the manufacturer's Q_G vs V_{GS} curves. For identical MOSFETs on TG and BG:

 $P_{OG} = 2(V_{CC})(Q_G)(f_{IN})$

To avoid damage due to power dissipation, the LTC4446 includes a temperature monitor that will pull BG and TG low if the junction temperature rises above 160°C. Normal operation will resume when the junction temperature cools to less than 135°C.

Bypassing and Grounding

The LTC4446 requires proper bypassing on the V_{CC} and $V_{\text{BONST-TS}}$ supplies due to its high speed switching (nanoseconds) and large AC currents (Amperes). Careless component placement and PCB trace routing may cause excessive ringing.

To obtain the optimum performance from the LTC4446:

A. Mount the bypass capacitors as close as possible between the V_{CC} and GND pins and the BOOST and TS pins. The leads should be shortened as much as possible to reduce lead inductance.

- B. Use a low inductance, low impedance ground plane to reduce any ground drop and stray capacitance. Remember that the LTC4446 switches greater than 3A peak currents and any significant ground drop will degrade signal integrity.
- C. Plan the power/ground routing carefully. Know where the large load switching current is coming from and going to. Maintain separate ground return paths for the input pin and the output power stage.
- D. Keep the copper trace between the driver output pin and the load short and wide.
- E. Be sure to solder the Exposed Pad on the back side of the LTC4446 package to the board. Correctly soldered to a 2500mm2 doublesided 1oz copper board, the LTC4446 has a thermal resistance of approximately 40°C/W for the MS8E package. Failure to make good thermal contact between the exposed back side and the copper board will result in thermal resistances far greater than 40°C/W.

TYPICAL APPLICATION

LTC3722/LTC4446 420W 36V-72V_{IN} to 12V/35A Isolated Full-Bridge Supply **LTC3722/LTC4446 420W 36V-72VIN to 12V/35A Isolated Full-Bridge Supply**

PACKAGE DESCRIPTION

BOTTOM VIEW OF EXPOSED PAD OPTION 2.06 ± 0.102 (0.081 ± 0.004) 1 1.83 ± 0.102 0.889 ± 0.127 2.794 ± 0.102 (0.072 ± 0.004) (0.035 ± 0.005) $(.110 \pm .004)$ 5.23 $\frac{2.083 \pm 0.102}{(.082 \pm .004)} \frac{3.20 - 3.45}{(.126 - .136)}$ 3.20 – 3.45 (206) MIN $(.082 \pm .004)$ 8 3.00 ± 0.102 (0.118 ± 0.004) 0.52 0.65 0.42 ± 0.038 (0.0205) (.0256) (NOTE 3) $(.0165 \pm .0015)$ $6\,$ 8 REF TYP **BSC** ┝ Н RECOMMENDED SOLDER PAD LAYOUT $\overline{\mathbf{r}}$ 3.00 ± 0.102 4.90 ± 0.152 $(.118 \pm .004)$ DETAIL "A" $\frac{11}{(193 \pm .006)}$ 0.254 (NOTE 4) (0.010) $0^\circ - 6^\circ$ TYP v GAUGE PLANE $\frac{\square}{2}$ 3 Е ↟ 0.53 ± 0.152 1.10 0.86 (0.021 ± 0.006) (0.043) (0.034) DETAIL "A" MAX REF 0.18 (.007) ا استار استار بار
الاستار ال SEATING PLANE $0.22 - 0.38$ 0.1016 ± 0.0508 $(0.009 - 0.015)$ (0.004 ± 0.002) 0.65 TYP MSOP (MS8E) 0307 REV D (0.0256) NOTE: BSC

MS8E Package 8-Lead Plastic MSOP, Exposed Die Pad (Reference LTC DWG # 05-08-1662 Rev D)

1. DIMENSIONS IN MILLIMETER/(INCH)

2. DRAWING NOT TO SCALE

3. DIMENSION DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS.

MOLD FLASH, PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.152mm (.006") PER SIDE

4. DIMENSION DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS.

INTERLEAD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.152mm (.006") PER SIDE

5. LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.102mm (.004") MAX

