19-4757: Rev 3: 10/98 EVALUATION KIT MANUAL

FOLLOWS DATA SHEET

ΜΙΧΙΜ 740MHz, Low-Noise, Low-Distortion **Op Amps in SOT23-5**

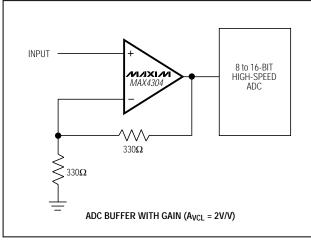
General Description

The MAX4104/MAX4105/MAX4304/MAX4305 op amps feature ultra-high speed, low noise, and low distortion in a SOT23 package. The unity-gain-stable MAX4104 requires only 20mA of supply current while delivering 625MHz bandwidth and 400V/µs slew rate. The MAX4304, compensated for gains of +2V/V or greater, delivers a 730MHz bandwidth and a 1000V/µs slew rate. The MAX4105 is compensated for a minimum gain of +5V/V and delivers a 410MHz bandwidth and a 1400V/sec slew rate. The MAX4305 has +10V/V minimum gain compensation and delivers a 340MHz bandwidth and a 1400V/µs slew rate.

Low voltage noise density of 2.1nV/VHz and -88dBc spurious-free dynamic range make these devices ideal for low-noise/low-distortion video and telecommunications applications. These op amps also feature a wide output voltage swing of ±3.7V and ±70mA output currentdrive capability. For space-critical applications, they are available in a miniature 5-pin SOT23 package.

Applications

Video ADC Preamp Pulse/RF Telecom Applications Video Buffers and Cable Drivers Ultrasound Active Filters ADC Input Buffers



M/IXI/M

Typical Application Circuit

Features

- ♦ Low 2.1nV/√Hz Voltage Noise Density
- Ultra-High 740MHz -3dB Bandwidth (MAX4304, AVCL = 2V/V
- 100MHz 0.1dB Gain Flatness (MAX4104/4105)
- 1400V/µs Slew Rate (MAX4105/4305)
- ◆ -88dBc SFDR (5MHz, RL = 100Ω) (MAX4104/4304)
- High Output Current Drive: ±70mA
- Low Differential Gain/Phase Error: 0.01%/0.01° (MAX4104/4304)
- Low ±1mV Input Offset Voltage
- Available in Space-Saving 5-Pin SOT23 Package

Selector Guide

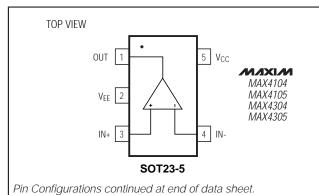
PART	MINIMUM STABLE GAIN (V/V)	BANDWIDTH (MHz)	PIN-PACKAGE
MAX4104	1	625	5-pin SOT23, 8-pin SO
MAX4304	2	740	5-pin SOT23, 8-pin SO
MAX4105	5	410	5-pin SOT23, 8-pin SO
MAX4305	10	340	5-pin SOT23, 8-pin SO

Ordering Information

PART	TEMP. RANGE	PIN- PACKAGE	SOT TOP MARK			
MAX4104ESA	-40°C to +85°C	8 SO	_			
MAX4104EUK-T	-40°C to +85°C	5 SOT23-5	ACCO			
Ondering hefermation continued at and of date about						

Ordering Information continued at end of data sheet.

Pin Configurations



Maxim Integrated Products 1

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ABSOLUTE MAXIMUM RATINGS

Supply Voltage (V_{CC} to V_{EE}).....+12V Voltage on Any Pin to Ground......(V_{EE} - 0.3V) to (V_{CC} + 0.3V) Short-Circuit Duration (V_{OUT} to GND).....Continuous Continuous Power Dissipation (T_A = +70°C) 5-pin SOT23 (derate 7.1mW/°C above +70°C).......571mW

Operating Temperature Range	-40°C to +85°C
Storage Temperature Range	65°C to +150°C
Lead Temperature (soldering, 10sec)	+300°C

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

DC ELECTRICAL CHARACTERISTICS

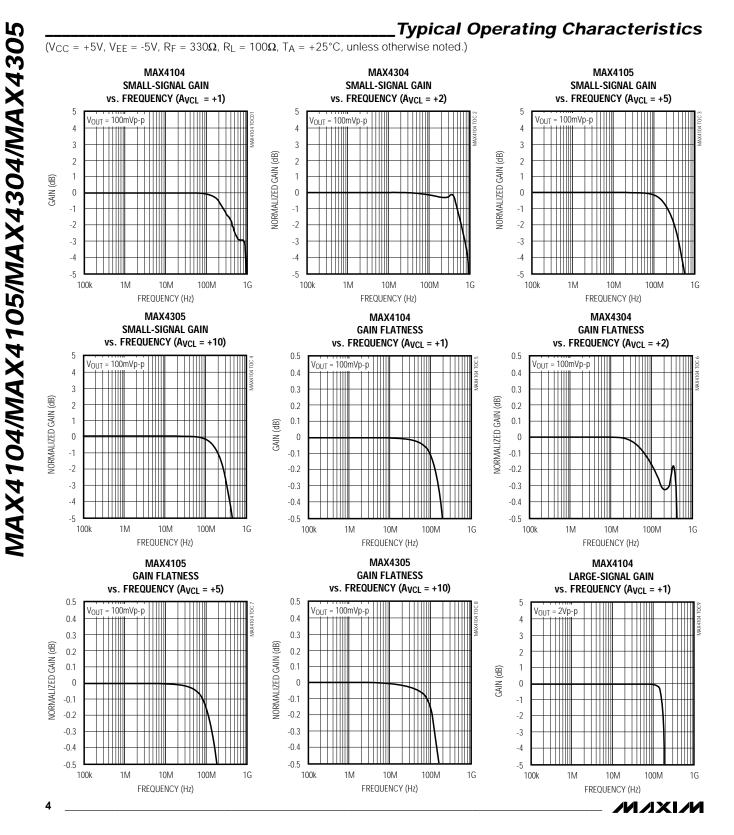
 $(V_{CC} = +5V, V_{EE} = -5V, V_{CM} = 0, R_L = 100k\Omega, T_A = T_{MIN}$ to T_{MAX} , unless otherwise noted. Typical values are at $T_A = +25^{\circ}C.$)

PARAMETER	SYMBOL	CONE	MIN	TYP	MAX	UNITS		
Operating Supply Voltage Range	V _{CC} /V _{EE}	Guaranteed by PSRR test		±3.5	±5	±5.5	V	
	M	N/	MAX4_0_ESA		1	6	mV	
input Onset voltage	put Offset Voltage V _{OS} V _{OUT} = 0		MAX4_0_EUK		1	8		
Input Offset-Voltage Drift	TCVOS				2.5		µV/°C	
Input Bias Current	IB				32	70	μA	
Input Offset Current	los				0.5	5.0	μA	
Differential Input Resistance	RIN	$-0.8V \le V_{IN} \le 0.8V$			6		kΩ	
Common-Mode Input Resistance	RIN	Either input		1.5		MΩ		
Input Common-Mode Voltage Range	V _{CM}	Guaranteed by CMRR	-2.8		+4.1	V		
Common-Mode Rejection Ratio	CMRR	$-2.8V \le V_{CM} \le 4.1V$	80	95		dB		
Positive Power-Supply Rejection Ratio	PSSR+	$V_{CC} = 3.5V$ to 5.5V		75	85		dB	
Negative Power-Supply Rejection Ratio	PSRR-	$V_{EE} = -3.5V \text{ to } -5.5V$	55	65		dB		
Quiescent Supply Current	Is	V _{OUT} = 0			20	27	mA	
Open-Loop Gain	Avol	$-2.8V \le V_{OUT} \le 2.8V$, F	55	65		dB		
Output Voltage Swing	Maur	$R_L = 100 k \Omega$		±3.5 -	-3.7 to +3.	8	V	
Output voltage Swing	Vout	$R_L = 100\Omega$	±3.0 -	-3.5 to +3.	4			
Output Current Drive	lout	$R_L = 30\Omega$ ±5			±70		mA	
Short-Circuit Output Current	Isc	R _L = short to ground 80				mA		
Open-Loop Output Impedance	Zout				9		Ω	

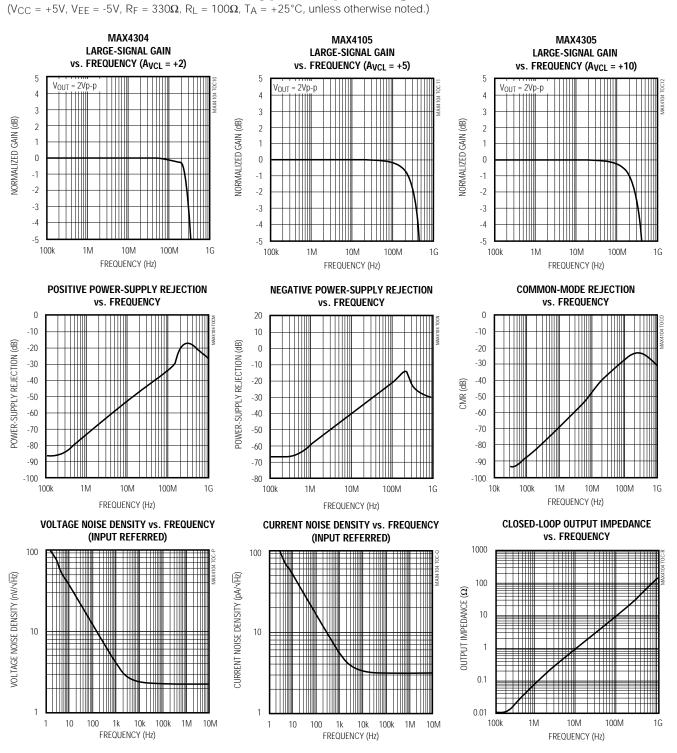
AC ELECTRICAL CHARACTERISTICS

 $(V_{CC} = +5V, V_{EE} = -5V, V_{CM} = 0, R_L = 100\Omega; A_V = +1V/V \text{ for MAX4104}, +2V/V \text{ for MAX4304}, +5V/V \text{ for MAX4105}, +10V/V \text{ for MAX4305}; T_A = +25°C; unless otherwise noted.)$

PARAMETER	SYMBOL	CONDITIONS			MIN	IIN TYP	MAX	UNITS		
-3dB Bandwidth					MAX4104		625		– MHz	
	DM(x = x = x)	V _{OUT} = 100mVp-p		MAX4304		740				
	BW(-3dB)			MAX4105		410				
				MAX4305		340		1		
		V _{OUT} = 100mVp-p		MAX4104		100		1		
0.1dB Bandwidth	BW(0,1)			MAX4304		60		- MHz		
	DVV(0.1)			MAX4105		80				
				MAX4305		70				
		V _{OUT} = 2Vp-p		MAX4104		115		-		
Full-Power Bandwidth				MAX4304		285				
Full-Power Bandwidth	FPBW			MAX4105		370		- MHz		
				MAX4305		320				
		V _{OUT} = 2Vp-p		MAX4104		400		- V/µs		
Slew Rate	SR			MAX4304		1000				
SIEW RALE				MAX4105		1400				
				MAX4305		1400				
Sattling Time to 0.1%	to	$V_{OUT} = 2V_{D-D}$		to 0.1%		20		nc		
Settling Time to 0.1%	ts			to 0.01%		25		ns		
	SFDR		MAX41	104/	$f_{\rm C} = 5 \rm MHz$		-88			
Spurious-Free		V _{OUT} = 2Vp-p	MAX43	304	$f_{\rm C} = 20 \rm MHz$		-67		dBc	
Dynamic Range			MAX4 ²	105/	$f_{\rm C} = 5 \rm MHz$		-74			
				MAX43	305	$f_{\rm C} = 20 \rm MHz$		-61		
Differential Gain Error	DG	NTSC, $R_L = 150\Omega$		MAX4104/MAX4			0.01		%	
Differential Gain Error				MAX	4105/MAX4305		0.02		- 70	
Differential Phase Error	DP	NTSC, $R_{\rm I} = 150\Omega$		MAX	4104/MAX4304		0.01		dograa	
Dinerential Phase Endi				4105/MAX4305		0.02		- degree		
Input Voltage Noise Density	en	f = 1MHz			2.1		nV/√Hz			
Input Current Noise Density	in	f = 1MHz					3.1		pA/√Hz	
Output Impedance	Z _{OUT}	f = 10MHz 1					Ω			



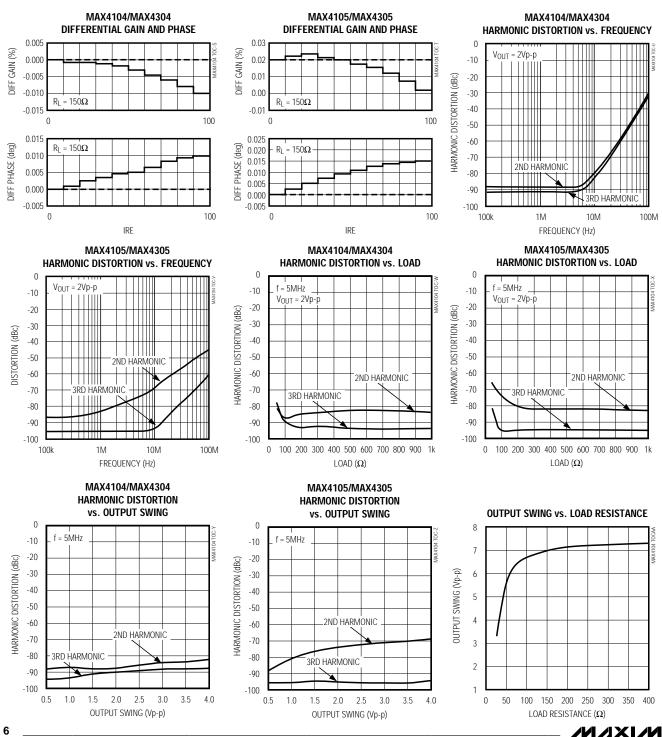
Typical Operating Characteristics (continued)



MAX4104/MAX4105/MAX4304/MAX4305

Typical Operating Characteristics (continued)

 $(V_{CC} = +5V, V_{EE} = -5V, R_F = 330\Omega, R_L = 100\Omega, T_A = +25^{\circ}C, unless otherwise noted.)$



Typical Operating Characteristics (continued) $(V_{CC} = +5V, V_{EE} = -5V, R_F = 330\Omega, R_L = 100\Omega, T_A = +25^{\circ}C, unless otherwise noted.)$ INPUT OFFSET VOLTAGE INPUT OFFSET CURRENT INPUT BIAS CURRENT vs. TEMPERATURE vs. TEMPERATURE vs. TEMPERATURE 3.0 4 35 2.5 3 2.0 34 NPUT OFFSET VOLTAGE (mV) INPUT OFFSET CURRENT (JuA) INPUT BIAS CURRENT (µA) 1.5 2 1.0 33 0.5 1 0.0 0 -0.5 32 -1.0 -1 -1.5 31 -2.0 -2 -2.5 -3.0 -3 30 -40 -15 85 -15 35 85 -40 -15 10 35 60 85 10 35 60 -40 10 60 TEMPERATURE (°C) TEMPERATURE (°C) TEMPERATURE (°C) SUPPLY CURRENT POSITIVE OUTPUT VOLTAGE SWING SUPPLY CURRENT vs. SUPPLY VOLTAGE vs. TEMPERATURE vs. TEMPERATURE 25 25 4.0 24 24 3.9 23 23 $R_{I} = 100 k \Omega$ 3.8 SUPPLY CURRENT (mA) SUPPLY CURRENT (mA) 22 22 VOLTAGE SWING (V) 3.7 21 21 20 20 3.6 19 19 3.5 $R_L = 100 k\Omega$ 18 18 3.4 17 17 3.3 16 16 15 3.2 15 9.5 85 9.0 10.0 10.5 11.0 -40 -15 10 35 60 -15 60 -40 10 35 85 SUPPLY VOLTAGE (V) TEMPERATURE (°C) TEMPERATURE (°C) MAX4304 MAX4104 MAX4105 SMALL-SIGNAL PULSE RESPONSE SMALL-SIGNAL PULSE RESPONSE SMALL-SIGNAL PULSE RESPONSE $(A_V = +1)$ $(A_V = +2)$ $(A_V = +5)$ MAX4104 TOCHE MAX4104 TOC LI IN +50mV +25mV GND +10mV IN GND IN GND -10mV -50mV -25mV +50mV +50mV +50mV OUT OUT GND OUT GND GND -50mV -50mV -50mV 10ns/div 10ns/div 10ns/div

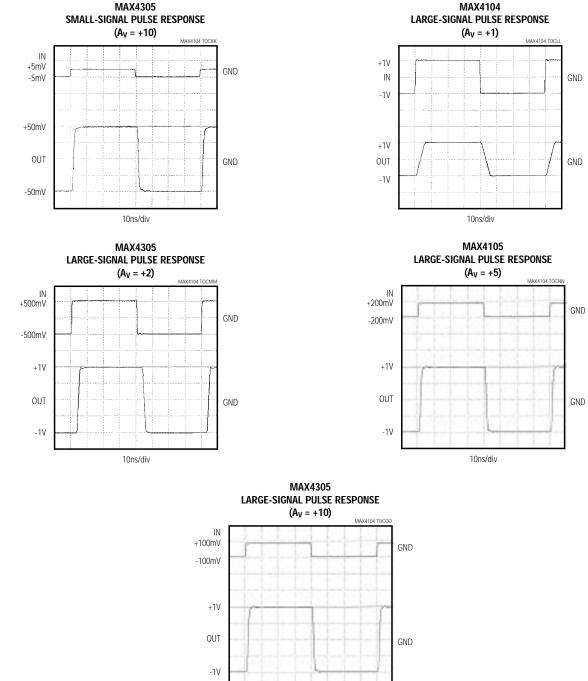
/M/IXI/M

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MAX4104/MAX4105/MAX4304/MAX4305

Typical Operating Characteristics (continued)

 $(V_{CC} = +5V, V_{EE} = -5V, R_F = 330\Omega, R_L = 100\Omega, T_A = +25^{\circ}C, unless otherwise noted.)$



10ns/div

P	NIN	NAME	FUNCTION
SOT23-5	SO		FORCHON
—	1, 5, 8	N.C.	Not internally connected.
4	2	IN-	Amplifier Inverting Input
3	3	IN+	Amplifier Noninverting Input
2	4	V _{EE}	Negative Power Supply
1	6	OUT	Amplifier Output
5	7	Vcc	Positive Power Supply

_Pin Description

Detailed Description

The MAX4104/MAX4105/MAX4304/MAX4305 are ultrahigh-speed, low-noise amplifiers featuring -3dB bandwidths up to 880MHz, 0.1dB gain flatness up to 100MHz, and low differential gain and phase errors of 0.01% and 0.01°, respectively. These devices operate on dual power supplies ranging from $\pm 3.5V$ to $\pm 5.5V$ and require only 20mA of supply current.

The MAX4104/MAX4304/MAX4105/MAX4305 are optimized for minimum closed-loop gains of +1V/V, +2V/V, +5V/V and +10V/V (respectively) with corresponding -3dB bandwidths of 880MHz, 730MHz, 430MHz, and 350MHz. Each device in this family features a low input voltage noise density of only 2.1nV/ $\sqrt{\text{Hz}}$ (at 1MHz), an output current drive of \pm 70mA, and spurious-free dynamic range as low as -88dBc (5MHz, R_L = 100 Ω).

_Applications Information

Layout and Power-Supply Bypassing

The MAX4104/MAX4105/MAX4304/MAX4305 have an extremely high bandwidth, and consequently require careful board layout, including the possible use of constant-impedance microstrip or stripline techniques.

To realize the full AC performance of these high-speed amplifiers, pay careful attention to power-supply bypassing and board layout. The PC board should have at least two layers: a signal and power layer on one side, and a large, low-impedance ground plane on the other side. The ground plane should be as free of voids as possible. With multilayer boards, locate the ground plane on a layer that incorporates no signal or power traces. Regardless of whether or not a constant-impedance board is used, it is best to observe the following guidelines when designing the board:

- Do not use wire-wrapped boards (they are much too inductive) or breadboards (they are much too capacitive).
- 2) Do not use IC sockets. IC sockets increase reactances.
- 3) Keep signal lines as short and straight as possible. Do not make 90° turns; round all corners.
- Observe high-frequency bypassing techniques to maintain the amplifier's accuracy and stability.
- 5) Bear in mind that, in general, surface-mount components have shorter bodies and lower parasitic reactance, resulting in greatly improved high-frequency performance over through-hole components.

The bypass capacitors should include 1nF and 0.1 μ F ceramic surface-mount capacitors between each supply pin and the ground plane, located as close to the package as possible. Optionally, place a 10 μ F tantalum capacitor at the power supply pins' point of entry to the PC board to ensure the integrity of incoming supplies. The power-supply trace should lead directly from the tantalum capacitor to the V_{CC} and V_{EE} pins. To minimize parasitic inductance, keep PC traces short and use surface-mount components.

Input termination resistors and output back-termination resistors, if used, should be surface-mount types, and should be placed as close to the IC pins as possible.

DC and Noise Errors

The MAX4104/MAX4105/MAX4304/MAX4305 output offset voltage, V_{OUT} (Figure 1), can be calculated with the following equation:

 $V_{OUT} = [V_{OS} + (I_{B+} \times R_S) + (I_{B-} \times (R_F || R_G))] [1 + R_F / R_G]$ where:

Vos = input offset voltage (in volts)

- 1 + R_F/R_G = amplifier closed-loop gain (dimensionless)
- I_{B+} = noninverting input bias current (in amps)
- IB- = inverting input bias current (in amps)
- R_G = gain-setting resistor (in ohms)
- R_F = feedback resistor (in ohms)
- Rs = source resistor at noninverting input (in ohms)

The following equation represents output noise density:

$$e_{n(OUT)} = \left[1 + \frac{R_F}{R_G}\right] \sqrt{\left(i_n \times R_S\right)^2 + \left[i_n \times \left(R_F \mid \mid R_G\right)\right]^2 + e_n^2}$$

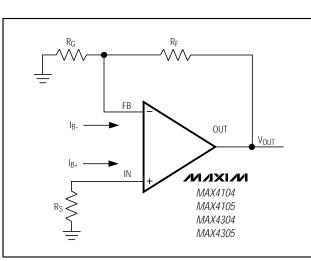


Figure 1. Output Offset Voltage

where:

 i_n = input current noise density (in pA/ \sqrt{Hz}) e_n = input voltage noise density (in nV/ \sqrt{Hz})

The MAX4104/MAX4105/MAX4304/MAX4305 have a very low, $2.1nV/\sqrt{Hz}$ input voltage noise density and $3.1pA/\sqrt{Hz}$ input current noise density.

An example of DC-error calculations, using the MAX4304 typical data and the typical operating circuit with $R_F = R_G = 330\Omega$ ($R_F \parallel R_G = 165\Omega$) and $R_S = 50\Omega$ gives:

$$V_{OUT} = \left[\left(32 \times 10^{-6} \right) (50) + \left(32 \times 10^{-6} \right) (165\Omega) + 1 \times 10^{-3} \right] \left[1 + 1 \right]$$

$$V_{OUT} = 15.8 \text{mV}$$

Calculating total output noise in a similar manner yields the following:

$$\begin{split} & e_{n(OUT)} = \\ & \left[1+1\right] \sqrt{\left(3.1 \times 10^{-12} \times 50\right)^2 + \left(3.1 \times 10^{-12} \times 165\right)^2 + \left(2.1 \times 10^{-9}\right)^2} \\ & e_{n(OUT)} = 4.3 \text{nV} \sqrt{\text{Hz}} \end{split}$$

With a 200MHz system bandwidth, this calculates to $60.8\mu V_{RMS}$ (approximately $365\mu V_{P-P}$, using the six-sigma calculation).

ADC Input Buffers

Input buffer amplifiers can be a source of significant error in high-speed ADC applications. The input buffer is usually required to rapidly charge and discharge the ADC's input, which is often capacitive. In addition, the input impedance of a high-speed ADC often changes

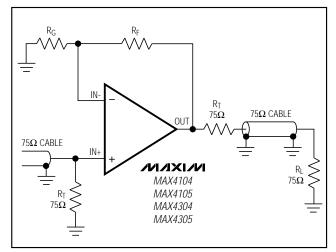


Figure 2. Video Line Driver

very rapidly during the conversion cycle—a condition that demands an amplifier with very low output impedance at high frequencies to maintain measurement accuracy. The combination of high-speed, fast slew rate, low noise, and low-distortion available in the MAX4104/MAX4105/MAX4304/MAX4305 makes them ideally suited for use as buffer amplifiers in high-speed ADC applications.

Video Line Driver

The MAX4104/MAX4105/MAX4304/MAX4305 are optimized to drive coaxial transmission lines when the cable is terminated at both ends, as shown in Figure 2. To minimize reflections and maximize power transfer, select the termination resistors to match the characteristic impedance of the transmission line. Cable frequency response can cause variations in the flatness of the signal.

Driving Capacitive Loads

The MAX4104/MAX4105/MAX4304/MAX4305 provide maximum AC performance when driving no output load capacitance. This is the case when driving a correctly terminated transmission line (i.e., a back-terminated cable).

In most amplifier circuits, driving a large load capacitance increases the chance of oscillations occurring. The amplifier's output impedance and the load capacitor combine to add a pole and excess phase to the loop response. If the pole's frequency is low enough and phase margin is degraded sufficiently, oscillations may result.

A second concern when driving capacitive loads originates from the amplifier's output impedance, which



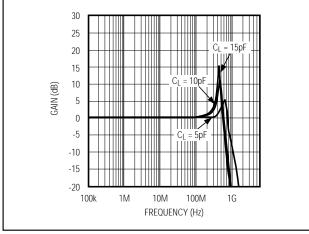


Figure 3a. MAX4104 Frequency Response with Capacitive Load and No Isolation Resistor

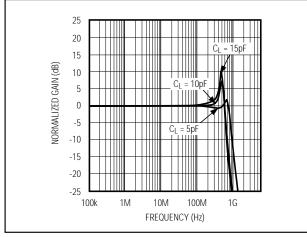


Figure 3c. MAX4105 Frequency Response with Capacitive Load and No Isolation Resistor

appears inductive at high frequencies. This inductance forms an L-C resonant circuit with the capacitive load, which causes peaking in the frequency response and degrades the amplifier's phase margin.

The MAX4104/MAX4105/MAX4304/MAX4305 drive capacitive loads up to 10pF without oscillation. However, some peaking may occur in the frequency domain (Figure 3). To drive larger capacitance loads or to reduce ringing, add an isolation resistor between the amplifier's output and the load (Figure 4).

The value of R_{ISO} depends on the circuit's gain and the capacitive load (Figure 5). Figure 6 shows the MAX4104/MAX4105/MAX4304/MAX4305 frequency response with the isolation resistor and a capacitive

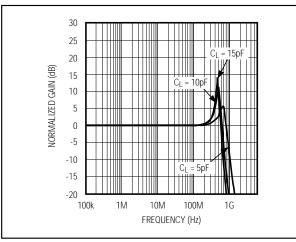


Figure 3b. MAX4304 Frequency Response with Capacitive Load and No Isolation Resistor

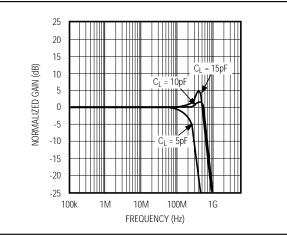


Figure 3d. MAX4305 Frequency Response with Capacitive Load and No Isolation Resistor

load. With higher capacitive values, bandwidth is dominated by the RC network formed by R_{ISO} and C_L ; the bandwidth of the amplifier itself is much higher. Also note that the isolation resistor forms a divider that decreases the voltage delivered to the load.

Maxim's High-Speed Evaluation Boards The MAX4104 evaluation kit manual shows a suggested layout for Maxim's high-speed, single-amplifier evaluation boards. This board was developed using the techniques described previously (*see Layout and Power-Supply Bypassing* section). The smallest available surface-mount resistors were used for the feedback and back-termination resistors to minimize the

