

General Description

The MAX8662/MAX8663 power-management ICs (PMICs) are efficient, compact devices suitable for smart cellular phones, PDAs, Internet appliances, and other portable devices. They integrate two synchronous buck regulators, a boost regulator driving two to seven white LEDs, four low-dropout linear regulators (LDOs), and a linear charger for a single-cell Li-ion (Li+) battery.

Maxim's Smart Power Selector™ (SPS) safely distributes power between an external power source (AC adapter, auto adapter, or USB source), battery, and the system load. When system load peaks exceed the external source capability, the battery supplies supplemental current. When system load requirements are small, residual power from the external power source charges the battery. A thermal-limiting circuit limits battery-charge rate and external power-source current to prevent overheating. The PMIC also allows the system to operate with no battery or a discharged battery.

The MAX8662 is available in a 6mm x 6mm, 48-pin TQFN package, while the MAX8663, without the LED driver, is available in a 5mm x 5mm, 40-pin TQFN package.

Applications

Smart Phones and PDAs MP3 and Portable Media Players Palmtop and Wireless Handhelds

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Features

- ♦ **Two 95%-Efficient 1MHz Buck Regulators Main Regulator: 0.98V to VIN at 1200mA Core Regulator: 0.98V to VIN at 900mA**
- ♦ **1MHz Boost WLED Driver Drives Up to 7 White LEDs at 30mA (max) PWM and Analog Dimming Control**
- ♦ **Four Low-Dropout Linear Regulators 1.7V to 5.5V Input Range 15µA Quiescent Current**
- ♦ **Single-Cell Li+ Charger Adapter or USB Input Thermal-Overload Protection**
- ♦ **Smart Power Selector (SPS) AC Adapter/USB or Battery Source Charger-Current and System-Load Sharing**

Ordering Information

+Denotes a lead(Pb)-free/RoHS-compliant package.

*EP = Exposed pad.

Typical Operating Circuit

Smart Power Selector is a trademark of Maxim Integrated

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For pricing, delivery, and ordering information, please contact Maxim Direct at 1-888-629-4642, or visit Maxim's website at www.maxim-ic.com.

ABSOLUTE MAXIMUM RATINGS

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

ELECTRICAL CHARACTERISTICS (Input Limiter and Battery Charger)

(V_{DC} = 5V, V_{BAT} = 4V, V_{CEN} = 0V, V_{PEN} = 5V, R_{PSET} = 3k Ω , R_{ISET} = 3.15k Ω , C_{CT} = 0.068µF, T_A = -40°C to +85°C, unless otherwise noted.) (Note 1)

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ELECTRICAL CHARACTERISTICS (Input Limiter and Battery Charger) (continued)

(V_{DC} = 5V, V_{BAT} = 4V, V_{CEN} = 0V, V_{PEN} = 5V, R_{PSET} = 3k Ω , R_{ISET} = 3.15k Ω , C_{CT} = 0.068µF, T_A = -40°C to +85°C, unless otherwise noted.) (Note 1)

ELECTRICAL CHARACTERISTICS (Input Limiter and Battery Charger) (continued)

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ELECTRICAL CHARACTERISTICS (Output Regulator)

 $(VSSS = VPV = VIN45 = VIN67 = 4.0V, VBRT = 1.25V,$ circuit of Figure 1, TA = -40°C to +85°C, unless otherwise noted.) (Note 1)

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ELECTRICAL CHARACTERISTICS (Output Regulator) (continued)

 $(V_{SYS_} = V_{PV_} = V_{IN45} = V_{IN67} = 4.0V$, $V_{BRT} = 1.25V$, circuit of Figure 1, $T_A = -40°C$ to $+85°C$, unless otherwise noted.) (Note 1)

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ELECTRICAL CHARACTERISTICS (Output Regulator) (continued)

 $(V_{SYS_} = V_{PV_} = V_{IN45} = V_{IN67} = 4.0V$, $V_{BRT} = 1.25V$, circuit of Figure 1, $T_A = -40°C$ to $+85°C$, unless otherwise noted.) (Note 1)

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ELECTRICAL CHARACTERISTICS (OUTPUT REGULATOR) (continued)

(V_{SYS} = V_{PV} = V_{IN45} = V_{IN67} = 4.0V, V_{BRT} = 1.25V, circuit of Figure 1, T_A = -40°C to +85°C, unless otherwise noted.) (Note 1)

Note 1: Limits are 100% production tested at T_A = +25°C. Limits over the operating temperature range are guaranteed through correlation using statistical quality control (SQC) methods.

Note 2: Input withstand voltage. Not designed to operate above V_{DC} = 6.5V due to thermal-dissipation issues.

Note 3: ISET voltage when CT timer stops. Occurs only when in constant-current mode. Translates to 20% of fast-charge current. **Note 4:** Temperature at which the input current limit begins to reduce.

Note 5: The WLED driver's sink current ramp time is a function of the external compensation at CC3. With a compensation of 1kΩ in series with 0.22µF and a target sink current of 30mA, the WLED boost's output voltage ramps up in 1.25ms, but the WLED sink current of 30mA settles in 12ms. See the OUT3 Enable and Disable Response graph in the Typical Operating Characteristics section for more information.

0.068µF, CREF = CVL = 0.1µF, RTHM = 10kΩ, L1 = 3.3µH, L2 = 4.7µH, L3 = 22µH, VGND = VPG1 = VPG2 = VPG3 = 0V, TA = +25°C,

(Circuit of Figure 1, V_{DC} = 5V, R_{PSET} = 1.5kΩ, R_{ISET} = 3kΩ, V_{OUT1} = 3.3V, V_{OUT2} = 1.3V, SL1 = SL2 = open, V_{CEN} = 0V, V_{PEN1} = $V_{\text{PEN2}} = 5V$, $C_{\text{OUT1}} = 2 \times 10$ µF, $C_{\text{OUT2}} = 2 \times 10$ µF, $C_{\text{OUT3}} = 0.1$ µF, $C_{\text{OUT4}} = 4.7$ µF, $C_{\text{OUT5}} = 1$ µF, $C_{\text{OUT6}} = 2.2$ µF, $C_{\text{OUT7}} = 1$ µF, CT =

Typical Operating Characteristics

BATTERY VOLTAGE (V)

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BATTERY VOLTAGE (V)

BATTERY VOLTAGE (V)

Typical Operating Characteristics (continued)

(Circuit of Figure 1, V_{DC} = 5V, Rpset = 1.5k Ω , R_{ISET} = 3k Ω , V_{OUT1} = 3.3V, V_{OUT2} = 1.3V, SL1 = SL2 = open, V_{CEN} = 0V, Vp_{EN1} = VPEN2 = 5V, COUT1 = 2 x 10µF, COUT2 = 2 x 10µF, COUT3 = 0.1µF, COUT4 = 4.7µF, COUT5 = 1µF, COUT6 = 2.2µF, COUT7 = 1µF, CT = 0.068µF, CREF = CVL = 0.1µF, RTHM = 10kΩ, L1 = 3.3µH, L2 = 4.7µH, L3 = 22µH, VGND = VPG1 = VPG2 = VPG3 = 0V, TA = +25°C, unless otherwise noted.)

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AC ADAPTER CONNECT (ISYS = 500mA) USB DISCONNECTED (500mA USB) MAX8662/63 toc18 MAX8662/63 toc19 5V/div **V_{DC}** 5V 5V consultation to the consultation of 5V/div V_{DC} 0V 475mA $+1280mA$ IIN 1A/div IIN 0mA 500mA/div V_{SYS} 5V 2V/div 4.4V VPOK $\overline{4.0V}$ 4.4V V_{SYS} 1V/div 5V/div VCHG ببإجر 5V/div 5V/div **V_{CHG}** $0V$ 0V 0mA 500mA 1A/div -780mA IBAT 500mA/div -475mA IBAT NEGATIVE BATTERY CURRENT FLOWS INTO THE BATTERY (CHARGING). 400µs/div 200µs/div $PEN1 = PEN2 = 1, \overline{CEN} = 0.$ $PEN1 = 0$, $PEN2 = 1$, $\overline{CEN} = 0$, $V_{BAT} = 4.0V$, $I_{SYS} = 500$ mA, $EN_ = 1$ $V_{BAT} = 4.0V$, $I_{SYS} = 0mA$ **OUT1 REGULATOR EFFICIENCY CHARGER ENABLE (ISYS = 0mA) vs. LOAD CURRENT** MAX8662/63 toc20 100 MAX8662/63 toc21 **VCEN** $0V$ 5V/div 2.8V 90 475mA OUT1 REGULATOR EFFICIENCY (%) OUT1 REGULATOR EFFICIENCY (%) 80 1A/div IIN 0mA $V_{\text{BAT}} = 3.6V$ 70 $V_{BAT} = 3.6V$ $\frac{5}{2}$ 4.4V VSYS 60 2V/div $V_{BAT} = 4.2V$ 50 $V_{\text{BAT}} = 4.2V$ **V_{CHG}** 0V 5V/div 40 0mA 30 **IBAT** -475mA 500mA/div 20 PWM **PWM** 10 VOUT1 = 3.3V 0 0.1 1 10 100 1000 10.000 1 10 100 1000 200µs/div LOAD CURRENT (mA) $PEN1 = 0$, $PEN2 = 1$, $V_{BAT} = 4.0V$, $I_{SYS} = 0mA$, $EN_{-} = 1$ **OUT1 REGULATOR LOAD REGULATION OUT1 REGULATOR LINE REGULATION OUT1 VOLTAGE vs. TEMPERATURE** 3.40 3.4 3.310 MAX8662/63 toc22 MAX8662/63 toc23 $V_{BAT} = 4.0V$ MAX8662/63 toc24 $R_{LOAD} = 330\Omega$ 3.3 3.36 3.306 3.2 $V_{\text{BAT}} = 4.2V$ \mathbf{S} OUTPUT VOLTAGE (V) OUTPUT VOLTAGE (V) OUTPUT VOLTAGE (V) 3.1 VOLTAGE (3.302 3.32 3.0 2.9 **OUTPUT** 3.28 3.298 $V_{\text{BAT}} = 3.6V$ 2.8 2.7 3.294 3.24 2.6

Typical Operating Characteristics (continued)

(Circuit of Figure 1, V_{DC} = 5V, Rpset = 1.5k Ω , R_{ISET} = 3k Ω , V_{OUT1} = 3.3V, V_{OUT2} = 1.3V, SL1 = SL2 = open, V_{CEN} = 0V, Vpen₁ = VPEN2 = 5V, COUT1 = 2 x 10µF, COUT2 = 2 x 10µF, COUT3 = 0.1µF, COUT4 = 4.7µF, COUT5 = 1µF, COUT6 = 2.2µF, COUT7 = 1µF, CT = 0.068µF, CREF = CVL = 0.1µF, RTHM = 10kΩ, L1 = 3.3µH, L2 = 4.7µH, L3 = 22µH, VGND = VPG1 = VPG2 = VPG3 = 0V, TA = +25°C, unless otherwise noted.)

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3.20

OUTPUT VOLTAGE (V)

OUTPUT VOLTAGE (V)

LOAD CURRENT (mA)

0.1 1 10 100 1000 10,000

10 100 1000

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Typical Operating Characteristics (continued)

(Circuit of Figure 1, V_{DC} = 5V, Rpset = 1.5k Ω , R_{ISET} = 3k Ω , V_{OUT1} = 3.3V, V_{OUT2} = 1.3V, SL1 = SL2 = open, V_{CEN} = 0V, Vp_{EN1} = VPEN2 = 5V, COUT1 = 2 x 10µF, COUT2 = 2 x 10µF, COUT3 = 0.1µF, COUT4 = 4.7µF, COUT5 = 1µF, COUT6 = 2.2µF, COUT7 = 1µF, CT = 0.068µF, CREF = CVL = 0.1µF, RTHM = 10kΩ, L1 = 3.3µH, L2 = 4.7µH, L3 = 22µH, VGND = VPG1 = VPG2 = VPG3 = 0V, TA = +25°C, unless otherwise noted.)

VEN1

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IDC

V_{OUT1}

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OUT2 REGULATOR LINE REGULATION OUT2 VOLTAGE vs. TEMPERATURE 1.310 1.3050 $R_{\text{LOAD}} = 130\Omega$ MAX8662/63 toc32 $V_{BAT} = 4.0V$ MAX8662/63 toc33 $R_{\text{LOAD}} = 130\Omega$ 1.308 1.3045 OUTPUT VOLTAGE (V) OUTPUT VOLTAGE (V) OUTPUT VOLTAGE (V) 1.306 1.3040 1.304 1.3035 1.302 1.300 1.3030 3.1 3.5 3.9 4.3 4.7 5.1 2.7 3.1 3.5 3.9 4.3 4.7 5.1 5.5 -40 -15 10 35 60 85 -15 10 35 60 V_{SYS} (V) AMBIENT TEMPERATURE (°C) **OUT2 REGULATOR LIGHT-LOAD OUT2 REGULATOR HEAVY-LOAD SWITCHING WAVEFORMSSWITCHING WAVEFORMS**MAX8662/63 toc35 MAX8662/63 toc34 $V_{BAT} = 4.0V$ $PWM = 0$ 10mV/div $I_{\text{OUT2}} = 10$ mA VOUT2 AC-COUPLED VOUT2 AC-COUPLED 20mV/div 2V/div V_L VLX 2V/div IL 500mA/div IL 100mA/div $V_{BAT} = 4.0V$ $I_{\text{OUT2}} = 900 \text{mA}$ 10µs/div 1µs/div **OUT2 REGULATOR LINE-OUT2 REGULATOR LOAD-TRANSIENT RESPONSETRANSIENT RESPONSE**MAX8662/63 toc37 MAX8662/63 toc36 5V **V_{LX}** 5V/div V_{SYS} $I_{\text{OUT1}} = 10 \text{m}$ 1V/div 4V PWM = 0 IOUT2 1A/div V_{OUT1} 20mV/div IL

Typical Operating Characteristics (continued)

100µs/div

200mA/div

*IVI AXI AV*I

5V/div

 \mathbf{l}_1

50mV/div

500mA/div

40µs/div

 $I_{\text{OUT2}} = 10 \text{mA}$ TO 900 mA TO 10 mA PWM = 0

V_{OUT2} AC-COUPLED

 $V_{BAT} = 4.0 V$

V_{LX}

(Circuit of Figure 1, V_{DC} = 5V, R_{PSET} = 1.5kΩ, R_{ISET} = 3kΩ, V_{OUT1} = 3.3V, V_{OUT2} = 1.3V, SL1 = SL2 = open, V<u>CEN</u> = 0V, Vp_{EN1} = VPEN2 = 5V, COUT1 = 2 x 10µF, COUT2 = 2 x 10µF, COUT3 = 0.1µF, COUT4 = 4.7µF, COUT5 = 1µF, COUT6 = 2.2µF, COUT7 = 1µF, CT = 0.068µF, CREF = CVL = 0.1µF, RTHM = 10kΩ, L1 = 3.3µH, L2 = 4.7µH, L3 = 22µH, VGND = VPG1 = VPG2 = VPG3 = 0V, TA = +25°C, unless otherwise noted.)

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Typical Operating Characteristics (continued)

(Circuit of Figure 1, V_{DC} = 5V, Rpset = 1.5kΩ, R_{ISET} = 3kΩ, V_{OUT1} = 3.3V, V_{OUT2} = 1.3V, SL1 = SL2 = open, V_{CEN} = 0V, VpEN₁ = VPEN2 = 5V, COUT1 = 2 x 10µF, COUT2 = 2 x 10µF, COUT3 = 0.1µF, COUT4 = 4.7µF, COUT5 = 1µF, COUT6 = 2.2µF, COUT7 = 1µF, CT = 0.068µF, CREF = CVL = 0.1µF, RTHM = 10kΩ, L1 = 3.3µH, L2 = 4.7µH, L3 = 22µH, VGND = VPG1 = VPG2 = VPG3 = 0V, TA = +25°C, unless otherwise noted.)

MAX8662/MAX8663 **MAX8662/MAX8663**

Typical Operating Characteristics (continued)

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(Circuit of Figure 1, V_{DC} = 5V, R_{PSET} = 1.5kΩ, R_{ISET} = 3kΩ, V_{OUT1} = 3.3V, V_{OUT2} = 1.3V, SL1 = SL2 = open, V<u>CEN</u> = 0V, Vp_{EN1} = VPEN2 = 5V, COUT1 = 2 x 10µF, COUT2 = 2 x 10µF, COUT3 = 0.1µF, COUT4 = 4.7µF, COUT5 = 1µF, COUT6 = 2.2µF, COUT7 = 1µF, CT = 0.068µF, CREF = CVL = 0.1µF, RTHM = 10kΩ, L1 = 3.3µH, L2 = 4.7µH, L3 = 22µH, VGND = VPG1 = VPG2 = VPG3 = 0V, TA = +25°C, unless otherwise noted.)

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Typical Operating Characteristics (continued)

(Circuit of Figure 1, V_{DC} = 5V, R_{PSET} = 1.5kΩ, R_{ISET} = 3kΩ, V_{OUT1} = 3.3V, V_{OUT2} = 1.3V, SL1 = SL2 = open, V<u>CEN</u> = 0V, Vp_{EN1} = VPEN2 = 5V, COUT1 = 2 x 10µF, COUT2 = 2 x 10µF, COUT3 = 0.1µF, COUT4 = 4.7µF, COUT5 = 1µF, COUT6 = 2.2µF, COUT7 = 1µF, CT = 0.068µF, CREF = CVL = 0.1µF, RTHM = 10kΩ, L1 = 3.3µH, L2 = 4.7µH, L3 = 22µH, VGND = VPG1 = VPG2 = VPG3 = 0V, TA = +25°C, unless otherwise noted.)

OUTPUT VOLTAGE (V)

MAX8662/MAX8663 **MAX8662/MAX8663**

Typical Operating Characteristics (continued)

(Circuit of Figure 1, V_{DC} = 5V, R_{PSET} = 1.5kΩ, R_{ISET} = 3kΩ, V_{OUT1} = 3.3V, V_{OUT2} = 1.3V, SL1 = SL2 = open, V<u>CEN</u> = 0V, Vp_{EN1} = VPEN2 = 5V, COUT1 = 2 x 10µF, COUT2 = 2 x 10µF, COUT3 = 0.1µF, COUT4 = 4.7µF, COUT5 = 1µF, COUT6 = 2.2µF, COUT7 = 1µF, CT = 0.068µF, CREF = CVL = 0.1µF, RTHM = 10kΩ, L1 = 3.3µH, L2 = 4.7µH, L3 = 22µH, VGND = VPG1 = VPG2 = VPG3 = 0V, TA = +25°C, unless otherwise noted.)

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Typical Operating Characteristics (continued)

(Circuit of Figure 1, V_{DC} = 5V, Rpset = 1.5kΩ, R_{ISET} = 3kΩ, V_{OUT1} = 3.3V, V_{OUT2} = 1.3V, SL1 = SL2 = open, V_{CEN} = 0V, VpEN₁ = VPEN2 = 5V, COUT1 = 2 x 10µF, COUT2 = 2 x 10µF, COUT3 = 0.1µF, COUT4 = 4.7µF, COUT5 = 1µF, COUT6 = 2.2µF, COUT7 = 1µF, CT = 0.068µF, CREF = CVL = 0.1µF, RTHM = 10kΩ, L1 = 3.3µH, L2 = 4.7µH, L3 = 22µH, VGND = VPG1 = VPG2 = VPG3 = 0V, TA = +25°C, unless otherwise noted.)

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Pin Description

Pin Description (continued)

Pin Description (continued)

Figure 1. Block Diagram and Application Circuit

MAX8662/MAX8663 MAX8662/MAX8663

Power-Management ICs for Single-Cell, Li+ Battery-Operated Devices

Detailed Description

The MAX8662/MAX8663 highly integrated PMICs are designed for use in smart cellular phones, PDAs, Internet appliances, and other portable devices. They integrate two synchronous buck regulators, a boost regulator driving two to seven white LEDs (MAX8662 only), four low dropout (LDO) linear regulators, and a linear charger for a single-cell Li+ battery. Figure 1 is the block diagram and application circuit.

SPS circuitry offers flexible power distribution between an AC adapter or USB source, battery, and system load, and makes the best use of available power from the AC adapter/USB input. The battery is charged with any available power not used by the system load. If a system load peak exceeds the current limit, supplemental current is taken from the battery. Thermal limiting prevents overheating by reducing power drawn from the input source.

Two step-down DC-DC converters achieve excellent light-load efficiency and have on-chip soft-start circuitry; 1MHz switching frequency allows for small external components. Four LDO linear regulators feature low quiescent current and operate from inputs as low as 1.7V. This allows the LDOs to operate from the stepdown output voltage to improve efficiency. The white LED driver features easy adjustment of LED brightness and open-LED overvoltage protection. A 1-cell Li+ charger has programmable charge current up to 1.25A and a charge timer.

Smart Power Selector (SPS)

SPS seamlessly distributes power between the external input, the battery, and the system load (Figure 2). The basic functions of SPS are:

- With both the external power supply and battery connected:
	- a) When the system load requirements exceed the capacity of the external power input, the battery supplies supplemental current to the load.
	- b) When the system load requirements are less than the capacity of the external power input, the battery is charged with residual power from the input.
- When the battery is connected and there is no external power input, the system is powered from the battery.
- When an external power input is connected and there is no battery, the system is powered from the external power input.

A thermal-limiting circuit reduces battery-charge rate and external power-source current to prevent overheating.

Figure 2. Smart Power Selector Block Diagram

Input Limiter

All regulated outputs (OUT1–OUT7) derive their power from the SYS output. With an AC adapter or USB source connected at DC, the input limiter distributes power from the external power source to the system load and battery charger. In addition to the input limiter's primary function of passing the DC power source to the system and charger loads at SYS, it performs several additional functions to optimize use of available power:

- **Input Voltage Limiting:** If the voltage at DC rises, SYS limits to 5.3V, preventing an overvoltage of the system load. A DC voltage greater than 6.9V is considered invalid and the input limiter disconnects the DC input entirely. The withstand voltage at DC is guaranteed to be at least 9V. A DC input is also invalid if it is less than BAT, or less than the DC undervoltage threshold of 3.5V (falling). With an invalid DC input voltage, SYS connects to BAT through a 40m $Ω$ switch.
- **Input Overcurrent Protection:** The current at DC is limited to prevent input overload. This current limit is automatically adjusted to match the capabilities of source, whether it is a 100mA or 500mA USB source, or an AC adapter. When the load exceeds the input current limit, SYS drops to 100mV below BAT and supplemental load current is provided by the battery.

- **Thermal Limiting:** The input limiter includes a thermal-limiting circuit that reduces the current drawn from DC when the IC junction temperature increases beyond +100°C in an attempt to prevent further heating. The current limit is be reduced by 5%/°C for temperatures above +100°C, dropping to 0mA at +120°C. Due to the adaptive nature of the charging circuitry, the charger current reduces to 0mA before the system load is affected by thermal limiting.
- Adaptive Battery Charging: While the system is powered from DC, the charger can also draw power from SYS to charge the battery. If the charger load plus system load exceeds the current capability of the input source, an adaptive charger control loop reduces charge current to prevent the SYS voltage from collapsing. Maintaining a higher SYS voltage improves efficiency and reduces power dissipation in the input limiter by running the switching regulators at lower current.

Figure 3 shows the SYS voltage and its relationship to DC and BAT under three conditions:

- a) Charger is off and SYS is driven from DC.
- b) Charger is on and adaptive charger control is limiting charge current.
- c) The load at SYS is greater than the available input current.

The adaptive battery-charger circuit reduces charging current when the SYS voltage drops 550mV below DC. For example, if DC is at 5V, the charge current reduces to prevent SYS from dropping below 4.45V. When DC is greater than 5.55V, the adaptive charging circuitry reduces charging current when SYS drops 300mV below the 5.3V SYS regulation point (5.0V). Finally, the circuit prevents itself from pulling SYS down to within 100mV of BAT.

Figure 3. SYS Voltage and Charge Current vs. DC and BAT Voltage

DC Input Current-Limit Selection (PEN1/PEN2)

The input current limit can be set to a variety of values as shown in Table 1. When the PEN1 input is low, a USB source is expected at DC and the current limit is set to either 95mA or 475mA by PEN2.

When PEN1 is high, an AC adapter is expected at DC and the current limit is set based on a programming resistor at PSET. The DC input current limit is calculated from:

 $IDC_LIM = 2000 \times (1.5 / RPSET)$

An exception is when the battery charger is disabled (CEN high) with PEN2 low, where the MAX8662/ MAX8663 enter USB suspend mode.

Power-OK Output (POK**)**

POK is an active-low open-drain output indicating DC status. When the voltage at DC is between the undervoltage and the overvoltage thresholds, and is greater than the BAT voltage, POK pulls low to indicate that input power is OK. Otherwise, POK is high impedance. POK is not affected by the states of PEN1, PEN2, or CEN. POK remains active in thermal overload.

Battery Charger

The battery charger state diagram is illustrated in Figure 4.

With a valid AC adapter/USB voltage present, the battery charger initiates a charge cycle when the charger

Table 1. DC Input Current and Charger Current-Limit Select

*X = Don't care. ***The maximum charge will not exceed the DC Input current.

Figure 4. Charger State Diagram

is enabled. It first detects the battery voltage. If the battery voltage is less than the BAT prequalification threshold (3.0V), the charger enters prequalification mode in which the battery charges at 10% of the maximum fastcharge current. This slow charge ensures that the battery is not damaged by fast-charge current while deeply discharged. Once the battery voltage rises to 3.0V, the charger transitions to fast-charge mode and applies the maximum charge current. As charging continues, the battery voltage rises until it reaches the battery regulation voltage (4.2V) where charge current starts tapering down. When charge current decreases to 7.5% of fast-charge current, the charger enters topoff mode. Top-off charging continues for 30min, then all charging stops. If the battery voltage subsequently drops below the 4.1V recharge threshold, charging restarts and the timers reset.

Charge Current

ISET adjusts the MAX8662/MAX8663 charging current to match the capacity of the battery. A resistor from ISET to ground sets the maximum fast-charge current, the charge current in prequal, and the charge-current threshold below which the battery is considered completely charged. Calculate these thresholds as follows:

> ICHG-MAX = 1556 x 1.5V / RISET $IPRE-QUAL = 10% \times ICHG-MAX$

 $I_{\text{TOP-OFF}}$ = 7.5% x $I_{\text{CHG-MAX}}$

Determine the ICHG-MAX value by considering the characteristics of the battery, and not the capabilities of the expected AC adapter/USB charging input, the system load, or thermal limitations of the PCB. The MAX8662/ MAX8663 automatically adjust the charging algorithm to accommodate these factors.

In addition to setting the charge current, ISET also provides a means to monitor battery-charge current. The output voltage of the ISET pin tracks the charge current delivered to the battery, and can be used to monitor the charge rate, as shown in Figure 5. A 1.5V output indicates the battery is being charged at the maximum set fast-charge current; 0V indicates no charging. This voltage is also used by the charger control circuitry to set and monitor the battery current. Avoid adding more than 10pF capacitance directly to the ISET pin. If filtering of the charge-current monitor is necessary, add a resistor of 100kΩ or more between ISET and the filter capacitor to preserve charger stability.

Figure 5. Monitoring the Battery Charge Current with ISET Output Voltage

Charge Timer

As shown in Figure 3, the MAX8662/MAX8663 feature a fault timer for safe charging. If prequalification charging or fast charging does not complete within the time limits, which are programmed by the timer capacitor at CT, the charger stops charging and issues a timeout fault. Charging can be resumed by either toggling CEN or cycling the DC input voltage.

The MAX8662/MAX8663 support values of CCT from $0.01\mu F$ to $1\mu F$:

$$
t_{PREQUAL} = 30 \text{min} \times \frac{C_{CT}}{0.068 \mu\text{F}}
$$

$$
t_{FST-CHG} = 300 \text{min} \times \frac{C_{CT}}{0.068 \mu\text{F}}
$$

When the charger exits fast-charge mode, CHG goes high impedance and top-off mode is entered. Top-off time is also determined by the capacitance at CT:

$$
t_{\text{TOP-OFF}} = 300 \text{min} \times \frac{C_{\text{CT}}}{0.068 \mu\text{F}}
$$

In fast-charge mode, the fault timer is suspended when the charge current is limited, by input or thermal limiting, to less than 20% of ICHG-MAX.

Connect CT to GND to disable the prequalification and fast-charge timers, allowing the battery to charge indefinitely in top-off mode, or if other system timers are to be used to control charging.

Charge-Enable Input (CEN**)**

Driving CEN high disables the battery charger. Driving CEN low enables the charger when a valid source is connected at DC. CEN does not affect the input limit current, except that driving CEN high and PEN2 low activates USB suspend mode.

In many systems, there is no need for the system controller (typically a microprocessor) to disable the charger because the SPS circuitry independently manages charging and adapter/battery power hand-off. In these situations, CEN can be connected to ground.

Charge Status Output (CHG**)**

CHG is an open-drain output that indicates charger status. CHG is low when the battery charger is in prequalification or fast-charge mode. It is high impedance when the charger is done, in top-off, or disabled.

The charger faults if the charging timer expires in prequalification or fast charge. In this state, CHG pulses at 1Hz to indicate that a fault occurred.

Battery Charger Thermistor Input (THM)

Battery or ambient temperature can be monitored with a negative temperature coefficient (NTC) thermistor. Charging is allowed when the thermistor temperature is within the allowable range.

The charger enters a temperature suspend state when the thermistor resistance falls below 3.97kΩ (too hot) or rises above 28.7k Ω (too cold). This corresponds to a 0 to +50°C range when using a 10kΩ NTC thermistor with

a beta of 3500. The relation of thermistor resistance to temperature is defined by the following equation:

$$
R_{\mathsf{T}} = R25 \times e^{\left\{\beta \left(\frac{1}{\mathsf{T} + 273} - \frac{1}{298} \right) \right\}}
$$

where:

 R_{t} = The resistance in ohms of the thermistor at temperature T in Celsius

 $R25 =$ The resistance in ohms of the thermistor at $+25^{\circ}$ C

 β = The material constant of the thermistor, which typically ranges from 3000K to 5000K

 $T =$ The temperature of the thermistor in $°C$

Table 2 shows temperature limits for different thermistor material constants.

Some designs may prefer other trip temperatures. This can usually be accommodated by connecting a resistor in series and/or in parallel with the thermistor and/or using a thermistor with different ß. For example, a +45°C hot threshold and 0°C cold threshold can be realized by using a thermistor with a ß of 4250 and connecting 120kΩ in parallel. Since the thermistor resistance near 0°C is much higher than it is near +50°C, a large parallel resistance lowers the cold threshold, while only slightly lowering the hot threshold. Conversely, a small series resistance raises the cold threshold, while only slightly raising the hot threshold.

The charger timer pauses when the thermistor resistance goes out of range: charging stops and the timer counters hold their state. When the temperature comes back into range, charging resumes and the counters continue from where they left off. Connecting THM to GND disables the thermistor function.

Table 2. Fault Temperatures for Different Thermistors

Figure 6. Thermistor Input

Figure 6 shows a simplified version of the THM input. Ensure that the physical size of the thermistor is such that the circuit of Figure 6 does not cause self-heating.

Step-Down DC-DC Converters (OUT1 and OUT2)

OUT1 and OUT2 are high-efficiency, 1MHz, current-mode step-down converters with adjustable output voltage. The OUT1 regulator outputs 0.98V to V_{IN} at up to 1200mA while OUT2 outputs 0.98V to V_{IN} at up to 900mA.

OUT1 and OUT2 have individual enable inputs. When enabled, the OUT1 and OUT2 gradually ramp the output voltage over a 400µs soft-start time. This soft-start eliminates input inrush current spikes.

OUT1 and OUT2 can operate at a 100% duty cycle, which allows the regulators to maintain regulation at the lowest possible battery voltage. The OUT1 dropout voltage is 72mV with a 600mA load and the OUT2 dropout voltage is 90mV with a 450mA load (does not include inductor resistance). During 100% duty-cycle operation, the high-side p-channel MOSFET turns on continuously, connecting the input to the output through the inductor.

Step-Down Converter Operating Modes

OUT1 and OUT2 can operate in either auto-PWM mode (PWM low) or forced-PWM mode (PWM high). In auto-PWM mode, OUT1 and OUT2 enter skip mode when the load current drops below a predetermined level. In skip mode, the regulator skips cycles when they are not needed, which greatly decreases quiescent current and improves efficiency at light loads. In forced-PWM mode, the converters operate with a constant 1MHz switching frequency regardless of output load. Output voltage is regulated by modulating the switching duty cycle. Forced-PWM mode is preferred for low-noise systems, where switching harmonics can occur only at multiples of the constant-switching frequency and are easily filtered; however, regulator operating current is greater and light-load efficiency is reduced.

Synchronous Rectification

Internal n-channel synchronous rectifiers eliminate the need for external Schottky diodes and improve efficiency. The synchronous rectifier turns on during the second half of each switching cycle. During this time, the voltage across the inductor is reversed, and the inductor current ramps down. In PWM mode, the synchronous rectifier turns off at the end of the switching cycle. In

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skip mode, the synchronous rectifier turns off when the inductor current falls below the n-channel zero-crossing threshold or at the end of the switching cycle, whichever occurs first.

Setting OUT1 and OUT2 Output Voltage

Select an output voltage for OUT1 between 0.98V and VIN by connecting FB1 to the center of a resistive voltage-divider between OUT1 and GND. Choose R3 (Figure 1) for a reasonable bias current in the resistive divider; choose R3 to be between 100kΩ and 200kΩ. Then, R2 (Figure 1) is given by:

 $R2 = R3 ((V_{OUT1}/V_{FB}) - 1)$

where $V_{FB} = 0.98V$. For OUT2, R4 and R5 are calculated using:

 $R4 = R5 ((V_{OUT2}/V_{FB}) - 1)$

OUT1 and OUT2 Inductors

3.3µH and 4.7µH inductors are recommended for the OUT1 and OUT2 step-down converters. Ensure that the inductor saturation current rating exceeds the peak inductor current, and the rated maximum DC inductor current exceeds the maximum output current. For lower load currents, the inductor current rating may be reduced. For most applications, use an inductor with a current rating 1.25 times the maximum required output current. For maximum efficiency, the inductor's DC resistance should be as low as possible. See Table 4 for component examples.

Boost Converter with White LED Driver (OUT3, MAX8662 Only)

The MAX8662 contains a boost converter, OUT3, which drives up to seven white LEDs in series at up to 30mA. The boost converter regulates its output voltage to maintain the bottom of the LED stack at 320mV. A 1MHz switching rate allows for a small inductor and small input and output capacitors, while also minimizing input and output ripple.

Reference Voltage

REF is a 1.5V regulated output that is available to drive the BRT input when the boost converter is enabled. This voltage can be used to control LED brightness by driving BRT through a resistor-divider.

Boost Overvoltage Protection (OVP)

OVP limits the maximum voltage of the boost output for protection against overvoltage due to open or disconnected LEDs. An external resistor between OUT3 and OVP, with an internal 20µA pulldown current from OVP to GND, sets the maximum boost output to:

 $V_{\text{BOOST_MAX}} = (R_{\text{OVP}} \times 20 \mu\text{A}) + 1.25 \text{V}$

For example, with R $OVP = 1.2M\Omega$, the OUT3 maximum voltage is set at 25.25V. The OVP circuit also provides soft-start to reduce inrush current by ramping the internal pulldown current from 0 to 20µA over 1.25ms at startup. The 20µA internal current is disconnected when EN3 goes low.

OUT3 can also be used as a voltage-output boost by setting Royp for the desired output voltage. When doing this, the output filter capacitor must be at least 1µF, and the compensation network should be a 0.01µF capacitor in series with a 10k Ω resistor from CC3 to ground.

Brightness Control (Voltage or PWM)

LED current is set by the voltage at BRT. The VBRT range for adjusting output current from 1mA to 30mA is 50mV to 1.5V. Connecting BRT to a 1.5V reference voltage (such as REF) sets LED current to 30mA.

The EN3 input can also be driven by a logic-level PWM brightness control signal, such as that supplied by a microcontroller. The allowed PWM frequency range is from 1kHz to 100kHz. A 100% duty cycle corresponds to full current set by the BRT pin. The MAX8662 digitally decodes the PWM brightness signal and eliminates PWM ripple found in more common PWM brightness controls. As a result, no external filtering is needed to prevent intensity ripple at the PWM rate.

In order to properly distinguish between a DC or PWM control signal, the MAX8662 delays turn-on from the rising edge of EN3, and turn-off from the falling edge of EN3, by 2ms. If there are no more transitions in the EN3 signal after 2ms, EN3 assumes the control signal is DC and sets LED brightness based on the DC level. If two rising edges occur within 2ms, the circuit assumes the control is PWM and sets brightness based on the duty cycle.

OUT3 Inductor

For the white LED driver, OUT3, a 22µH inductor is recommended for most applications. For best efficiency, the inductor's DC resistance should also be as low as possible. See Table 4 for component examples.

OUT3 Compensation

An RC compensation network from CC3 to GND and an output capacitor (C14 of Figure 1) ensure boost converter stability. For WLED applications, connect a 0.22µF ceramic capacitor in series with a 1k Ω resistor from CC3 to GND and use a 0.1µF output capacitor. For fixed output voltage applications such as OLED, connect a 0.01µF ceramic capacitor in series with a 10kΩ resistor from CC3 to GND and use a 1µF capacitor. These components for fixed output voltage applications improve the load transient performance of the boost converter. The trade-off for this improved load

transient performance is the larger (1µF) high-voltage (30V) output capacitor.

The RC compensation network from CC3 to GND affects the WLED driver's sink current ramp time. As shown in the OUT3 Enable and Disable Response graph in the Typical Operating Characteristics section, the OUT3 voltage ramps up in 1.25ms, but the WLED sink current of 30mA settles in 12ms. This 12ms is associated with the compensation of $1k\Omega$ in series with 0.22µF. Smaller RC time constants reduce the WLED sink current ramp time.

OUT3 Diode Selection

The MAX8662 boost converter's high-switching frequency demands a high-speed rectification diode (D1) for optimum efficiency. A Schottky diode is recommended due to its fast recovery time and low forwardvoltage drop. Ensure the diode's peak current rating exceeds the peak inductor current. In addition, the diode's reverse breakdown voltage must exceed VOUT3. See Table 4 for component examples.

Linear Regulators (OUT4, OUT5, OUT6, and OUT7)

The MAX8662/MAX8663 contain four low-dropout, lowquiescent current, low-operating voltage linear regulators. The maximum output currents for OUT4, OUT5, OUT6, and OUT7 are 500mA, 150mA, 300mA, and 150mA, respectively. Each regulator has its own enable input. When enabled, a linear regulator soft-starts by ramping the outputs at 34V/ms. This limits inrush current when the regulators are enabled.

The LDO output voltages, OUT4, OUT5, OUT6, and OUT7 are pin programmable by SL1 and SL2 (Table 3). SL1 and SL2 are intended to be hardwired and cannot be driven by active logic. Changes to SL1 and SL2 after power-up are ignored.

VL Linear Regulator

VL is the output of a 3.3V linear regulator that powers the on-chip input limiter and charger control circuitry. VL is powered from DC and can provide up to 10mA when a DC source is present. Bypass VL to GND with a 0.1µF capacitor.

Regulator Enable Inputs (EN_)

The OUT1–OUT7 regulators have individual enable inputs. Drive EN_ high to initiate soft-start and enable OUT_. Drive EN_ low to disable OUT_. When disabled, each regulator (OUT1–OUT7) switches in an active pulldown resistor to discharge the output.

Soft-Start/Inrush Current

The MAX8662/MAX8663 implement soft-start on many levels to control inrush current and avoid collapsing source supply voltages. The input-voltage limit and battery charger have a 1.5ms soft-start time. All regulators also implement soft-start. White LED driver soft-start is accomplished by ramping the OVP current from 0 to 20µA in 1.25ms. During soft-start, the PWM controller forces 0% switching duty cycle to avoid an input current surge at turn-on.

Undervoltage and Overvoltage Lockout DC UVLO

When the DC voltage is below the DC undervoltage threshold (VUVLO_DC, typically 3.5V falling), the MAX8662/MAX8663 enter DC undervoltage lockout (DC UVLO). DC UVLO forces the power management circuits to a known dormant state until the DC voltage is high enough to allow the device to make accurate decisions. In DC UVLO, Q1 is open (Figure 2), the charger is disabled, POK is high-Z, and CHG is high-Z. The system load switch, Q2 (Figure 2) is closed in DC UVLO, allowing the battery to power the SYS node. All regulators are allowed to operate from the battery in DC UVLO.

CONNECT SL_TO:		LINEAR REGULATOR OUTPUT VOLTAGES			
SL ₁	SL ₂	OUT4 (V)	OUT5 (V)	OUT6 (V)	OUT7 (V)
Open circuit	Open circuit	3.3	3.3	3.3	3.3
Ground	Open circuit	3.3	2.85	1.85	1.85
SYS	Open circuit	2.85	2.85	1.85	1.85
Open circuit	Ground	3.3	2.85	2.85	1.85
Ground	Ground	2.5	3.3	1.5	1.5
SYS	Ground	2.5	3.3	1.5	1.3
Open circuit	SYS	1.2	1.8	1.1	1.3
Ground	SYS	3.3	2.85	1.5	1.5
SYS	SYS	1.8	2.5	3.3	2.85

Table 3. SL1 and SL2, Output Voltage Selection

DC OVLO

When the DC voltage is above the DC overvoltage threshold (VOVLO DC, typically 6.9V), the MAX8662/ MAX8663 enter DC overvoltage lockout (DC OVLO). DC OVLO mode protects the MAX8662/MAX8663 and downstream circuitry from high-voltage stress up to 9V. In DC OVLO, VL is on, Q1 (Figure 2) is open, the charger is disabled, \overline{POK} is high-Z, and \overline{CHG} is high-Z. The system load switch Q2 (Figure 2) is closed in DC OVLO, allowing the battery to power SYS. All regulators are allowed to operate from the battery in DC OVLO.

SYS UVLO

When the SYS voltage falls below the SYS undervoltage threshold (VUVLO_SYS, typically 2.4V falling), the MAX8662/MAX8663 enter SYS undervoltage lockout (SYS UVLO). SYS UVLO forces all regulators off. All regulators assume the states determined by the corresponding enable input (EN_) when the SYS voltage rises above VUVLO_SYS.

Input-Limiter Thermal Limiting

The MAX8662/MAX8663 reduce input-limiter current by 5%/°C when its die temperature exceeds +100°C. The system load (SYS) has priority over charger current, so input current is first reduced by lowering charge current. If the junction temperature still reaches +120°C in spite of charge-current reduction, no current is drawn from DC, the battery supplies the entire system load, and SYS is regulated at 100mV below BAT. Note that this on-chip thermal-limiting circuitry is not related to, and operates independently from, the thermistor input.

Regulator Thermal-Overload Shutdown

The MAX8662/MAX8663 disable all charger, SYS, and regulator outputs (except VL) if the junction temperature rises above +165°C, allowing the device to cool. When the junction temperature cools by approximately 15°C, resume the state they held prior to thermal overload. Note that this on-chip thermal-protection circuitry is not related to, and operates independently from, the thermistor input. Also note that thermal-overload shutdown is a fail-safe mechanism. Proper thermal design should ensure that the junction temperature of the MAX8662/MAX8663 never exceeds the absolute maximum rating of $+150^{\circ}$ C.

Applications Information

Step-Down Converters (OUT1 and OUT2)

Capacitor Selection

The input capacitor in a DC-DC converter reduces current peaks drawn from the battery or other input power source and reduces switching noise in the controller. The impedance of the input capacitor at the switching frequency should be less than the input source's output impedance so that high-frequency switching currents do not pass through the input source. The DC-DC converter output capacitor keeps output ripple small and ensures control-loop stability. The output capacitor must also have low impedance at the switching frequency. Ceramic capacitors with X5R or X7R dielectrics are highly recommended for both input and output capacitors due to their small size, low ESR, and small temperature coefficients.

See Table 4 for example OUT1/OUT2 input and output capacitors and manufacturers.

Table 4. External Components List (See Figure 1)

Table 4. External Components List (See Figure 1) (continued)

Power Dissipation

The MAX8662/MAX8663 have a thermal-limiting circuitry, as well as a shutdown feature to protect the IC from damage when the die temperature rises. To allow the maximum charging current and load current on each regulator, and to prevent thermal overload, it is important to ensure that the heat generated by the MAX8662/MAX8663 is dissipated into the PCB. The package's exposed paddle must be soldered to the PCB, with multiple vias tightly packed under the exposed paddle to ensure optimum thermal contact to the ground plane.

Table 5 shows the thermal characteristics of the MAX8662/MAX8663 packages. For example, the junction-to-case thermal resistance $(θ_{JC})$ of the MAX8663 is 1.7°C/W. When properly mounted on a multilayer PCB, the junction-to-ambient thermal resistance (θ_{JA}) is typically 28°C/W.

PCB Layout and Routing

High switching frequencies and relatively large peak currents make the PCB layout a very important aspect of design. Good design minimizes ground bounce, excessive EMI on the feedback paths, and voltage gradients in the ground plane, which can result in instability or regulation errors.

A separate low-noise analog ground plane containing the reference, linear regulator, signal ground, and GND must connect to the power-ground plane at only one point to minimize the effects of power-ground currents. PG_, DC power, and battery grounds must connect directly to the power-ground plane. Connect GND to the exposed paddle directly under the IC. Use multiple tightly spaced vias to the ground plane under the exposed paddle to help cool the IC.

Position input capacitors from DC, SYS, BAT, PV1, and PV2 to the power-ground plane as close as possible to the IC. Connect input capacitors and output capacitors from inputs of linear regulators to low-noise analog ground as close as possible to the IC. Connect the inductors, output capacitors, and feedback resistors as close to the IC as possible and keep the traces short, direct, and wide.

Refer to the MAX8662/MAX8663 evaluation kit for a suitable PCB layout example.

Table 5. MAX8662/MAX8663 Package Thermal Characteristics

Pin Configurations (continued) Pin Configuration

For the latest package outline information and land patterns, go to **www.maxim-ic.com/packages**. Note that a "+", "#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.

