MBRB30H30CT-1G, NRVBB30H30CT-1G, MBR30H30CTG

Switch-mode Power Rectifiers 30 V, 30 A

Features and Benefits

- Low Forward Voltage
- Low Power Loss/High Efficiency
- High Surge Capacity
- 150°C Operating Junction Temperature
- 30 A Total (15 A Per Diode Leg)
- Guard−Ring for Stress Protection
- NRVBB Prefix for Automotive and Other Applications Requiring Unique Site and Control Change Requirements; AEC−Q101 Qualified and PPAP Capable
- These Devices are Pb−Free and are RoHS Compliant

Applications

- Power Supply − Output Rectification
- Power Management
- Instrumentation

Mechanical Characteristics:

- Case: Epoxy, Molded
- Epoxy Meets UL 94 V−0 @ 0.125 in
- Weight: 1.5 Grams (I²PAK) (Approximately) 1.9 Grams (TO−220) (Approximately)
- Finish: All External Surfaces Corrosion Resistant and Terminal Leads are Readily Solderable
- Lead Temperature for Soldering Purposes: 260°C Max. for 10 Seconds

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ORDERING AND MARKING INFORMATION

See detailed ordering and shipping information on page [5](#page-4-0) of this data sheet.

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MAXIMUM RATINGS (Per Diode Leg)

Stresses exceeding those listed in the Maximum Ratings table may damage the device. If any of these limits are exceeded, device functionality should not be assumed, damage may occur and reliability may be affected.

1. The heat generated must be less than the thermal conductivity from Junction–to–Ambient: dP_D/dT_J < 1/R_{θJA}.

THERMAL CHARACTERISTICS

ELECTRICAL CHARACTERISTICS (Per Diode Leg)

Product parametric performance is indicated in the Electrical Characteristics for the listed test conditions, unless otherwise noted. Product performance may not be indicated by the Electrical Characteristics if operated under different conditions.

2. Pulse Test: Pulse Width = $300 \mu s$, Duty Cycle $\leq 2.0\%$.

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2

4 6

 $0\frac{1}{0}$

0 5 10 15

5 10

I_O, AVERAGE FORWARD CURRENT (AMPS)

20 25

Figure 6. Forward Power Dissipation

Figure 5. Current Derating T_{C} , CASE TEMPERATURE (°C)

130 160 140 150

110 120

10

5

0

100

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Figure 7. Typical Capacitance

Figure 8. Thermal Response Junction−to−Case

The unclamped inductive switching circuit shown in Figure 9 was used to demonstrate the controlled avalanche capability of this device. A mercury switch was used instead of an electronic switch to simulate a noisy environment when the switch was being opened.

When S_1 is closed at t_0 the current in the inductor I_L ramps up linearly; and energy is stored in the coil. At t_1 the switch is opened and the voltage across the diode under test begins to rise rapidly, due to di/dt effects, when this induced voltage reaches the breakdown voltage of the diode, it is clamped at BV_{DUT} and the diode begins to conduct the full load current which now starts to decay linearly through the diode, and goes to zero at t₂.

By solving the loop equation at the point in time when S_1 is opened; and calculating the energy that is transferred to the diode it can be shown that the total energy transferred is equal to the energy stored in the inductor plus a finite amount of energy from the V_{DD} power supply while the diode is in breakdown (from t_1 to t_2) minus any losses due to finite component resistances. Assuming the component resistive

ORDERING INFORMATION

Figure 9. Test Circuit Figure 10. Current−Voltage Waveforms

elements are small Equation (1) approximates the total energy transferred to the diode. It can be seen from this equation that if the V_{DD} voltage is low compared to the breakdown voltage of the device, the amount of energy contributed by the supply during breakdown is small and the total energy can be assumed to be nearly equal to the energy stored in the coil during the time when S_1 was closed, Equation (2).

EQUATION (1):

$$
W_{AVAL} \approx \frac{1}{2}LI_{LPK}^2 \left(\frac{BV_{DUT}}{BV_{DUT} - V_{DD}}\right)
$$

EQUATION (2):

 $W_{AVAL} \approx \frac{1}{2}LI_{LPK}^2$

DUSEWI

MAX.

 15.75

10.53

4.83

0.96

4.09

 2.66

4.10

0.61

14.27

 1.52

5.33

 3.04

2.79

1.41

6.47

 1.27

2.04

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