

# 2A, 2.5V to 5.5V, Synchronous Step-Down Converter with 25µA IQ in CSP Package

#### **DESCRIPTION**

The MP2192 is a monolithic, step-down switchmode converter with built-in internal power MOSFETs. The MP2192 achieves 2A of continuous output current from a 2.5V to 5.5V input voltage, with excellent load and line regulation. The output voltage can be regulated to as low as 0.6V.

Constant-on-time (COT) control provides fast transient response and eases loop stabilization. Fault protections include cycle-by-cycle current limiting and thermal shutdown.

The MP2192 is well-suited for a wide range of applications, including high-performance DSPs, wireless power, portable and mobile devices, and other low-power systems.

The MP2192 requires a minimal number of readily available. standard external components. It is available in an ultra-small CSP-6 (0.85mmx1.25mm) package.

### **FEATURES**

- Low 25uA lo
- 1.1MHz Switching Frequency
- **EN for Power Sequencing**
- 1% FB Accuracy
- Wide 2.5V to 5.5V Operating Input Range
- Output Adjustable from 0.6V
- Up to 2A Output Current
- $75m\Omega$  and  $45m\Omega$  Internal Power MOSFET Switches
- 100% Duty Cycle
- **Output Discharge**
- V<sub>OUT</sub> Over-Voltage Protection (OVP)
- Short-Circuit Protection (SCP) with Hiccup Mode
- Available in a WLCSP-6 (0.85mmx1.25mm) Package
- **Excellent Transient Response with Minimal Output Capacitors**

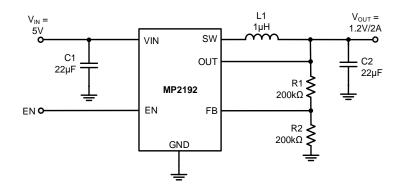
MPL Optimized Performance with MPS Inductor MPL-AL4020 Series

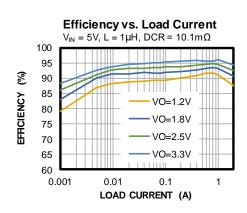
#### **APPLICATIONS**

- Solid State Drives (SSDs)
- Portable Instruments
- **Battery-Powered Devices**
- **Multi-Function Printers**

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### TYPICAL APPLICATION







## **ORDERING INFORMATION**

Part Number*	Package	Top Marking	V <sub>OUT</sub> Range	MSL Rating
MP2192GC	WLCSP-6 (0.85mmx1.25mm)	See Below	Adjustable	1

<sup>\*</sup> For Tape & Reel, add suffix –Z (e.g. MP2192GC–Z).

#### **TOP MARKING**

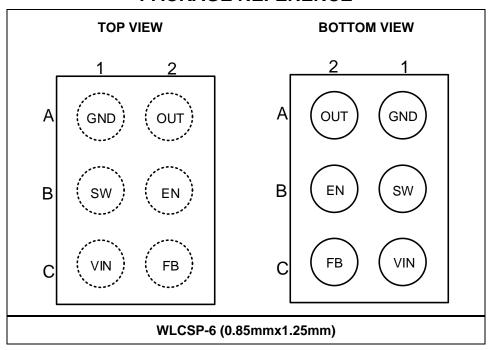
LMY

LLL

LM: Product code of MP2192GC

Y: Year code LLL: Lot number

## **PACKAGE REFERENCE**





#### PIN FUNCTIONS

Pin#	Name	Description
A1	GND	Power ground.
A2	OUT	Output sense. OUT is the voltage power rail and input sense pin for the output voltage. Use an output capacitor to reduce the output voltage ripple.
B1	SW	<b>Output switching node.</b> SW is the drain of the internal high-side P-channel MOSFET. Connect the inductor to SW to complete the converter.
B2	EN	On/off control.
C1	VIN	<b>Supply voltage.</b> The MP2192 operates from an unregulated input between 2.5V and 5.5V. A decoupling capacitor is required to prevent large voltage spikes from appearing at the input.
C2	FB	<b>Feedback.</b> An external resistor divider connected from the output to GND, then tapped to the FB pin, sets the output voltage.

## **ABSOLUTE MAXIMUM RATINGS (1)**

Supply voltage (V <sub>IN</sub> )	6.5V
V <sub>SW</sub>	0.3V (-5V for <10ns) to
	+6.5V (+10V for <10ns)
All other pins	0.3V to +6.5V
Junction temperature	150°C
Lead temperature	260°C
Continuous power dissip	pation $(T_A = 25^{\circ}C)$ (2) (4)
	1.39W
Storage temperature	65°C to +150°C

#### ESD Ratings

Human body model (HBM) ..... ±2000V Charged device model (CDM).. +1000V, -1500V

#### Recommended Operating Conditions (3)

Supply voltage (V<sub>IN</sub>) ......2.5V to 5.5V Operating junction temp (T<sub>J</sub>)....-40°C to +125°C

Thermal Resistance	$oldsymbol{ heta}_{JA}$	$oldsymbol{ heta}$ JC(TOP)
EVL2192-C-00A (4)	90	30°C/W
WLCSP-6 (5)	141	2°C/W

#### Notes:

- 1) Exceeding these ratings may damage the device.
- The maximum allowable power dissipation is a function of the maximum junction temperature,  $T_J$  (MAX), the junction-toambient thermal resistance,  $\theta_{JA}$ , and the ambient temperature,  $T_{\text{A}}$ . The maximum allowable continuous power dissipation at any ambient temperature is calculated by PD  $(MAX) = (T_J (MAX) - T_A) / \theta_{JA}$ . Exceeding the maximum allowable power dissipation may produce an excessive die temperature, and the device may go into thermal shutdown. Internal thermal shutdown circuitry protects the device from permanent damage.
- The device is not guaranteed to function outside of its operating conditions.
- Measured on the EVL2192-C-00A evaluation board, 2-layer
- Measured on JESD51-7, 4-layer PCB. The value of  $\theta_{JA}$  given in this table is only valid for comparison with other packages and cannot be used for design purposes. These values are calculated in accordance with JESD51-7, and simulated on a specified JEDEC board. They do not represent the performance obtained in an actual application.

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## **ELECTRICAL CHARACTERISTICS**

 $V_{IN}=3.6V$ ,  $T_J=-40^{\circ}C$  to +125°C  $^{(6)}$ , typical value is tested at  $T_J=25^{\circ}C$ . The over-temperature limit is guaranteed by characterization, unless otherwise noted.

Parameter	Symbol	Condition	Min	Тур	Max	Units	
VIN range			2.5		5.5	V	
UVLO threshold rising				2.3	2.45	V	
UVLO threshold hysteresis				135		mV	
Feedback voltage	voltage V <sub>FB</sub>	$T_J = 25$ °C, $2.5V \le V_{IN} \le 5.5V$ , $I_{OUT} = 0.1A$	594	600	606	mV	
reedback voltage	VFB	$T_J = -40^{\circ}\text{C to } +125^{\circ}\text{C},$ $I_{OUT} = 0.1\text{A}$	591	600	609	IIIV	
Feedback current	I <sub>FB</sub>	$V_{FB} = 0.63V$		50	100	nA	
P-channel MOSFET switch on resistance	RDS(ON)_P	V <sub>IN</sub> = 5V		75		mΩ	
N-channel MOSFET switch on resistance	R <sub>DS(ON)_N</sub>	V <sub>IN</sub> = 5V		45		mΩ	
Switch leakage		$V_{EN} = 0V$ , $V_{IN} = 6V$ , $T_J = 25$ °C, $V_{SW} = 0V$ and $6V$		0	1	μA	
P-channel MOSFET peak current limit			2.8	3.5	4.1	Α	
N-channel MOSFET valley current limit				2.5		Α	
ZCD				50		mA	
On time	tou	$V_{IN} = 5V$ , $V_{OUT} = 1.2V$		220		nc	
On time	ton	$V_{IN} = 3.6V, V_{OUT} = 1.2V$		300		ns	
Switching frequency	fsw	V <sub>OUT</sub> =1.2V, I <sub>OUT</sub> =0.5A		1100		kHz	
Minimum off time	t <sub>MIN-OFF</sub>			100		ns	
Minimum on time (7)	t <sub>мім-ом</sub>			60		ns	
Soft-start time	tss-on	Vout rising from 10% to 90%		1.1		ms	
EN turn-on delay		EN on to SW active		220		μs	
EN input logic low voltage					0.4	V	
EN input logic high voltage			1.2			V	
Output discharge resistor	Rois	$V_{EN} = 0V$ , $V_{OUT} = 1.2V$		13		Ω	
EN input current		$V_{EN} = 2V$		1.2		μΑ	
Liv input current		V <sub>EN</sub> = 0V		0		μΑ	
Supply current (shutdown)		$V_{EN} = 0V$ , $T_J = 25$ °C		0	1	μA	
Supply current (quiescent) Adjustable version		$V_{EN} = 2V$ , $V_{FB} = 0.63V$ , $V_{IN} = 5V$ , $T_{J} = 25^{\circ}C$		25	30	μA	
Output over-voltage threshold	V <sub>OVP</sub>		112%	117%	122%	V <sub>FB</sub>	
VOUT OVP hysteresis	V <sub>OVP_HYS</sub>			13%		$V_{FB}$	
OVP delay				12		μs	



## **ELECTRICAL CHARACTERISTICS** (continued)

 $V_{IN} = 3.6V$ ,  $T_J = -40$ °C to +125°C (6), typical value is tested at  $T_J = 25$ °C. The over-temperature limit is guaranteed by characterization, unless otherwise noted.

Parameter	Symbol	Condition	Min	Тур	Max	Units
Low-side current		Current flowing from SW to GND		1.5		Α
Absolute V <sub>IN</sub> OVP		After Vout OVP is enabled		6.2		V
Absolute V <sub>IN</sub> OVP hysteresis				400		mV
Thermal shutdown (7)				160		°C
Thermal hysteresis (7)				30		°C

#### Notes:

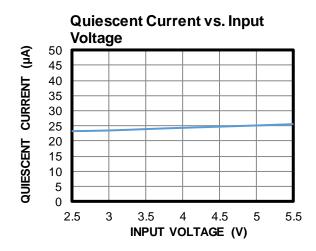
- 6) Not tested in production. Guaranteed by over-temperature correlation.
- 7) Guaranteed by engineering sample characterization.

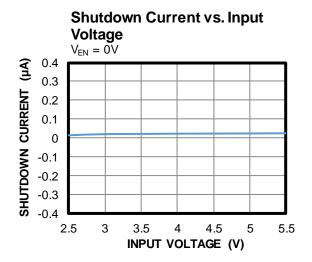
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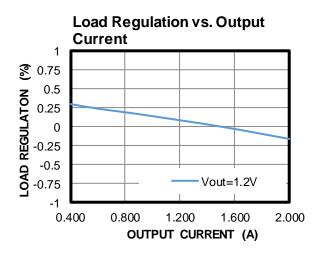


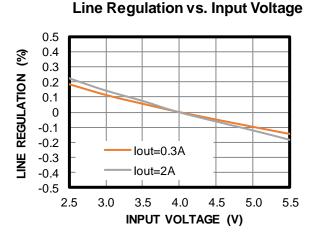
#### TYPICAL PERFORMANCE CHARACTERISTICS

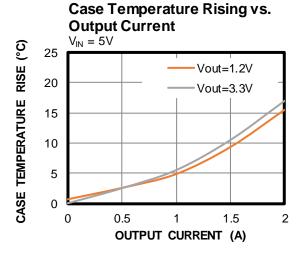
 $V_{IN} = 3.6V$ ,  $V_{OUT} = 1.2V$ ,  $L = 1\mu H$ ,  $C_{OUT} = 22\mu F$ ,  $T_A = 25^{\circ}C$ , unless otherwise noted.

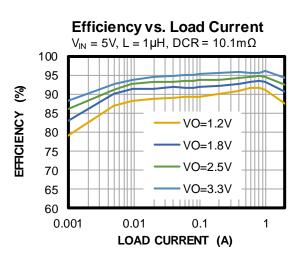








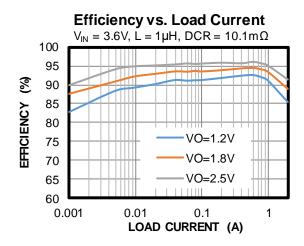


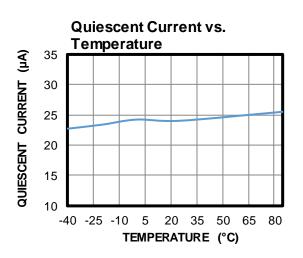


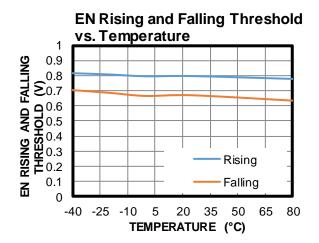


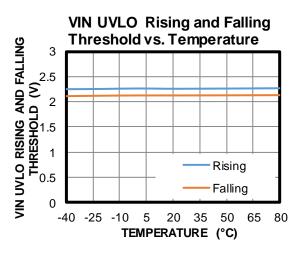
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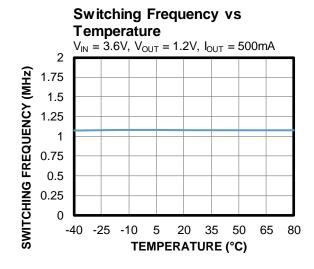
 $V_{IN} = 3.6V$ ,  $V_{OUT} = 1.2V$ ,  $L = 1\mu H$ ,  $C_{OUT} = 22\mu F$ ,  $T_A = 25^{\circ}C$ , unless otherwise noted.

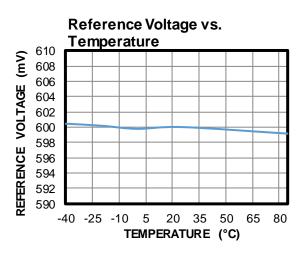








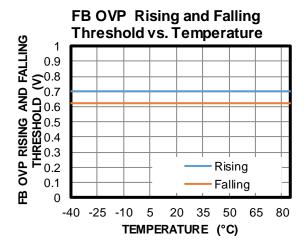


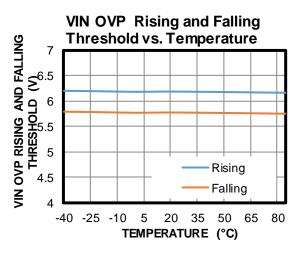




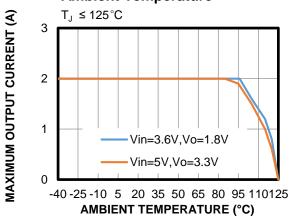
## TYPICAL CHARACTERISTICS (continued)

 $V_{IN} = 3.6V$ ,  $V_{OUT} = 1.2V$ ,  $L = 1\mu H$ ,  $C_{OUT} = 22\mu F$ ,  $T_A = 25^{\circ}C$ , unless otherwise noted.

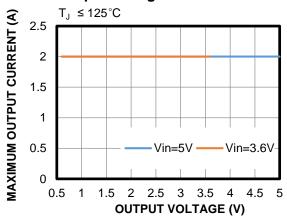


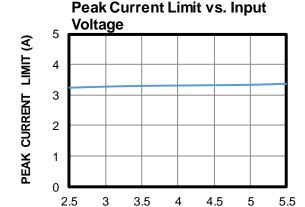


## Maximum Output Current vs. Ambient Temperature

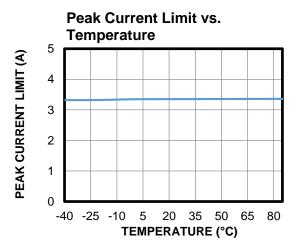


# Maximum Output Current vs. Output Voltage





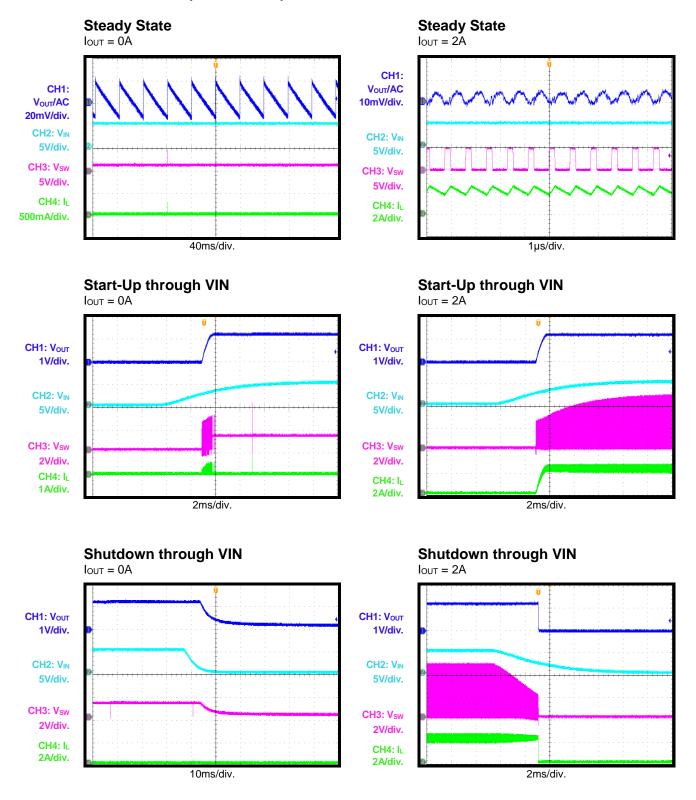
INPUT VOLTAGE (V)





## TYPICAL PERFORMANCE CHARACTERISTICS (continued)

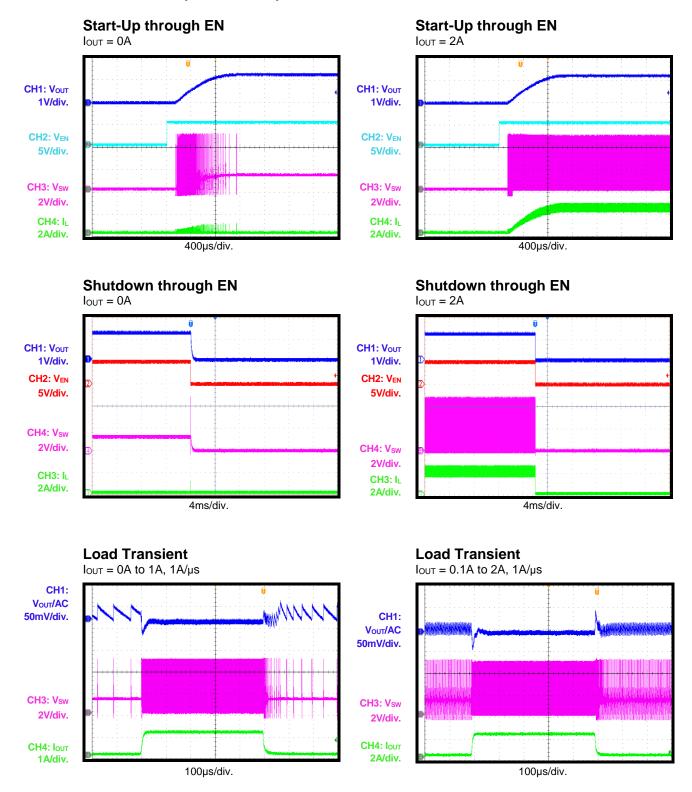
 $V_{IN}$  = 5V,  $V_{OUT}$  = 1.2V, L = 1 $\mu$ H,  $C_{OUT}$  = 22 $\mu$ F,  $T_A$  = 25°C, unless otherwise noted.





## TYPICAL PERFORMANCE CHARACTERISTICS (continued)

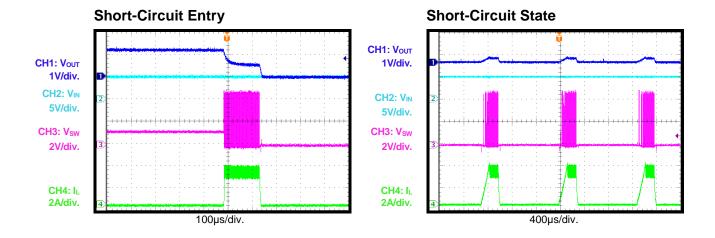
 $V_{IN}$  = 5V,  $V_{OUT}$  = 1.2V, L = 1 $\mu$ H,  $C_{OUT}$  = 22 $\mu$ F,  $T_A$  = 25°C, unless otherwise noted.

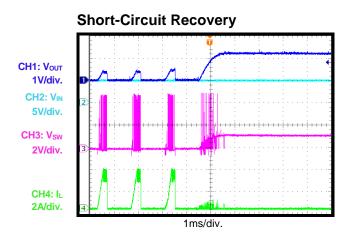




## TYPICAL PERFORMANCE CHARACTERISTICS (continued)

 $V_{IN}$  = 5V,  $V_{OUT}$  = 1.2V, L = 1 $\mu$ H,  $C_{OUT}$  = 22 $\mu$ F,  $T_A$  = 25°C, unless otherwise noted.

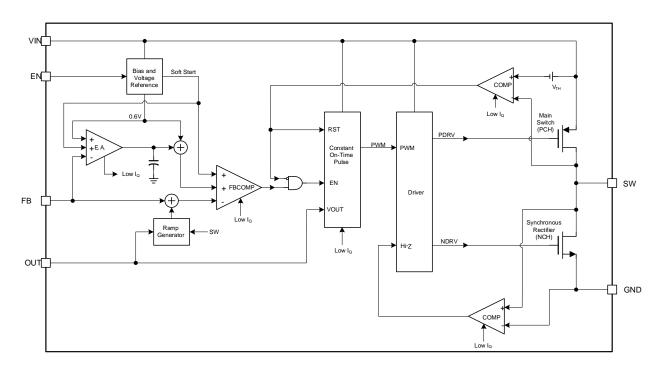




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## **FUNCTIONAL BLOCK DIAGRAM**



**Figure 1: Functional Block Diagram** 



#### **OPERATION**

The MP2192 uses constant-on-time control (COT) with input voltage feed-forward to stabilize the switching frequency across the entire input voltage range. The MP2192 achieves 2A of continuous output current from a 2.5V to 5.5V input voltage, with excellent load and line regulation. The output voltage can be regulated to as low as 0.6V.

#### **Constant-On-Time (COT) Control**

When compared to the fixed-frequency pulsewidth modulation (PWM) control, constant-on-time (COT) control offers a simpler control loop and a faster transient response. By using input voltage feed-forward, the MP2192 maintains a fairly constant switching frequency across the input and output voltage ranges. The switching pulse on time  $(t_{\text{ON}})$  can be estimated with Equation (1):

$$t_{ON} = \frac{V_{OUT}}{V_{IN}} \times 0.91 \mu s \tag{1}$$

To prevent inductor current runaway during the load transient, the MP2192 has a fixed minimum off time of 100ns.

#### **Sleep Mode Operation**

The MP2192 features sleep mode to achieve high efficiency at extremely light loads. In sleep mode, most of the circuit blocks are turned off except for the error amplifier (EA) and PWM comparator. This reduces the operation current to a minimal value (see Figure 2).

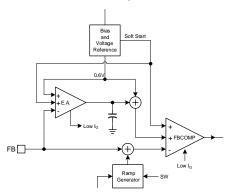


Figure 2: Operation Blocks in Sleep Mode

When the load becomes lighter, the output voltage ripple becomes larger, which then drives the error amplifier output (EAO) lower. When the EAO reaches the internal low

threshold, it is clamped at that level, and the MP2192 enters sleep mode.

During sleep mode, the valley of the FB voltage  $(V_{FB})$  is regulated to the internal reference voltage. Therefore, the average output voltage in sleep mode exceeds the output voltage in discontinuous conduction mode (DCM) or continuous conduction mode (CCM). The ontime pulse in sleep mode is longer than the ontime pulse in DCM or CCM. Figure 3 shows the relationship between the average  $V_{FB}$  and the internal reference voltage  $(V_{REF})$  in sleep mode.



Figure 3: FB Average Voltage in Sleep Mode

When the MP2192 is in sleep mode, the average output voltage exceeds the internal reference voltage. The EAO stays low and is clamped in sleep mode. When the load **PWM** increases. the switching period decreases to regulate the output voltage ripple. The output voltage ripple drops relative to the PWM switching period. Once the EAO exceeds the internal low threshold, the MP2192 exits sleep mode and enters either DCM or CCM, depending on the load. In DCM or CCM, the EA regulates the average output voltage to V<sub>REF</sub> (see Figure 4).



Figure 4: DCM Control

Due to the EA's clamping response time, there is always a loading hysteresis when entering or exiting sleep mode.

# Advanced Asynchronous Modulation (AAM) during Light-Load Operation

The MP2192 uses advanced asynchronous modulation (AAM) power-save mode and a zero-current detection (ZCD) circuit for light-load operation.

The MP2192 uses AAM power-save mode for light loads (see Figure 5). The AAM current ( $I_{AAM}$ ) is set internally. The SW on-pulse time is determined by the on-time generator and AAM comparator.



Figure 5: Simplified AAM Control Logic

Under light-load conditions, the SW on-pulse time is the longer pulse. If the AAM comparator pulse is longer than the on-time generator, the operation mode is controlled by AAM (see Figure 6).

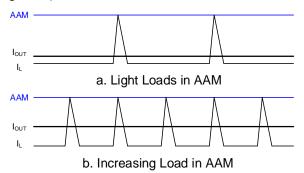


Figure 6: The AAM Comparator Controls ton

If the AAM comparator pulse is shorter than the on-time generator, the operation mode is controlled by the on-time generator (see Figure 7).

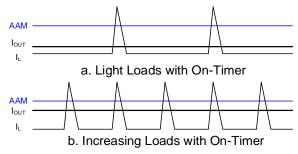


Figure 7: The On-Timer Controls ton

Figure 8 shows that when the AAM threshold decreases, ton increases gradually. For CCM, lour must exceed at least 50% of the AAM threshold. Generally, the AAM threshold is below the inductor current during normal duty cycles.

The MP2192 uses ZCD to determine if the inductor current has started reversing. When the inductor current reaches the ZCD threshold, the LS-FET turns off.

AAM with a ZCD circuit forces the MP2192 to work in DCM under light loads, even if Vout is close to V<sub>IN</sub>.

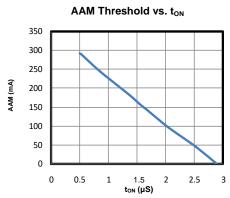


Figure 8: AAM Threshold Decreases as ton **Increases** 

#### Enable (EN)

If the input voltage exceeds the under-voltage lockout (UVLO) threshold (typically 2.3V), the MP2192 can be enabled by pulling EN above 1.2V. Leave EN floating or pull EN down to ground to disable the MP2192. There is an internal  $1M\Omega$  resistor connected from EN to ground.

When the device is disabled, the part enters output discharge mode automatically. The device's internal discharge MOSFET provides a resistive discharge path for the output capacitor.

#### Soft Start (SS)

The MP2192 has built-in soft start that ramps up the output voltage at a controlled slew rate to avoid overshooting at start-up. The soft-start time is about 1.1ms.

#### **Current Limit**

The MP2192 has a typical 3.5A HS-FET current limit. When the high-side switch reaches its current limit, the MP2192 remains in hiccup mode until the current drops. This prevents the inductor current from continuing to rise and damaging components.

#### **Short Circuit and Recovery**

The MP2192 triggers short-circuit protection (SCP) when it reaches its current limit and attempts to recover with hiccup mode. The MP2192 disables the output power stage, discharges soft-start capacitor, the attempts soft start again automatically. If the short-circuit condition remains after soft start ends, the MP2192 repeats this cycle until the



short circuit is removed and the output rises back to the regulation level.

#### Over-Voltage Protection (Vout OVP)

The MP2192 monitors V<sub>FB</sub> to detect overvoltage (OV) conditions. If V<sub>FB</sub> rises above 117% of the target voltage, the controller enters a dynamic regulation period. During this period, the LS-FET stays on until the low-side current drops to -1.5A. This discharges the output to keep it within the normal range.

If the OV condition still remains, the LS-FET turns on again after a 1µs time delay. The MP2192 exits this regulation period when V<sub>FB</sub> drops below 104% of V<sub>REF</sub>. If the dynamic regulation cannot limit the increasing output voltage, and input OVP occurs when VIN exceeds 6.2V, the MP2192 stops switching until the input voltage drops below 5.7V. Then the MP2192 resumes operation.



#### APPLICATION INFORMATION

#### **Setting the Output Voltage**

The external resistor divider sets the output voltage (see the Typical Application Circuit on page 18). Select a feedback resistor (R1) that reduces the output voltage leakage current. It is recommended for R1 to be between 100kΩ and  $200k\Omega$ . There is no strict requirement for the feedback resistor. Select R1 to exceed  $10k\Omega$ . R2 can then be calculated with Equation (2):

$$R2 = \frac{R1}{\frac{V_{OUT}}{0.6} - 1}$$
 (2)

Figure 9 shows the feedback circuit.

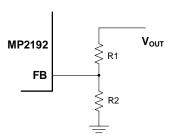


Figure 9: Feedback Network

Table 1 lists recommended resistor values for common output voltages.

**Table1: Resistor Selection for Common Output Voltages** 

V <sub>OUT</sub> (V)	R1 (kΩ)	R2 (kΩ)
1.0	200 (1%)	300 (1%)
1.2	200 (1%)	200 (1%)
1.8	200 (1%)	100 (1%)
2.5	200 (1%)	63.2 (1%)
3.3	200 (1%)	44.2 (1%)

#### Selecting the Inductor

Most applications work best with a 1µH to 2.2µH inductor. Select an inductor with a DC resistance below  $50m\Omega$  to optimize efficiency.

A high-frequency switch-mode power supply with a magnetic device has strong electronic magnetic inference. Do not use unshielded power inductors. Metal alloy inductors or multiplayer chip power inductors are ideal shielded inductors because they can effectively reduce electromagnetic interference.

For most designs, estimate the inductance value with Equation (3):

$$L_{1} = \frac{V_{OUT} \times (V_{IN} - V_{OUT})}{V_{IN} \times \Delta I_{L} \times f_{OSC}}$$
(3)

Where  $\Delta I_{\perp}$  is the inductor ripple current.

the Choose inductor current be approximately 30% of the maximum load current. The maximum inductor peak current can be calculated with Equation (4):

$$I_{L(MAX)} = I_{LOAD} + \frac{\Delta I_{L}}{2}$$
 (4)

MPS inductors are optimized and tested for use with our complete line of integrated circuits. 2 lists our power inductor recommendations.

**Table 2: Power Inductor Selection** 

Part Number	Inductance Value	Manufacturer		
MPL-AL4020-1R0	1µH	MPS		
MPL-AL4020-1R2	1.2µH	MPS		
MPL-AL4020-1R5	1.5µH	MPS		
MPL-AL4020-2R2	2.2µH	MPS		

Visit MonolithicPower.com under Products > Inductors for more information.

#### Selecting the Input Capacitor

The step-down converter has a discontinuous input current, and requires a capacitor to supply AC current to the converter while maintaining the DC input voltage. Use low-ESR capacitors for the best performance. Ceramic capacitors with X5R or X7R dielectrics are highly recommended due to their low ESR and small temperature coefficients. For most applications, a 22µF capacitor is sufficient. Higher output voltages may require a 44µF capacitor to increase system stability.

The input capacitor requires an adequate ripple current rating since it absorbs the input switching current. Estimate the RMS current in the input capacitor with Equation (5):

$$I_{C1} = I_{LOAD} \times \sqrt{\frac{V_{OUT}}{V_{IN}}} \left( 1 - \frac{V_{OUT}}{V_{IN}} \right)$$
 (5)



The worst-case condition occurs at  $V_{IN} = 2V_{OUT}$ , calculated with Equation (6):

$$I_{C1} = \frac{I_{LOAD}}{2} \tag{6}$$

For simplification, choose an input capacitor with an RMS current rating greater than half of the maximum load current.

The input capacitor can be electrolytic, tantalum, or ceramic. When using electrolytic or tantalum capacitors, add a small, high-quality, 0.1µF ceramic capacitor as close to the IC as possible. When using ceramic capacitors, ensure that they have enough capacitance to provide a sufficient charge to prevent excessive voltage ripple at the input. The input voltage ripple caused by the capacitance can be estimated with Equation (7):

$$\Delta V_{IN} = \frac{I_{LOAD}}{f_{SW} \times C1} \times \frac{V_{OUT}}{V_{IN}} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$
 (7)

#### **Selecting the Output Capacitor**

The output capacitor (C2) stabilizes the DC output voltage. Low-ESR ceramic capacitors are recommended to limit the output voltage ripple. Estimate the output voltage ripple with Equation (8):

$$\Delta V_{\text{OUT}} = \frac{V_{\text{OUT}}}{f_{\text{SW}} \times L_{1}} \times \left(1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}\right) \times \left(R_{\text{ESR}} + \frac{1}{8 \times f_{\text{SW}} \times C2}\right) (8)$$

Where  $L_1$  is the inductor value, and  $R_{\text{ESR}}$  is the equivalent series resistance (ESR) value of the output capacitor.

When using ceramic capacitors, the capacitance dominates the impedance at the switching frequency and causes most of the output voltage ripple. For simplification, the output voltage ripple can be estimated with Equation (9):

$$\Delta V_{\text{OUT}} = \frac{V_{\text{OUT}}}{8 \times f_{\text{SW}}^2 \times L_1 \times C2} \times \left(1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}\right) \quad (9)$$

For tantalum or electrolytic capacitors, the ESR dominates the impedance at the switching frequency. For simplification, the output ripple can be calculated with Equation (10):

$$\Delta V_{\text{OUT}} = \frac{V_{\text{OUT}}}{f_{\text{SW}} \times L_{\text{1}}} \times \left(1 - \frac{V_{\text{OUT}}}{V_{\text{IN}}}\right) \times R_{\text{ESR}} \tag{10}$$

The characteristics of the output capacitor also affect the stability of the regulation system.

#### Design Example

Table 3 lists a design example following the application guidelines for the specifications below.

**Table 3: Design Example** 

V <sub>IN</sub>	5V		
V <sub>out</sub>	1.2V		
f <sub>SW</sub>	1100kHz		

For the detailed application schematic, see Figure 11 on page 19. For the typical performance and circuit waveforms, see the Typical Performance Characteristics section on page 6. For more device applications, refer to the related evaluation board datasheets.



#### **PCB Layout Guidelines**

Efficient PCB layout is critical for stable operation. For the high-frequency switching converter, a poor layout design can result in poor line or load regulation and stability issues. For the best results, refer to Figure 10 and follow the guidelines below:

- 1. Place the high-current paths (GND, VIN, and SW) close to the device with short, direct, and wide traces.
- 2. Place the input capacitor as close to VIN and GND as possible.
- 3. Place the external feedback resistors next to FB.
- 4. Keep the switching node (SW) short, and route it away from the feedback network.
- 5. Keep the  $V_{\text{OUT}}$  sense line as short as possible, and and away from the power inductor (especially the surrounding inductor).

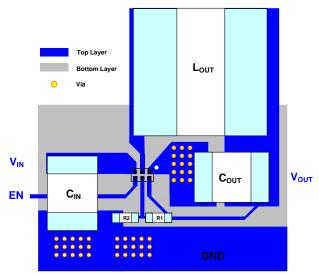


Figure 10: Recommended PCB Layout



## **TYPICAL APPLICATION CIRCUITS**

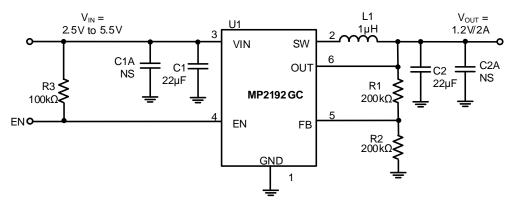


Figure 11: Typical Application Circuit for the MP2192GC

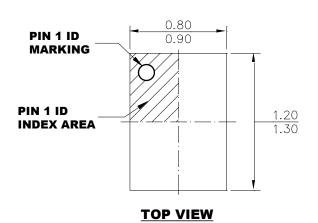
#### Note:

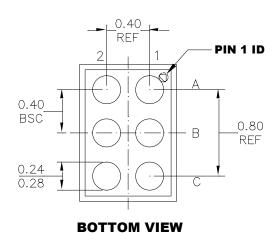
8) For applications where  $V_{\text{IN}}$  < 3.3V, additional input capacitors may be required.

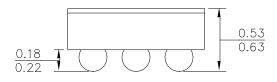


## **PACKAGE INFORMATION**

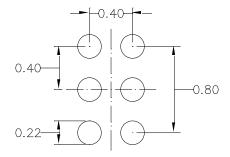
### WLCSP-6 (0.85mmx1.25mm)







**SIDE VIEW** 



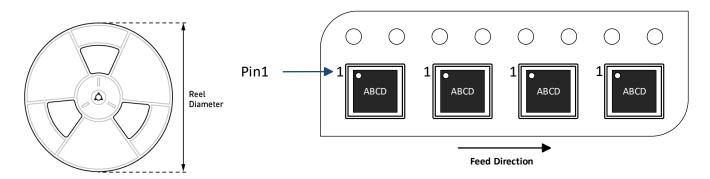
### RECOMMENDED LAND PATTERN

#### **NOTE:**

- 1) ALL DIMENSIONS ARE IN MILLIMETERS.
- 2) BALL COPLANARITY SHALL BE 0.05 MILLIMETER MAX.
- 3) JEDEC REFERENCE IS MO-211.
- 4) DRAWING IS NOT TO SCALE.



## **CARRIER INFORMATION**



Part Number	Package Description	Quantity/ Reel	Quantity/ Tube	Quantity/ Tray	Reel Diameter	Carrier Tape Width	Carrier Tape Pitch
MP2192GC-Z	WLCSP-6 (0.85mmx1.25mm)	3000	N/A	N/A	7in	8mm	4mm