

## Dual High-Efficiency PWM Step-Down DC/DC Converter

### General Description

The RT8020 is a dual high-efficiency Pulse-Width-Modulated (PWM) step-down DC/DC converter. It is capable of delivering 1A output current over a wide input voltage range from 2.5V to 5.5V, the RT8020 is ideally suited for portable electronic devices that are powered from 1-cell Li-ion battery or from other power sources within the range such as cellular phones, PDAs and other hand-held devices.

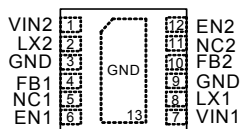
Two operational modes are available : PWM/Low-Dropout auto-switch and shutdown modes. Internal synchronous rectifier with low  $R_{DS(ON)}$  dramatically reduces conduction loss at PWM mode. No external Schottky diode is required in practical application.

The RT8020 enters Low-Dropout mode when normal PWM cannot provide regulated output voltage by continuously turning on the upper PMOS. The RT8020 enter shutdown mode and consumes less than 0.1 $\mu$ A when EN pin is pulled low.

The switching ripple is easily smoothed-out by small package filtering elements due to a fixed operation frequency of 1.5MHz. This along with small WDFN-12L 3x3 package provides small PCB area application. Other features include soft start, lower internal reference voltage with 2% accuracy, over temperature protection, and over current protection.

### Pin Configurations

(TOP VIEW)



WDFN-12L 3x3

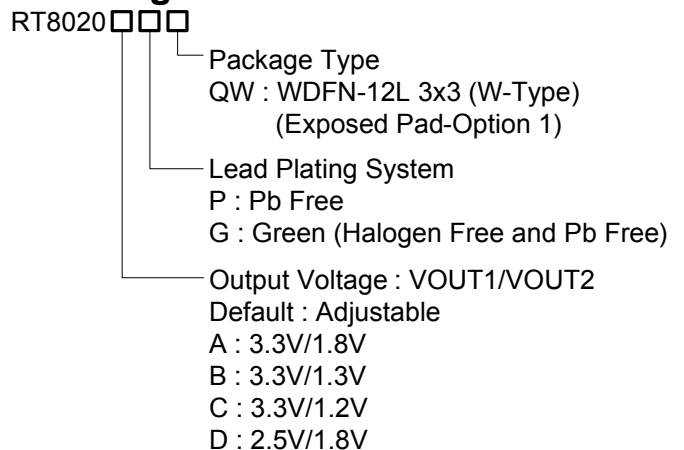
### Features

- 2.5V to 5.5V Input Range
- Adjustable Output From 0.6V to  $V_{IN}$
- 1.2V, 1.3V, 1.8V, 2.5V and 3.3V Fixed/ Adjustable Output Voltage
- 1A Output Current
- 95% Efficiency
- No Schottky Diode Required
- 50 $\mu$ A Quiescent Current per Channel
- 1.5MHz Fixed Frequency PWM Operation
- Small 12-Lead WDFN Package
- RoHS Compliant and 100% Lead (Pb)-Free

### Applications

- Mobile Phones
- Personal Information Appliances
- Wireless and DSL Modems
- MP3 Players
- Portable Instruments

### Ordering Information



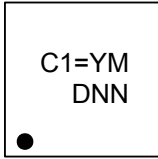
Note :

Richtek products are :

- ▶ RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- ▶ Suitable for use in SnPb or Pb-free soldering processes.

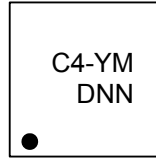
## Marking Information

RT8020GQW



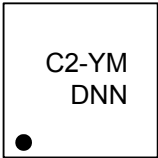
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YMDNN : Date Code

RT8020CPQW



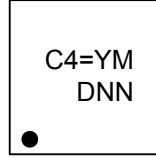
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RT8020APQW



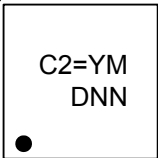
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RT8020CGQW



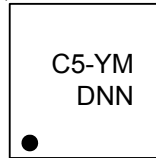
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RT8020AGQW



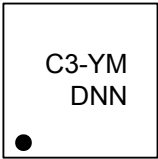
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RT8020DPQW



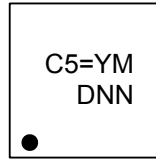
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RT8020BPQW



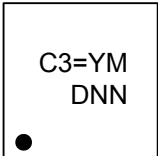
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RT8020DGQW



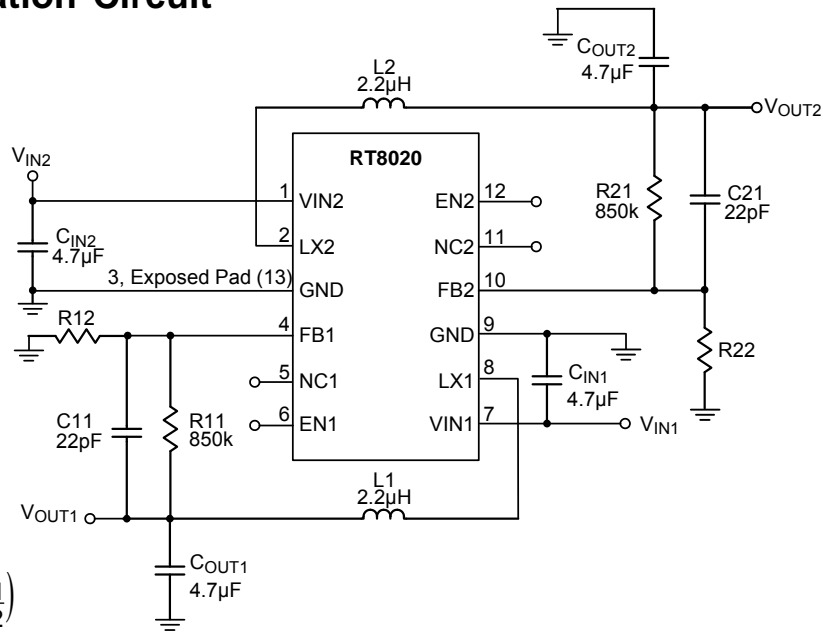
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RT8020BGQW



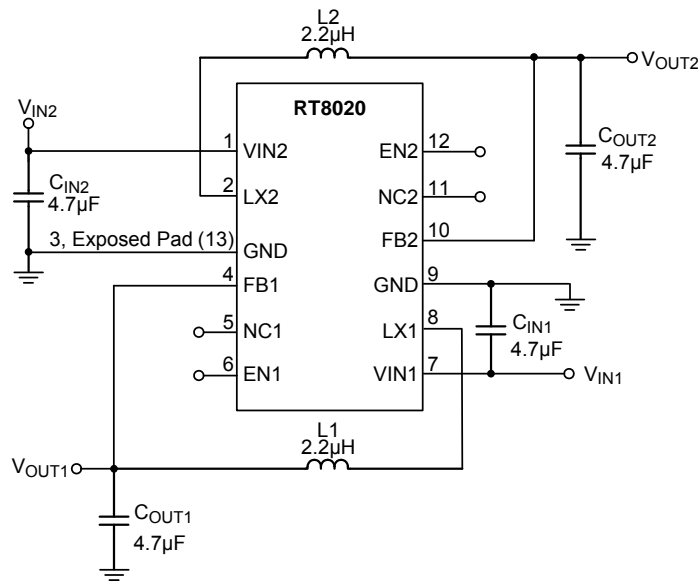
C3= : Product Code  
YMDNN : Date Code

**Typical Application Circuit**



$$V_{OUTx} = V_{REF} \times \left(1 + \frac{R_{x1}}{R_{x2}}\right)$$

Figure 1. Adjustable Voltage Regulator



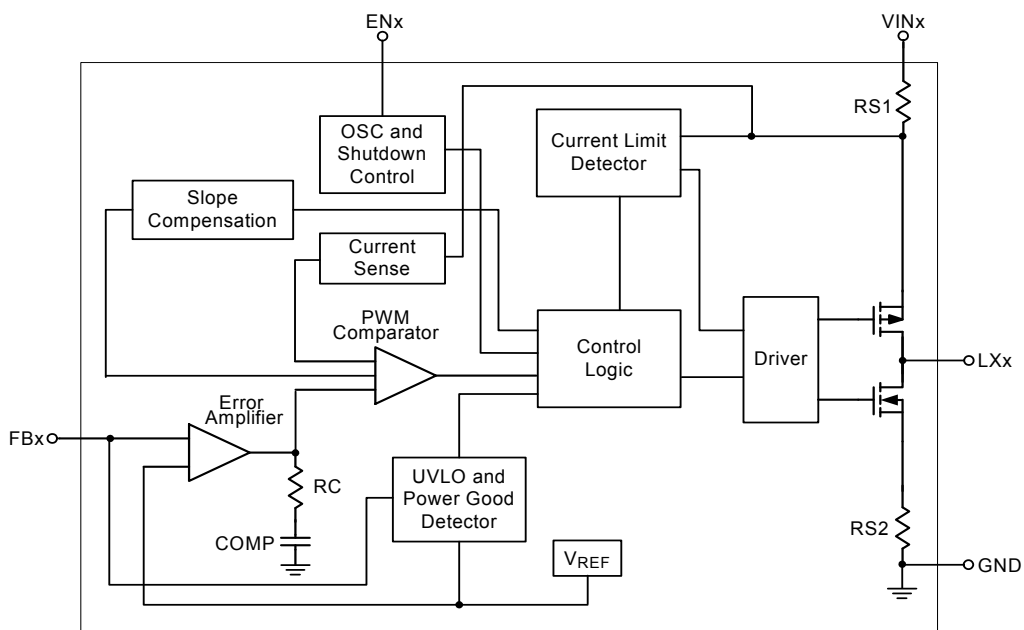
$V_{OUTx} = 1.2V, 1.3V, 1.8V, 2.5V \text{ or } 3.3V$

Figure 2. Fixed Voltage Regulator

Functional Pin Description

Pin No.	Pin Name	Pin Function
1	VIN2	Power Input of Channel 2.
2	LX2	Pin for Switching of Channel 2.
3, 9, Exposed Pad (13)	GND	Ground. The exposed pad must be soldered to a large PCB and connected to GND for maximum power dissipation.
4	FB1	Feedback of Channel 1.
5, 11	NC1, NC2	No Connection or Connect to $V_{IN}$ .
6	EN1	Chip Enable of Channel 1 (Active High). $V_{EN1} \leq V_{IN1}$ .
7	VIN1	Power Input of Channel 1.
8	LX1	Pin for Switching of Channel 1.
10	FB2	Feedback of Channel 2.
12	EN2	Chip Enable of Channel 2 (Active High). $V_{EN2} \leq V_{IN2}$ .

Function Block Diagram



**Absolute Maximum Ratings** (Note 1)

- Supply Input Voltage,  $V_{IN1}$ ,  $V_{IN2}$  ----- -0.3V to 6.5V
- EN1, FB1, LX1, EN2, FB2 and LX2 Pin Voltage ----- -0.3V to ( $V_{IN} + 0.3V$ )
- LX1 to GND, LX2 to GND (<200ns) ----- -1.5V to 7.5V
- Power Dissipation,  $P_D$  @  $T_A = 25^\circ C$ 
  - WDFN-12L 3x3 ----- 1.667W
- Package Thermal Resistance (Note 2)
  - WDFN-12L 3x3,  $\theta_{JA}$  -----  $60^\circ C/W$
  - WDFN-12L 3x3,  $\theta_{JC}$  -----  $8.2^\circ C/W$
- Lead Temperature (Soldering, 10 sec.) -----  $260^\circ C$
- Junction Temperature -----  $150^\circ C$
- Storage Temperature Range -----  $-65^\circ C$  to  $150^\circ C$
- ESD Susceptibility (Note 3)
  - HBM (Human Body Model) ----- 2kV
  - MM (Machine Model) ----- 200V

**Recommended Operating Conditions** (Note 4)

- Supply Input Voltage ----- 2.5V to 5.5V
- Junction Temperature Range -----  $-40^\circ C$  to  $125^\circ C$
- Ambient Temperature Range -----  $-40^\circ C$  to  $85^\circ C$

**Electrical Characteristics**

( $V_{IN} = 3.6V$ ,  $V_{OUT} = 2.5V$ ,  $V_{REF} = 0.6V$ ,  $L = 2.2\mu H$ ,  $C_{IN} = 4.7\mu F$ ,  $C_{OUT} = 10\mu F$ ,  $T_A = 25^\circ C$ ,  $I_{MAX} = 1A$  unless otherwise specified)

Parameter	Symbol	Test Conditions	Min	Typ	Max	Unit	
<b>Channel 1 and Channel 2</b>							
Input Voltage Range	$V_{IN}$		2.5	--	5.5	V	
Under Voltage Lock Out threshold	UVLO		--	1.8	--	V	
Hysteresis			--	0.1	--	V	
Quiescent Current	$I_Q$	$I_{OUT} = 0mA$ , $V_{FB} = V_{REF} + 5\%$	--	50	70	$\mu A$	
Shutdown Current	$I_{SHDN}$	EN = GND	--	0.1	1	$\mu A$	
Reference Voltage	$V_{REF}$	For Adjustable Output Voltage	0.588	0.6	0.612	V	
Adjustable Output Voltage Range	$V_{OUT}$	(Note 6)	$V_{REF}$	--	$V_{IN} - \Delta V$	V	
Output Voltage Accuracy	Fix	$\Delta V_{OUT}$	$V_{IN} = 2.5V$ to $5.5V$ , $V_{OUT} = 1.2V$ $0A < I_{OUT} < 1A$	-3	--	3	%
		$\Delta V_{OUT}$	$V_{IN} = 2.5V$ to $5.5V$ , $V_{OUT} = 1.3V$ $0A < I_{OUT} < 1A$	-3	--	3	%
		$\Delta V_{OUT}$	$V_{IN} = 2.5$ to $5.5V$ , $V_{OUT} = 1.8V$ $0A < I_{OUT} < 1A$	-3	--	3	%
		$\Delta V_{OUT}$	$V_{IN} = V_{OUT} + \Delta V$ to $5.5V$ (Note 5) $V_{OUT} = 2.5V$ , $0A < I_{OUT} < 1A$	-3	--	3	%
		$\Delta V_{OUT}$	$V_{IN} = V_{OUT} + \Delta V$ to $5.5V$ (Note 5) $V_{OUT} = 3.3V$ , $0A < I_{OUT} < 1A$	-3	--	3	%

Parameter		Symbol	Test Conditions	Min	Typ	Max	Unit	
Output Voltage Accuracy	Adjustable	$\Delta V_{OUT}$	$V_{IN} = V_{OUT} + \Delta V$ to 5.5V (Note 5) $0A < I_{OUT} < 1A$	-3	--	3	%	
FB Input Current		$I_{FB}$	$V_{FB} = V_{IN}$	-50	--	50	nA	
R <sub>DS(ON)</sub> of P-MOSFET		R <sub>DS(ON)_P</sub>	I <sub>OUT</sub> = 200mA	V <sub>IN</sub> = 2.5V	--	0.38	--	Ω
				V <sub>IN</sub> = 3.6V	--	0.28	--	
R <sub>DS(ON)</sub> of N-MOSFET		R <sub>DS(ON)_N</sub>	I <sub>OUT</sub> = 200mA	V <sub>IN</sub> = 2.5V	--	0.35	--	Ω
				V <sub>IN</sub> = 3.6V	--	0.25	--	
P-Channel Current Limit		I <sub>LIM_P</sub>	V <sub>IN</sub> = 2.5V to 5.5 V	1.4	1.5	--	A	
EN Input Voltage	Logic-High	V <sub>EN_H</sub>	V <sub>IN</sub> = 2.5V to 5.5V	1.5	--	V <sub>IN</sub>	V	
	Logic-Low	V <sub>EN_L</sub>	V <sub>IN</sub> = 2.5V to 5.5V	--	--	0.4		
Oscillator Frequency		f <sub>OSC</sub>	V <sub>IN</sub> = 3.6V, I <sub>OUT</sub> = 100mA	1.2	1.5	1.8	MHz	
Thermal Shutdown Temperature		T <sub>SD</sub>		--	160	--	°C	
Maximum Duty Cycle				100	--	--	%	
LX Leakage Current		I <sub>LX</sub>	V <sub>IN</sub> = 3.6V, V <sub>LX</sub> = 0V or V <sub>LX</sub> = 3.6V	-1	--	1	μA	

**Note 1.** Stresses beyond those listed “Absolute Maximum Ratings” may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.

**Note 2.**  $\theta_{JA}$  is measured at  $T_A = 25^\circ\text{C}$  on a high effective thermal conductivity four-layer test board per JEDEC 51-7.  $\theta_{JC}$  is measured at the exposed pad of the package.

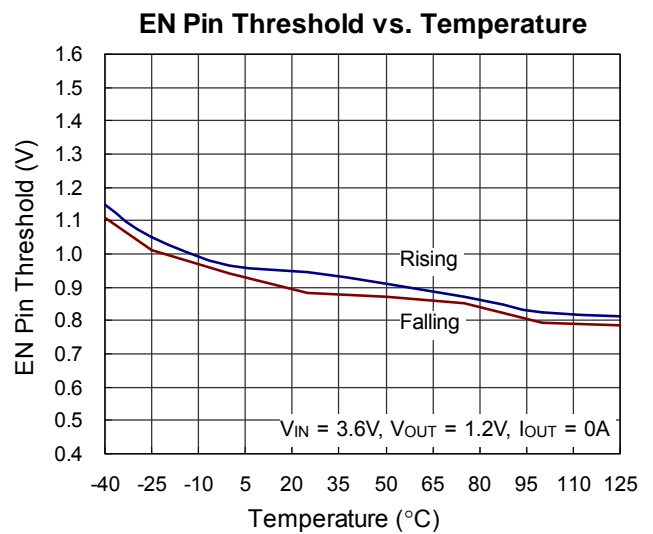
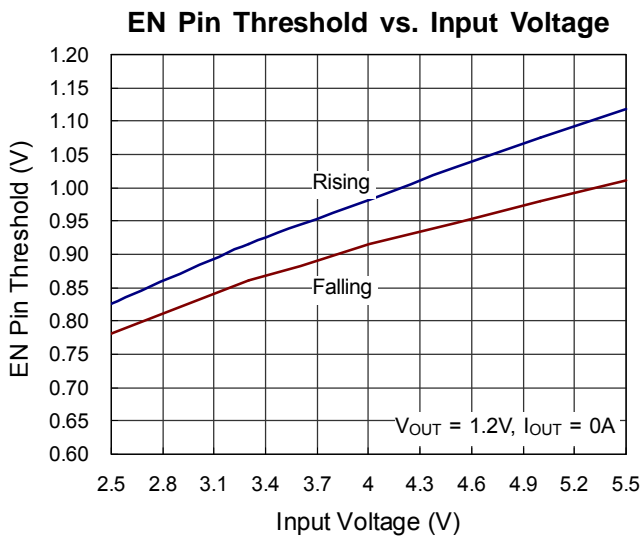
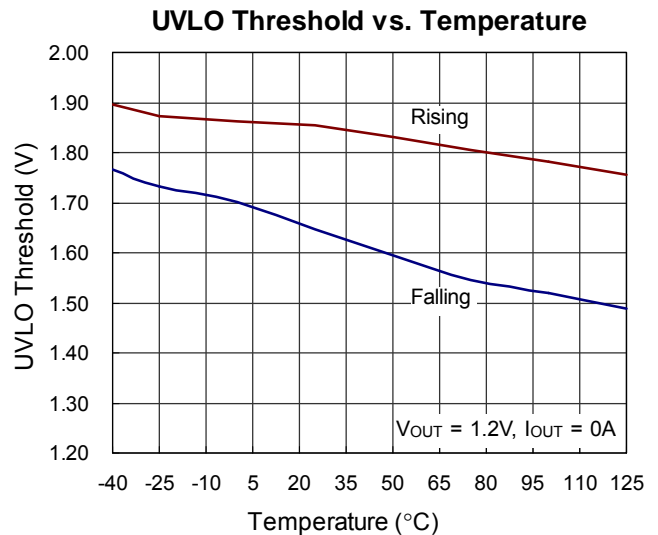
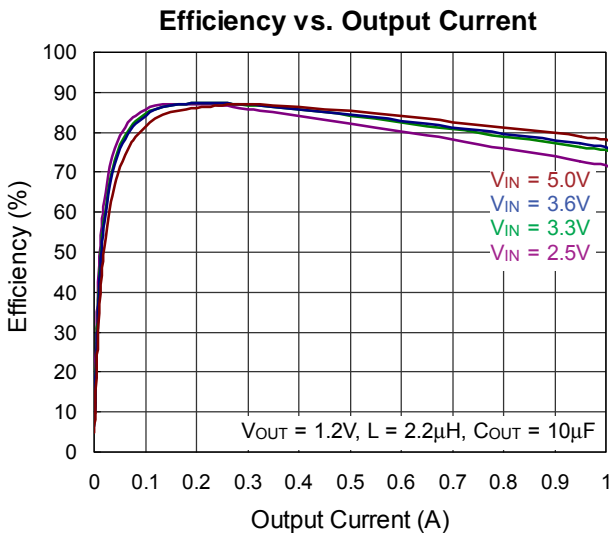
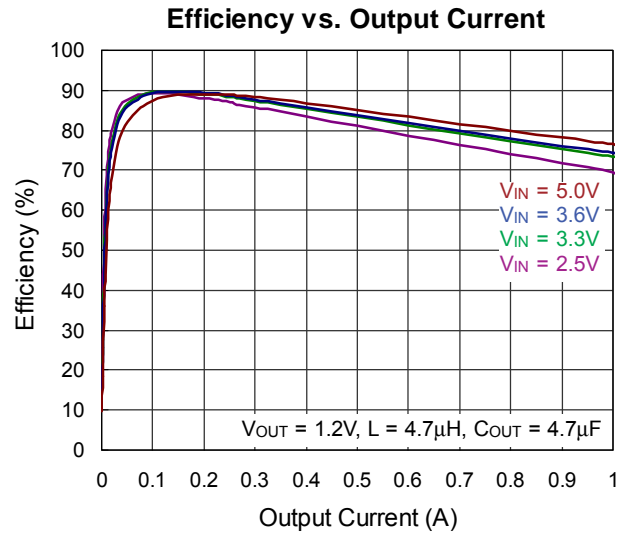
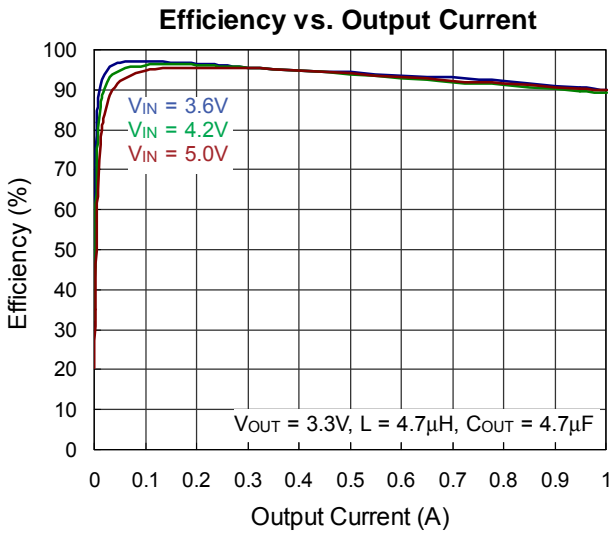
**Note 3.** Devices are ESD sensitive. Handling precaution recommended.

**Note 4.** The device is not guaranteed to function outside its operating conditions.

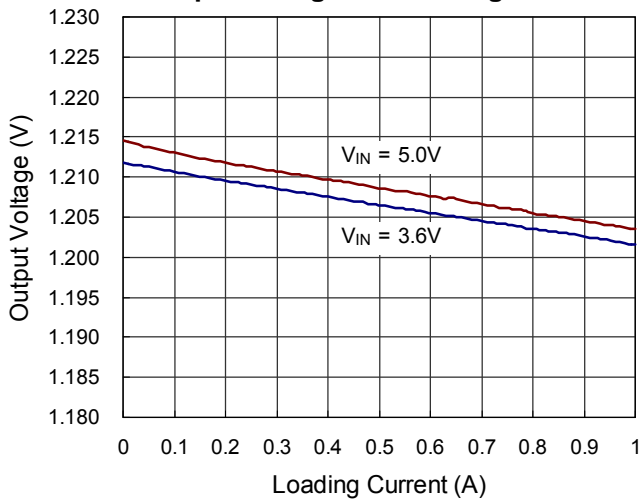
**Note 5.**  $\Delta V = I_{OUT} \times P_{RDS(ON)}$

**Note 6.** Guarantee by design.

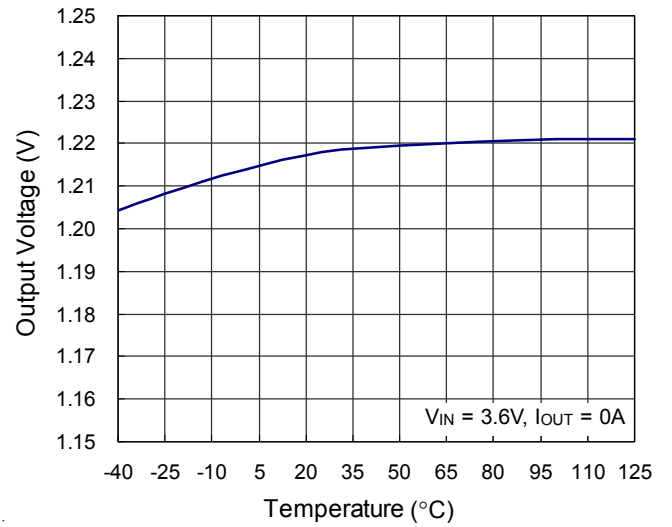
**Typical Operating Characteristics**



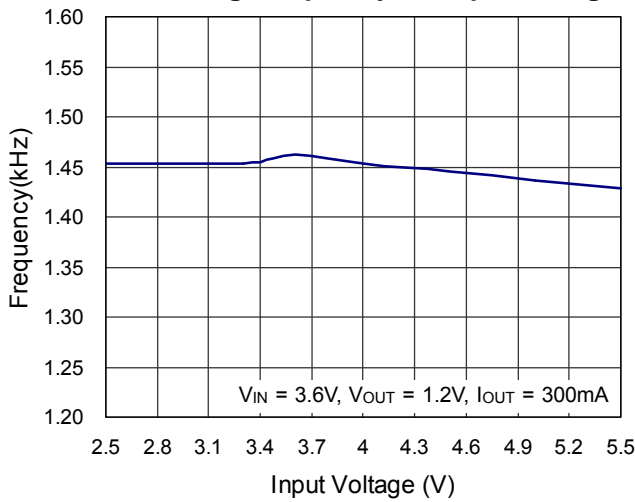
Output Voltage vs. Loading Current



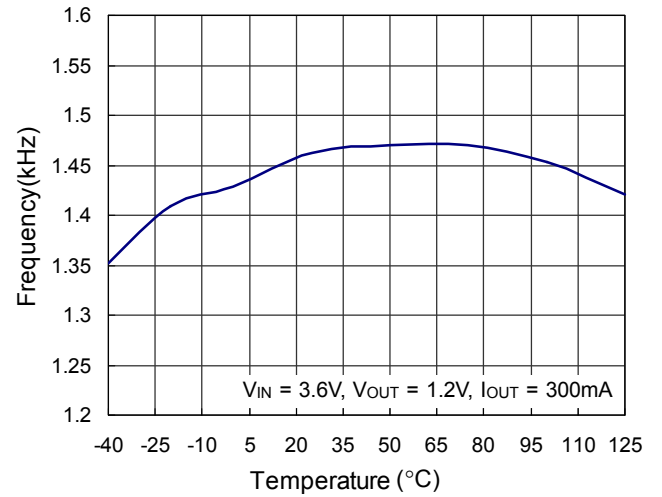
Output Voltage vs. Temperature



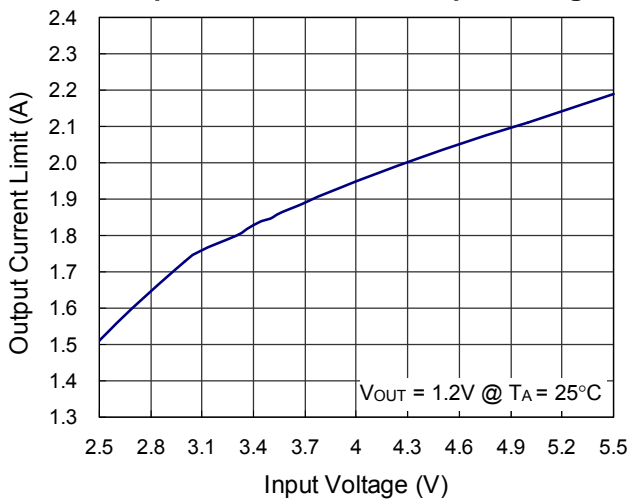
Switching Frequency vs. Input Voltage



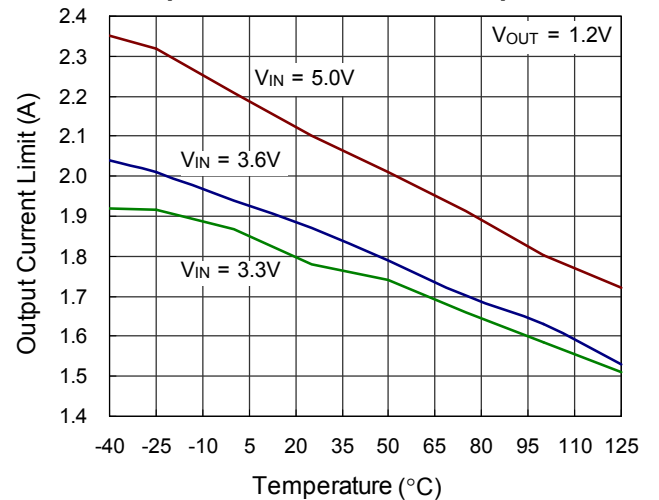
Switching Frequency vs. Temperature



Output Current Limit vs. Input Voltage

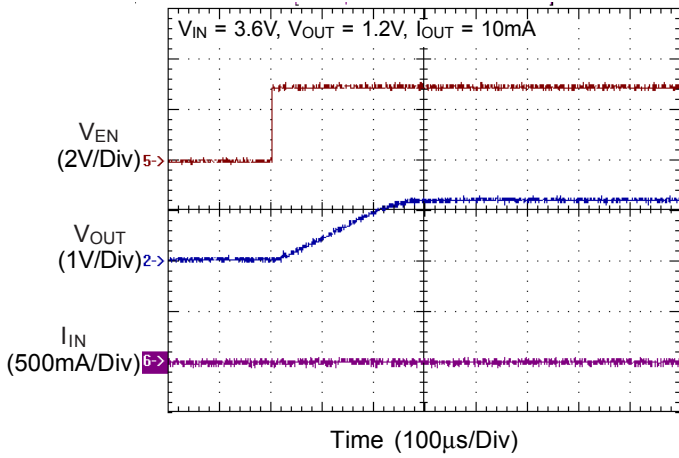


Output Current Limit vs. Temperature

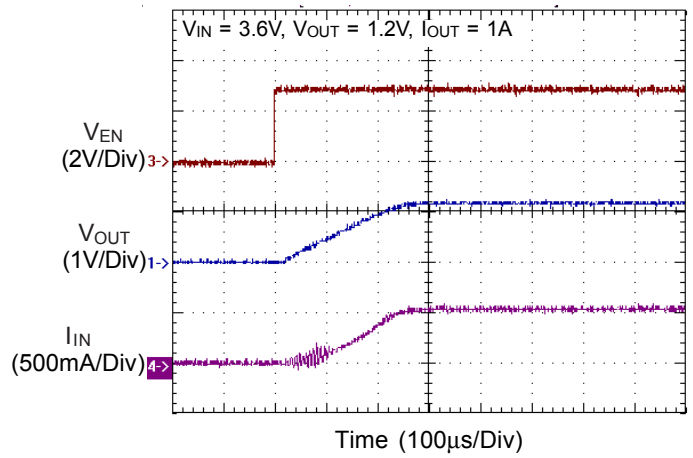




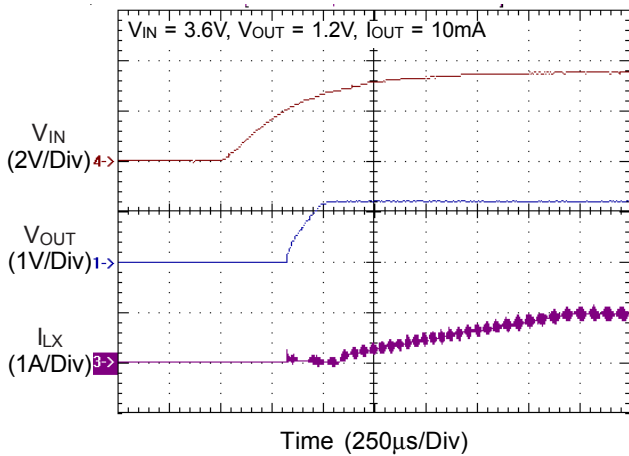
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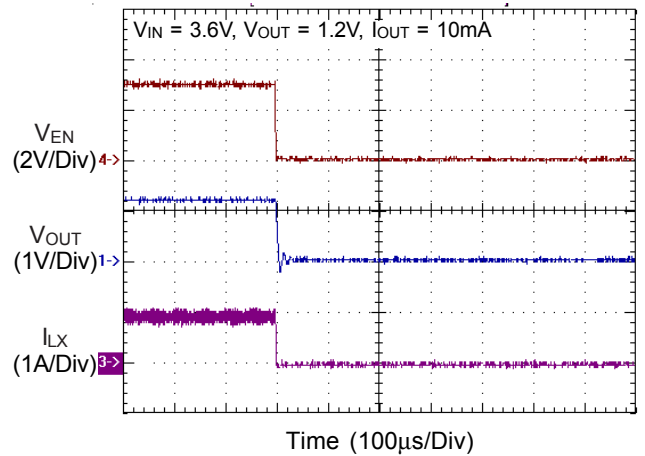
**Power On from EN**



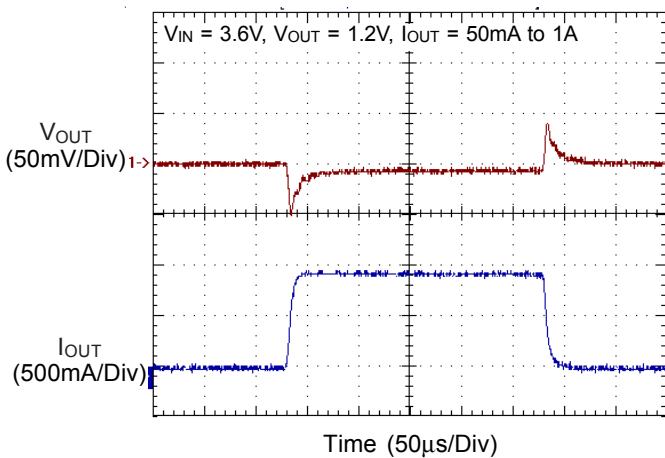
**Power On from V\_IN**



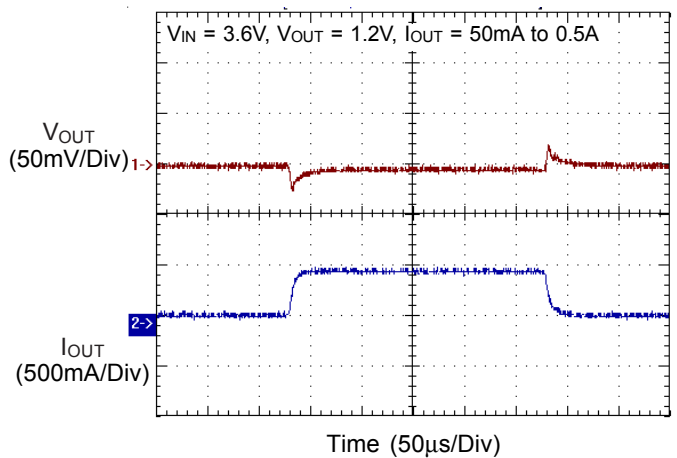
**Power Off from EN**



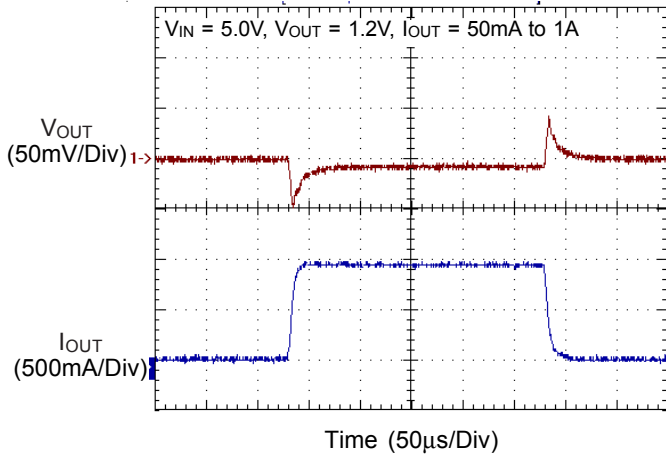
**Load Transient Response**



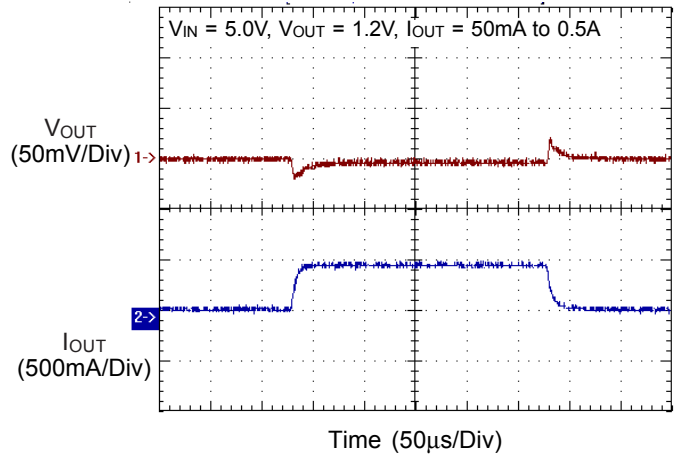
**Load Transient Response**



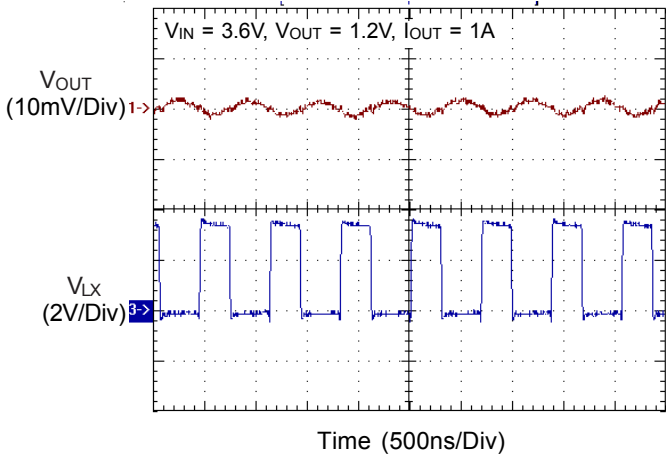
Load Transient Response



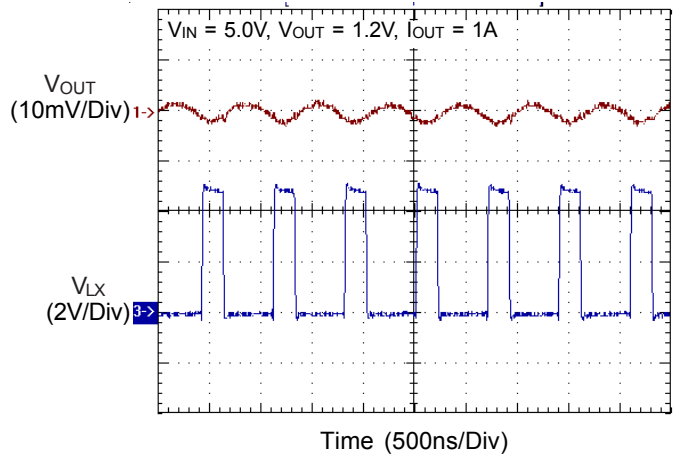
Load Transient Response



Ripple



Ripple



## Applications Information

The basic RT8020 application circuit is shown in Typical Application Circuit. External component selection is determined by the maximum load current and begins with the selection of the inductor value and operating frequency followed by  $C_{IN}$  and  $C_{OUT}$ .

### Inductor Selection

For a given input and output voltage, the inductor value and operating frequency determine the ripple current. The ripple current  $\Delta I_L$  increases with higher  $V_{IN}$  and decreases with higher inductance.

$$\Delta I_L = \left[ \frac{V_{OUT}}{f \times L} \right] \times \left[ 1 - \frac{V_{OUT}}{V_{IN}} \right]$$

Having a lower ripple current reduces the ESR losses in the output capacitors and the output voltage ripple. Highest efficiency operation is achieved at low frequency with small ripple current. This, however, requires a large inductor.

A reasonable starting point for selecting the ripple current is  $\Delta I_L = 0.4(I_{MAX})$ . The largest ripple current occurs at the highest  $V_{IN}$ . To guarantee that the ripple current stays below a specified maximum, the inductor value should be chosen according to the following equation :

$$L = \left[ \frac{V_{OUT}}{f \times \Delta I_L(MAX)} \right] \times \left[ 1 - \frac{V_{OUT}}{V_{IN(MAX)}} \right]$$

### Inductor Core Selection

Once the value for L is known, the type of inductor must be selected. High efficiency converters generally cannot afford the core loss found in low cost powdered iron cores, forcing the use of more expensive ferrite or permalloy cores. Actual core loss is independent of core size for a fixed inductor value but it is very dependent on the inductance selected. As the inductance increases, core losses decrease. However, increased inductance requires more turns of wire and therefore copper losses will increase.

Ferrite designs have very low core losses and are preferred at high switching frequencies, so design goals can concentrate on copper loss and preventing saturation. Ferrite core material saturates "hard", which means that inductance collapses abruptly when the peak design current is exceeded.

This results in an abrupt increase in inductor ripple current and consequent output voltage ripple.

Do not allow the core to saturate!

Different core materials and shapes will change the size/current and price/current relationship of an inductor. Toroid or shielded pot cores in ferrite or permalloy materials are small and don't radiate energy but generally cost more than powdered iron core inductors with similar characteristics. The choice of which style inductor to use mainly depend on the price vs. size requirements and any radiated field/EMI requirements.

### $C_{IN}$ and $C_{OUT}$ Selection

The input capacitance,  $C_{IN}$ , is needed to filter the trapezoidal current at the source of the top MOSFET. To prevent large ripple voltage, a low ESR input capacitor sized for the maximum RMS current should be used. RMS current is given by :

$$I_{RMS} = I_{OUT(MAX)} \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}} - 1}$$

This formula has a maximum at  $V_{IN} = 2V_{OUT}$ , where  $I_{RMS} = I_{OUT}/2$ . This simple worst-case condition is commonly used for design because even significant deviations do not offer much relief. Note that ripple current ratings from capacitor manufacturers are often based on only 2000 hours of life which makes it advisable to further de-rate the capacitor, or choose a capacitor rated at a higher temperature than required. Several capacitors may also be paralleled to meet size or height requirements in the design.

The selection of  $C_{OUT}$  is determined by the effective series resistance (ESR) that is required to minimize voltage ripple and load step transients, as well as the amount of bulk capacitance that is necessary to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response as described in a later section.

The output ripple,  $\Delta V_{OUT}$ , is determined by :

$$\Delta V_{OUT} \leq \Delta I_L \left[ ESR + \frac{1}{8fC_{OUT}} \right]$$

The output ripple is highest at maximum input voltage since  $\Delta I_L$  increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirements. Dry tantalum, special polymer, aluminum electrolytic and ceramic capacitors are all available in surface mount packages. Special polymer capacitors offer very low ESR but have lower capacitance density than other types. Tantalum capacitors have the highest capacitance density but it is important to only use types that have been surge tested for use in switching power supplies. Aluminum electrolytic capacitors have significantly higher ESR but can be used in cost-sensitive applications provided that consideration is given to ripple current ratings and long-term reliability. Ceramic capacitors have excellent low ESR characteristics but can have a high voltage coefficient and audible piezoelectric effects. The high Q of ceramic capacitors with trace inductance can also lead to significant ringing.

### Using Ceramic Input and Output Capacitors

Higher values, lower cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal for switching regulator applications. However, care must be taken when these capacitors are used at the input and output. When a ceramic capacitor is used at the input and the power is supplied by a wall adapter through long wires, a load step at the output can induce ringing at the input,  $V_{IN}$ . At best, this ringing can couple to the output and be mistaken as loop instability. At worst, a sudden inrush of current through the long wires can potentially cause a voltage spike at  $V_{IN}$  large enough to damage the part.

### Output Voltage Programming

The resistive divider allows the FB pin to sense a fraction of the output voltage as shown in Figure 3.

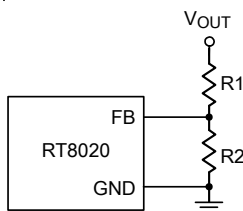


Figure 3. Setting the Output Voltage

For adjustable voltage mode, the output voltage is set by an external resistive divider according to the following equation :

$$V_{OUT} = V_{REF} \times (1 + R1/R2)$$

Where  $V_{REF}$  is the internal reference voltage (0.6V typical)

### Efficiency Considerations

The efficiency of a switching regulator is equal to the output power divided by the input power times 100%. It is often useful to analyze individual losses to determine what is limiting the efficiency and which change would produce the most improvement. Efficiency can be expressed as :

$$\text{Efficiency} = 100\% - (L1 + L2 + L3 + \dots)$$

where  $L1$ ,  $L2$ , etc. are the individual losses as a percentage of input power. Although all dissipative elements in the circuit produce losses, two main sources usually account for most of the losses:  $V_{IN}$  quiescent current and  $I^2R$  losses.

The  $V_{IN}$  quiescent current loss dominates the efficiency loss at very low load currents whereas the  $I^2R$  loss dominates the efficiency loss at medium to high load currents. In a typical efficiency plot, the efficiency curve at very low load currents can be misleading since the actual power lost is of no consequence.

1. The  $V_{IN}$  quiescent current appears due to two components : the DC bias current and the gate charge currents. The gate charge current results from switching the gate capacitance of the internal power MOSFET switches. Each time the gate is switched from high to low to high again, a packet of charge  $\Delta Q$  moves from  $V_{IN}$  to ground.

The resulting  $\Delta Q/\Delta t$  is the current out of  $V_{IN}$  that is typically larger than the DC bias current. In continuous mode,

$$I_{GATECHG} = f(Q_T + Q_B)$$

where  $Q_T$  and  $Q_B$  are the gate charges of the internal top and bottom switches. Both the DC bias and gate charge losses are proportional to  $V_{IN}$  and thus their effects will be more pronounced at higher supply voltages.

2.  $I^2R$  losses are calculated from the resistances of the internal switches,  $R_{SW}$  and external inductor  $R_L$ . In continuous mode the average output current flowing

through inductor L is “chopped” between the main switch and the synchronous switch. Thus, the series resistance looking into the LX pin is a function of both top and bottom MOSFET  $R_{DS(ON)}$  and the duty cycle (DC) is shown as follows :

$$R_{SW} = R_{DS(ON)TOP} \times DC + R_{DS(ON)BOT} \times (1 - DC)$$

The  $R_{DS(ON)}$  for both the top and bottom MOSFETs can be obtained from the Typical Performance Characteristics curves. Thus, to obtain  $I^2R$  losses, simply add  $R_{SW}$  to  $R_L$  and multiply the result by the square of the average output current. Other losses including  $C_{IN}$  and  $C_{OUT}$  ESR dissipative losses and inductor core losses generally account for less than 2% of the total loss.

**Thermal Considerations**

The maximum power dissipation depends on the thermal resistance of IC package, PCB layout, the rate of surroundings airflow and temperature difference between junction to ambient. The maximum power dissipation can be calculated by following formula :

$$P_{D(MAX)} = (T_{J(MAX)} - T_A) / \theta_{JA}$$

Where  $T_{J(MAX)}$  is the maximum junction temperature,  $T_A$  is the ambient temperature and the  $\theta_{JA}$  is the junction to ambient thermal resistance. For recommended operating conditions specification of RT8020 DC/DC converter, where  $T_{J(MAX)}$  is the maximum junction temperature of the die and  $T_A$  is the ambient temperature. The junction to ambient thermal resistance  $\theta_{JA}$  is layout dependent. For WDFN-12L 3x3 packages, the thermal resistance  $\theta_{JA}$  is 60°C/W on the standard JEDEC 51-7 four-layers thermal test board. The maximum power dissipation at  $T_A = 25^\circ\text{C}$  can be calculated by following formula :

$$P_{D(MAX)} = (125^\circ\text{C} - 25^\circ\text{C}) / (60^\circ\text{C/W}) = 1.667\text{W for WDFN-12L 3x3 packages}$$

The maximum power dissipation depends on operating ambient temperature for fixed  $T_{J(MAX)}$  and thermal resistance  $\theta_{JA}$ . The Figure 4 of de-rating curves allows the designer to see the effect of rising ambient temperature on the maximum power allowed.

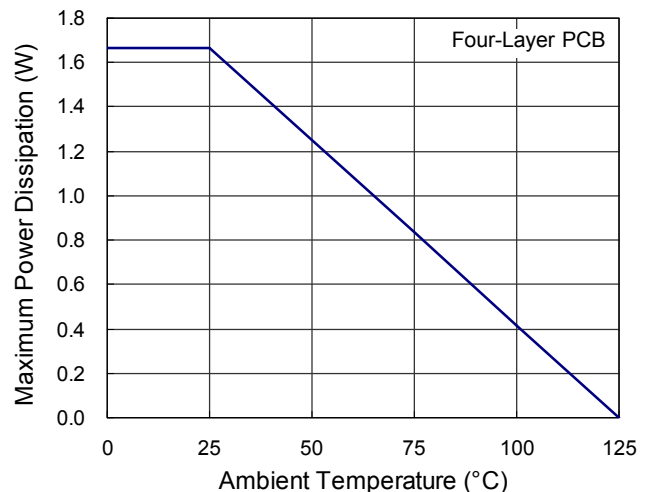


Figure 4. Derating Curve of Maximum Power Dissipation

**Checking Transient Response**

The regulator loop response can be checked by looking at the load transient response. Switching regulators take several cycles to respond to a step in load current. When a load step occurs,  $V_{OUT}$  immediately shifts by an amount equal to  $\Delta I_{LOAD}$  (ESR), where ESR is the effective series resistance of  $C_{OUT}$ .  $\Delta I_{LOAD}$  also begins to charge or discharge  $C_{OUT}$  generating a feedback error signal used by the regulator to return  $V_{OUT}$  to its steady-state value. During this recovery time,  $V_{OUT}$  can be monitored for overshoot or ringing that would indicate a stability problem.

**Layout Considerations**

Follow the PCB layout guidelines for optimal performance of RT8020.

- ▶ For the main current paths, keep their traces short and wide.
- ▶ Put the input capacitor as close as possible to the device pins ( $V_{IN}$  and GND).
- ▶ LX node is with high frequency voltage swing and should be kept small area. Keep analog components away from LX node to prevent stray capacitive noise pick-up.
- ▶ Connect feedback network behind the output capacitors. Keep the loop area small. Place the feedback components near the RT8020.
- ▶ Connect all analog grounds to a command node and then connect the command node to the power ground behind the output capacitors.

Table 1. Recommended Inductors

Component Supplier	Series	Inductance ( $\mu\text{H}$ )	DCR ( $\text{m}\Omega$ )	Current Rating (mA)	Dimensions (mm)
TAIYO YUDEN	NR 3015	2.2	60	1480	3 x 3 x 1.5
TAIYO YUDEN	NR 3015	4.7	120	1020	3 x 3 x 1.5
Sumida	CDRH2D14	2.2	75	1500	4.5 x 3.2 x 1.55
Sumida	CDRH2D14	4.7	135	1000	4.5 x 3.2 x 1.55
GOTREND	GTSD32	2.2	58	1500	3.85 x 3.85 x 1.8
GOTREND	GTSD32	4.7	146	1100	3.85 x 3.85 x 1.8

Table 2. Recommended Capacitors for  $C_{\text{IN}}$  and  $C_{\text{OUT}}$ 

Component Supplier	Part No.	Capacitance ( $\mu\text{F}$ )	Case Size
TDK	C1608JB0J475M	4.7	0603
TDK	C2012JB0J106M	10	0805
MURATA	GRM188R60J475KE19	4.7	0603
MURATA	GRM219R60J106ME19	10	0805
TAIYO YUDEN	JMK107BJ475RA	4.7	0603
TAIYO YUDEN	JMK107BJ106MA	10	0603
TAIYO YUDEN	JMK212BJ106RD	10	0805