RICHTEK®

1.5MHz, 600mA, High Efficiency PWM Step-Down Converter

General Description

The RT8099 is a Pulse-Width-Modulated (PWM) DC/DC step-down converter, and is capable of delivering 0.6A output current over a wide input voltage range from 2.7V to 5.5V. The RT8099 is ideally suited for portable electronic devices that are powered from 1-cell Li-ion battery such as cellular phones, PDAs and handy-terminals. Internal synchronous rectifier with low $R_{DS(ON)}$ dramatically reduces conduction loss at PWM mode. No external schottky barrier diode is required in practical application.

The RT8099 enters low-dropout mode when normal PWM cannot provide regulated output voltage by continuously turning on the high-side P-MOSFET. The RT8099 enters shut-down mode and consumes less than 0.1μ A when the EN pin is pulled low. The switching ripple is easily smoothed-out by small package filtering elements due to 1.5MHz high switching frequency. Other features include soft-start, auto discharge, lower internal reference voltage, over-temperature protection, and over-current protection.

The RT8099 is available in the small UDFN-6L 1.6x1.6 package for saving PCB space.

Features

- 2.7V to 5.5V Input Range
- Adjustable Output from 0.7V to 5V
- 0.6A Output Current
- 95% Efficiency
- No Schottky Barrier Diode Required
- 1.5MHz Spread Spectrum Frequency PWM Operation
- Auto Discharge Function
- Over-Current Protection
- Overt-Temperature Protection
- Integrated Soft-Start Function
- Small 6-Lead UDFN Package
- RoHS Compliant and Halogen Free

Applications

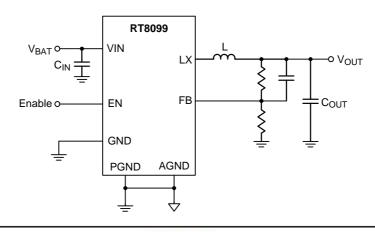
- Cellular Telephones
- Personal Information Appliances
- Wireless and DSL Modems
- MP3 Players
- Portable Instruments

Marking Information



0U : Product Code W : Date Code

Simplified Application Circuit





Ordering Information

RT8099 🖵 📮

Package Type
 QU : UDFN-6L 1.6x1.6 (U-Type)
 Lead Plating System
 G : Green (Halogen Free and Pb Free)

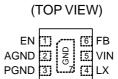
Note :

Richtek products are :

- RoHS compliant and compatible with the current requirements of IPC/JEDEC J-STD-020.
- Suitable for use in SnPb or Pb-free soldering processes.

Functional Pin Description

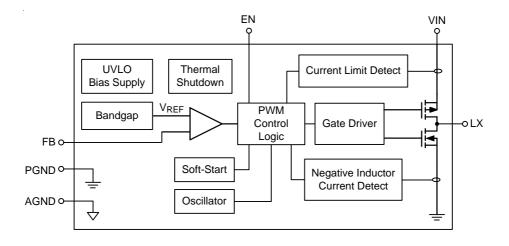
Pin Configuration



UDFN-6L 1.6x1.6

Pin No.	Pin Name	Pin Function				
1	EN	Enable control input (active high).				
2	AGND	nalog ground.				
3	PGND	Power ground.				
4	LX	Switch node.				
5	VIN	Power input.				
6	FB	Feedback voltage input.				
		Ground. The exposed pad must be soldered to a large PCB and connected to GND for maximum power dissipation.				

Functional Block Diagram



Operation

The RT8099 is a synchronous DC/DC step-down converter that can support the input voltage range from 2.7V to 5.5V. The output current is up to 600mA. While the power plugs in and EN = H, V_{OUT} is soft-started to avoid the inrush current of VIN by the soft-start block. Normally, the highside MOSFET is turned on by the PWM control logic block which drives the gate driver block when V_{FB} is lower than the internal reference voltage. After V_{FB} is higher than the internal reference voltage, the high-side MOSFET will be turned off. While the high-side MOSFET is turned off, the low-side MOSFET is turned on until the current of the inductor is around zero by the negative inductor current detection block. When the current of high-side MOSFET is over the rating current, the high-side MOSFET is turned off. When the temperature is over the rating temperature, the high-side MOSFET is turned off until the temperature is dropped by the thermal shutdown block. After the thermal shutdown is released, V_{OUT} will be soft-started again. When VIN is lower than 2.1V, the high-side MOSFET is turned off by the UVLO block. After VIN is higher than 2.2V, V_{OUT} will be soft-started again. The reference voltage is provided by the bandgap block. The internal clock related to the switching frequency is provided by the oscillator block.



Absolute Maximum Ratings (Note 1)

Supply Input Voltage, VIN	6V
• EN, FB Pin Voltage	–0.3V to V_{IN}
• Power Dissipation, $P_D @ T_A = 25^{\circ}C$	
UDFN-6L 1.6x1.6	2.15W
Package Thermal Resistance (Note 2)	
UDFN-6L 1.6x1.6, θ _{JA}	46.5°C/W
• Lead Temperature (Soldering, 10 sec.)	260°C
Junction Temperature	150°C
Storage Temperature Range	–65°C to 150°C
ESD Susceptibility (Note 3)	
HBM (Human Body Model)	2kV

Recommended Operating Conditions (Note 4)

Supply Input Voltage, VIN	· 2.3V to 5.5V
Junction Temperature Range	 −40°C to 125°C
Ambient Temperature Range	 −40°C to 85°C

Electrical Characteristics

 $(V_{\text{IN}} = 3.6\text{V}, V_{\text{OUT}} = 1.8\text{V}, V_{\text{REF}} = 0.6\text{V}, L = 2.2\mu\text{H}, C_{\text{IN}} = 4.7\mu\text{F}, C_{\text{OUT}} = 10\mu\text{F}, I_{\text{MAX}} = 0.6\text{A}, T_{\text{A}} = 25^{\circ}\text{C}, \text{ unless otherwise specified})$

Parameter		Symbol	Test Conditions		Min	Тур	Max	Unit
Input Voltage Start-Up VIN		VIN			2.3		5.5	V
Input Voltage Range		Vin	I _{OUT} = 600mA		2.7		5.5	V
Quiescent Current for Adjustable Output Voltage		I _{Q_adj}	$I_{OUT} = 0mA$, $V_{FB} = V_{REF} + 10\%$, without include EN pin current (Note 5)			20	35	μΑ
Shutdown Cu	rrent	ISHDN	EN = GND			0.1	1	μΑ
Reference Voltage		Vref	For Adjustable Output Voltage		0.591	0.6	0.609	V
Adjustable Output Range		Vout			0.7		V _{IN}	V
Output Voltage Accuracy		ΔVout	$V_{IN} = 2.7V$ to 5.5V, 0A < $I_{OUT} < 0.6A$		-3		3	%
FB Input Current		I _{FB}	V _{FB} = V _{IN}		-50		50	nA
High-Side MOSFET On-Resistance		RDS(ON)_P	I _{OUT} = 200mA	V _{IN} = 3.6V		0.28		Ω
				V _{IN} = 2.5V		0.38		
Low-Side MOSFET On-Resistance		R _{DS(ON)} _N	I _{OUT} = 200mA	V _{IN} = 3.6V		0.25		Ω
				V _{IN} = 2.5V		0.35		
High-Side MOSFET Current Limit		ILIM_P			1	1.5	2	A
EN Input Voltage Logic-High		V _{EN_H}			1.5			V
		V _{EN_L}					0.4	
Under Voltage Lock Out Threshold (Rising)		UVLO_R	V _{IN} Rising		2.1	2.2	2.3	V
UVLO Hysteresis		UVLO_Hys	V _{IN} Falling			0.1		V

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Parameter	Symbol	Test Conditions	Min	Тур	Max	Unit
Oscillator Frequency	fosc	V _{IN} = 3.6V, I _{OUT} = 600mA		1.5		MHz
Thermal Shutdown Temperature	T _{SD}			150		°C
Maximum Duty Cycle			100			%
Soft-Start Time	tss			150		μS
Discharge Time	tDIS	Cout = 10μF		5	10	ms
EN Pull-Low Resistor	R _{EN}			300		kΩ

Note 1. Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions may affect device reliability.

Note 2. θ_{JA} is measured at $T_A = 25^{\circ}C$ on a high effective thermal conductivity four-layer test board per JEDEC 51-7.

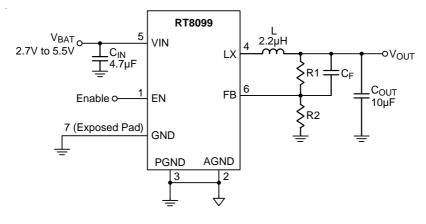
Note 3. Devices are ESD sensitive. Handling precaution is recommended.

Note 4. The device is not guaranteed to function outside its operating conditions.

Note 5. Supply 660mV in FB pin and record the VIN pin current.



Typical Application Circuit

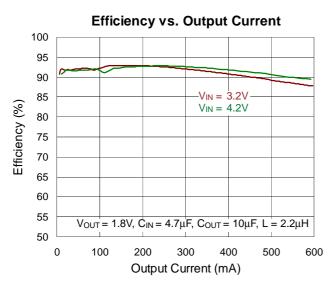


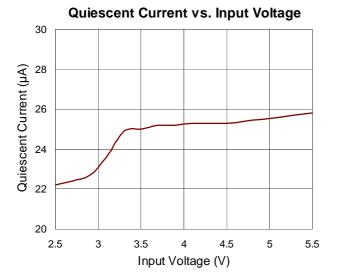
 $V_{OUT} = V_{REF} \times \left(1 + \frac{R1}{R2}\right)$

with R2 = $60k\Omega$ to $300k\Omega$ so the I_{R2} = 10μ A to 2μ A, and (R1 x C_{FF}) should be in the range between 22.4 x 10^{-6} and 88 x 10^{-6} for component selection.

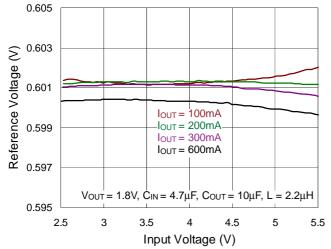


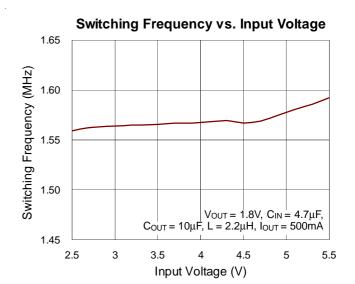
Typical Operating Characteristics



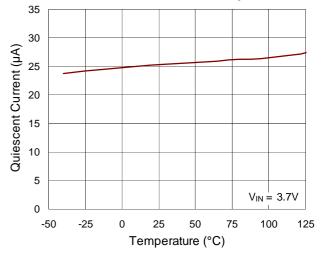




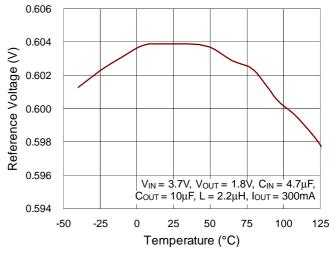




Quiescent Current vs. Temperature



Reference Voltage vs. Temperature

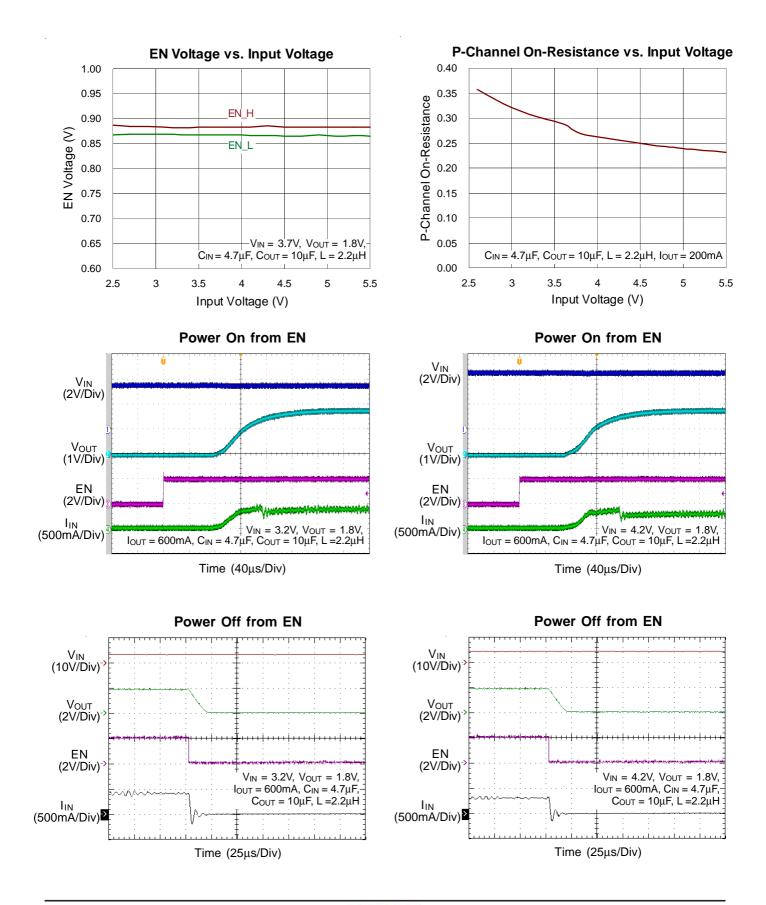


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Applications Information

The basic RT8099 application circuit is shown in Typical Application Circuit. External component selection is determined by the maximum load current and begins with the selection of the inductor value and operating frequency followed by C_{IN} and C_{OUT} .

Inductor Selection

For a given input and output voltage, the inductor value and operating frequency determine the ripple current. The ripple current ΔI_L increases with higher VIN and decreases with higher inductance.

$$\Delta I_{L} = \left(\frac{V_{OUT}}{f \times L}\right) \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

Having a lower ripple current reduces the ESR losses in the output capacitors and the output voltage ripple. Highest efficiency operation is achieved at low frequency with small ripple current. This, however, requires a large inductor.

A reasonable starting point for selecting the ripple current is $\Delta I_L = 0.4$ (IMAX). The largest ripple current occurs at the highest VIN. To guarantee that the ripple current stays below a specified maximum, the inductor value should be chosen according to the following equation :

 $L = \left(\frac{V_{OUT}}{f \times \Delta I_{L}(MAX)}\right) \times \left(1 - \frac{V_{OUT}}{V_{IN}(MAX)}\right)$

A 2.2 μ H inductor is recommended for L.

Model	Vendor	Dimensions L x W x H (mm)
NR4018T2R2M	Taiyo	4.0 x 4.0 x 1.8
VLS3010ET-2R2M	TDK	3.0 x 3.0 x 1.0
NR3010T2R2M	Taiyo	3.0 x 3.0 x 1.0
SWPA3010S2R2NT	Sunlord	3.0 x 3.0 x 1.0

Table 1. Suggested Inductors and Suppliers

C_{IN} and C_{OUT} Selection

The input capacitance, C_{IN} , is needed to filter the trapezoidal current at the Source of the high-side MOSFET. To prevent large ripple voltage, a low ESR input capacitor sized for the maximum RMS current should be used. RMS current is given by :

 $I_{RMS} = I_{OUT}(MAX) \frac{V_{OUT}}{V_{IN}} \sqrt{\frac{V_{IN}}{V_{OUT}} - 1}$

This formula has a maximum at $V_{IN} = 2V_{OUT}$, where $I_{RMS} = I_{OUT} / 2$. This simple worst-case condition is commonly used for design because even significant deviations do not offer much relief. Note that ripple current ratings from capacitor manufacturers are often based on only 2000 hours of life which makes it advisable to further derate the capacitor, or choose a capacitor rated at a higher temperature than required. Several capacitors may also be paralleled to meet size or height requirements in the design.

The selection of C_{OUT} is determined by the Effective Series Resistance (ESR) that is required to minimize voltage ripple and load step transients, as well as the amount of bulk capacitance that is necessary to ensure that the control loop is stable. Loop stability can be checked by viewing the load transient response as described in a later section. The output ripple, ΔV_{OUT} , is determined by :

$\Delta V_{OUT} \leq \Delta I_L \left(\text{ESR} + \frac{1}{8 f C_{OUT}} \right)$

The output ripple is highest at maximum input voltage since ΔI_L increases with input voltage. Multiple capacitors placed in parallel may be needed to meet the ESR and RMS current handling requirements. Dry tantalum, special polymer, aluminum electrolytic and ceramic capacitors are all available in surface mount packages. Special polymer capacitors offer very low ESR but have lower capacitance density than other types. Tantalum capacitors have the highest capacitance density but it is important to only use types that have been surge tested for use in switching power supplies. Aluminum electrolytic capacitors have significantly higher ESR but can be used in cost-sensitive applications that consideration is given to ripple current ratings and long term reliability. Ceramic capacitors have excellent low ESR characteristics but have a high voltage coefficient and audible piezoelectric effects. The high Q of ceramic capacitors with trace inductance can also lead to significant ringing.

Using Ceramic Input and Output Capacitors

Higher values, lower cost ceramic capacitors are now becoming available in smaller case sizes. Their high ripple current, high voltage rating and low ESR make them ideal

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for switching regulator applications. However, care must be taken when these capacitors are used at the input and output. When a ceramic capacitor is used at the input and the power is supplied by a wall adapter through long wires, a load step at the output can induce ringing at the input, VIN. At best, this ringing can couple to the output and be mistaken as loop instability. At worst, a sudden inrush of current through the long wires can potentially cause a voltage spike at VIN large enough to damage the part.

Output Voltage Programming

The resistive divider allows the FB pin to sense a fraction of the output voltage as shown in Figure 2.

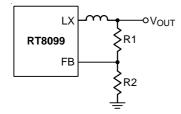


Figure 2. Setting the Output Voltage

For adjustable voltage mode, the output voltage is set by an external resistive divider according to the following equation :

 $V_{OUT} = V_{REF} \left(1 + \frac{R1}{R2} \right)$

where V_{REF} is the internal reference voltage (0.6V typ.)

Thermal Considerations

For continuous operation, do not exceed absolute maximum junction temperature. The maximum power dissipation depends on the thermal resistance of the IC package, PCB layout, rate of surrounding airflow, and difference between junction and ambient temperature. The maximum power dissipation can be calculated by the following formula :

$$\mathsf{P}_{\mathsf{D}(\mathsf{MAX})} = (\mathsf{T}_{\mathsf{J}(\mathsf{MAX})} - \mathsf{T}_{\mathsf{A}}) / \theta_{\mathsf{J}\mathsf{A}}$$

where $T_{J(MAX)}$ is the maximum junction temperature, T_A is the ambient temperature, and θ_{JA} is the junction to ambient thermal resistance.

For recommended operating condition specifications, the maximum junction temperature is 125°C. The junction to ambient thermal resistance, θ_{JA} , is layout dependent. For UDFN-6L 1.6x1.6 package, the thermal resistance, θ_{JA} , is 46.5°C/W on a standard JEDEC 51-7 four-layer thermal test board. The maximum power dissipation at $T_A = 25$ °C can be calculated by the following formula :

 $P_{D(MAX)} = (125^{\circ}C - 25^{\circ}C) / (46.5^{\circ}C/W) = 2.15W \text{ for } UDFN-6L 1.6x1.6 \text{ package}$

The maximum power dissipation depends on the operating ambient temperature for fixed $T_{J(MAX)}$ and thermal resistance, θ_{JA} . The derating curve in Figure 3 allows the designer to see the effect of rising ambient temperature on the maximum power dissipation.

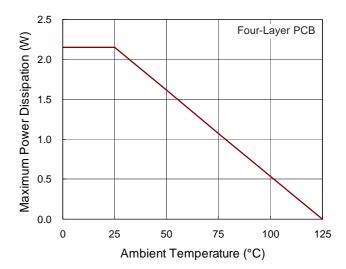


Figure 3. Derating Curve of Maximum Power Dissipation

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Layout Considerations

Follow the PCB layout guidelines for optimal performance of the RT8099.

- Put the input capacitor as close as possible to the device pins (VIN and GND).
- LX node is with high frequency voltage swing and should be kept small area. Keep analog components away from LX node to prevent stray capacitive noise pick-up.
- Connect feedback network behind the output capacitors.
 Keep the loop area small. Place the feedback components near the RT8099.
- Connect all analog grounds to a common node and then connect the common node to the power ground behind the output capacitors.

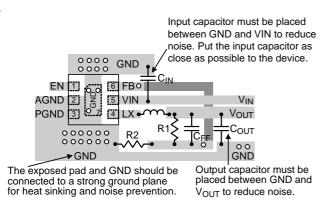


Figure 4. PCB Layout Guide